

N.I. 43-101 TECHNICAL REPORT & PRELIMINARY ECONOMIC ASSESSMENT FOR THE TURNAGAIN PROJECT – Amended

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REPORT AMENDMENTS

The attached report entitled “N.I. 43-101 Technical Report & Preliminary Economic Assessment For The Turnagain Project” (the “Technical Report”) prepared for Giga Metals Corporation and dated November 18, 2020 has been updated and refiled to provide the following additional detail and clarifying language:

1. In Section 1.12, the following wording was included “*The preliminary economic assessment is preliminary in nature. It includes inferred mineral resources that are too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that the preliminary economic assessment will be realized.*”
2. The fourth paragraph of Section 1.13, the final paragraph of Section 25.1, and the first paragraph of Section 26.1 were edited to the following “*This PEA indicates the Turnagain property generates an internal rate of return below the applied discount rate on the estimated N.I. 43-101 compliant resource at base case scenario modelling parameters. The project economics could improve with the opportunities noted in Section 25.8. It is recommended that Giga Metals carry the project forward to the pre-feasibility stage in accordance with the budget in Table 1.8. Recommendations by study area for the next phase are summarised in Section 26.*”
3. In Tables 1.2 and 16.1, a split between confidence classifications was added and the tables were retitled to “Scheduled In-pit Material”.
4. In Section 3.0, all commentary was removed.
5. In Sections 1, 14, 17, 18, 22, and 25, the term “ore” was replaced with the term “mineralized material” or “mill processing material” or “mill feed”.
6. In Figures 18-1, 18-3, 18-4 and 18-5, the graphic indication of a potential future Hatzl Open Pit was removed.
7. In Section 5.2, 5.3, 18.3.2 and 20.1.2, reference was added to the Turnagain Project Preliminary Economic Assessment, prepared by AMC Mining Consultants in 2011 (AMC 2011).
8. In Section 18.5.4, additional clarification language regarding the water balance modelling was provided.
9. In Section 20.1, additional clarification language regarding the environmental baseline programs was included.
10. In Section 6.3, detailed information on the 2018 drilling program was moved to Section 10.
11. In Section 8, an expanded description of the deposit was provided.
12. In Section 9, additional figures were provided to support the described exploration programs; past exploration programs that are not relevant to the current resource model were removed; and drilling information was moved to Section 10.
13. In Section 10, the description of the drill holes in the deposit area used for resource definition was improved, the drill hole map was replaced with an expanded view of the deposit, and tables of significant assay results and information on recent drill holes in the mineralization zones beyond the modeled deposit were added.

14. In Section 11, information on the 2018 QA/QC program was added.
15. In Table 13.5, the nickel grade on SGS 08-264 LCT 4 concentrate was corrected from 21.4% to 21.8% and the identification of test SGS 10-265 LCT3 was corrected to SGS 10-265 LCT2.
16. In Section 14 and 1.5, rationale around the inclusion of the Hatzl zone in the resource model, but exclusion from the current mine plan was added, further definition of the drill holes used in the resource model, and further information on the update of the resource model from 2011 were added.
17. In Section 23, improved compliance of discussion of adjacent properties with NI 43-101 requirements was provided.
18. Ian Thompson P.Eng. was re-designated as the QP for Sections 1.12, 22 and 25.7; Table 2.1 was updated accordingly.
19. In Sections 1.12 and 22, all references to the Wood Mackenzie ESG incentive price were removed. The 'PEA case' or 'Case 1' were relabelled as the 'PEA Base Case'.

Other than as noted above, the Technical Report remains the same in all respects.

IMPORTANT NOTICE TO READER

This report was prepared by the qualified persons (QPs) listed in Table 2.1. Each QP assumes responsibility for those sections or areas of this report that are referenced opposite their name in Table 2.1. None of the QPs, however, accepts any responsibility or liability for the sections or areas of this report that were prepared by other QPs. This report was prepared to allow Giga Metals Corporation (the "Owner") to reach informed decisions respecting the development of the Turnagain Project. Except for the purposes legislated under provincial securities law and without limiting any statutory right afforded thereunder, any use of this report by any third party is at that party's sole risk, and none of the contributors shall have any liability to any third party for any such use for any reason whatsoever, including negligence. This report is intended to be read as a whole, and sections should not be read or relied upon out of context. This report contains estimates, projections and conclusions that are forward-looking information within the meaning of applicable securities laws. Forward-looking statements are based upon the responsible QP's opinion at the time that they are made but in most cases involve significant risk and uncertainty. Although each of the responsible QPs has attempted to identify factors that could cause actual events or results to differ materially from those described in this report, there may be other factors that cause events or results to not be as anticipated, estimated or projected. None of the QPs undertake any obligation to update any information contained in this report, including, without limitation, any forward-looking information.

Report Contents

1.0	Summary	13
1.1	Introduction	13
1.2	Project Location	13
1.3	History	13
1.4	Geology & Mineralisation	14
1.5	Resource Estimate.....	14
1.6	Metallurgical Testing	16
1.7	Recovery Methods	18
1.8	Mining Methods.....	18
1.9	Infrastructure	21
	1.9.1 Power Supply.....	21
	1.9.2 Waste / Tailings Management.....	21
1.10	Environmental Considerations.....	21
1.11	Capital & Operating Costs	23
1.12	Economic Evaluation	24
1.13	Conclusions & Recommendations.....	26
2.0	Introduction	27
3.0	Reliance on Other Experts	29
4.0	Property Description & Location	30
4.1	Location.....	30
4.2	Mineral Claims	32
4.3	Permits & Environmental Liabilities	36
4.4	Royalties.....	37
5.0	Accessibility, Climate, Local Resources, Infrastructure & Physiography	38
5.1	Accessibility.....	38
5.2	Climate	39
5.3	Hydrology	40
5.4	Local Resources	43
5.5	Infrastructure	43
5.6	Physiography	44
6.0	History	47
6.1	2006-2008	48
6.2	2009-2011	48
6.3	2012-2019	49

7.0	Geological Setting & Mineralisation	50
7.1	Regional Geology.....	50
7.2	Property Geology	51
	7.2.1 Dunite	53
	7.2.2 Wehrlite.....	53
	7.2.3 Olivine Clinopyroxenite & Clinopyroxenite	53
	7.2.4 Hornblende Clinopyroxenite & Clinopyroxenite	54
	7.2.5 Magmatic Hornblendite & Hornblende Clinopyroxenite	54
	7.2.6 Hornblende Diorite.....	54
	7.2.7 Metasediments	54
7.3	Mineralisation	54
8.0	Deposit Types.....	57
9.0	Exploration	58
9.1	Geological Mapping	58
9.2	Geochemical Surveys	60
9.3	Geophysical Surveys	61
	9.3.1 Airborne Surveys	61
10.0	Drilling	63
10.1	Collar & Downhole Surveying	72
10.2	Significant Assay Intervals	73
11.0	Sample Preparation, Analyses & Security	79
11.1	Security & Chain of Custody	79
11.2	Sampling Methods	79
	11.2.1 Geotechnical Data	79
	11.2.2 Geological Data	80
	11.2.3 Sample Preparation and Analyses	80
	11.2.4 Density	81
11.3	Quality Assurance / Quality Control.....	81
11.4	Adequacy Statement.....	82
12.0	Data Verification.....	85
12.1	Site Visit & Verification	85
13.0	Mineral Processing & Metallurgical Testing	87
13.1	Introduction	87
13.2	Sources of Information for this Study.....	87
13.3	Grindability	88
13.4	Mineralogy.....	89
13.5	Flotation.....	92

13.6	Other Treatment Schemes.....	95
13.6.1	Two Concentrates	95
13.6.2	Hydrometallurgical Processing.....	96
13.7	Metallurgical Forecast.....	96
13.7.1	Introduction & Background	96
13.7.2	Rougher Flotation Recovery.....	97
13.7.3	Recovery to Final Concentrate.....	101
13.8	Final Concentrate Specifications	102
13.9	Recovery Methods & Equipment Selection	104
14.0	Mineral Resource Estimates	105
14.1	Introduction	105
14.2	Data.....	106
14.3	Data Analysis	108
14.4	Geology Model.....	111
14.5	Composites	118
14.6	Evaluation of Outlier Assay Values.....	122
14.7	Bulk Density Estimation	123
14.8	Variography.....	123
14.9	Block Model Definition	127
14.10	Resource Estimation Methodology.....	129
14.11	Resource Validation.....	129
14.12	Mineral Resource Classification	130
14.13	Sensitivity of the Block Model to Selection Cut-off Grade.....	131
14.14	Mineral Resource Statement	131
14.15	Discussion on Material Affects to the Mineral Resource Estimate.....	138
14.16	Comparison to Previous 2011 Mineral Resource Estimate.....	138
15.0	Mineral Reserve Estimates	140
16.0	Mining Methods.....	141
16.1	Summary.....	141
16.2	Open Pit Optimisation Study.....	143
16.2.1	Optimisation Parameters.....	144
16.2.2	Turnagain River Restriction.....	145
16.2.3	Pit Optimisation Variable – Net Metal Value	145
16.3	Pit Designs	148
16.3.1	Pit Slope Assumptions.....	153
16.3.2	In-Pit Resource Potential.....	153
16.3.3	Reported Grade Items	154
16.3.4	Cut-off Grade.....	154
16.3.5	Mineralisation Dilution	155

16.4	Mine Plan Development.....	156
16.4.1	Preliminary Mining Phases.....	156
16.5	Mine Production Schedule.....	158
16.6	Mine Equipment.....	161
16.6.1	Mobile Fleet.....	161
16.6.2	Mine Buildings.....	162
16.7	Waste Disposal & LG Stockpile Management Facility.....	162
17.0	Recovery Methods.....	164
17.1	Introduction.....	164
17.2	Process Design Criteria.....	164
17.3	Process Description.....	164
17.4	Phased Expansion.....	170
18.0	Project Infrastructure.....	172
18.1	Site Access Road.....	172
18.2	Waste Management Facility Alternatives.....	173
18.3	Waste Rock Management Facility.....	174
18.3.1	Non-Reactive Waste Rock.....	174
18.3.2	Potentially Reactive Waste Rock.....	174
18.4	Tailings Management Facility.....	175
18.4.1	Design Basis & Operating Criteria.....	175
18.4.2	Layout & Operating Strategy.....	177
18.5	Water & Waste Management.....	181
18.5.1	Site Water Management.....	181
18.5.2	TMF Water Management.....	181
18.5.3	Waste Dump, Low-Grade Stockpile, Open Pit & Plant Site Water Management.....	181
18.5.4	Site Water Balance.....	182
18.5.5	Water Supply.....	183
18.5.6	Sewage Disposal.....	183
18.5.7	Refuse Disposal.....	183
18.6	Plant Site Layout.....	183
18.7	Ancillary Facilities.....	185
18.7.1	Administration Building.....	185
18.7.2	Camp.....	185
18.7.3	Mine Dry.....	185
18.7.4	Truck Shop.....	186
18.7.5	Light Vehicle Maintenance/ Warehouse.....	186
18.7.6	Open Area Storage.....	186
18.7.7	Assay Laboratory.....	186
18.7.8	Fuel Storage & Distribution.....	186

18.7.9	Security/Gatehouse	187
18.8	Power Supply	187
18.9	Site Power Distribution.....	189
18.10	Communication System	190
19.0	Market Studies & Contracts	191
19.1	Nickel Markets.....	191
19.1.1	Overview	191
19.1.2	Uses & Marketing	191
19.1.3	Supply/Demand	191
19.1.4	Pricing	195
19.2	Cobalt Markets	197
19.2.1	Uses & Marketing	197
19.2.2	Supply/Demand	197
19.2.3	Pricing	199
19.3	Concentrate Markets.....	199
19.3.1	Nickel Concentrate Supply/Demand	199
19.3.2	Indicative Terms for Turnagain Concentrate.....	200
20.0	Environmental Baseline Studies, Permitting & Social or Community Impact	203
20.1	Environmental Baseline Studies	203
20.1.1	Aquatic Life	203
20.1.2	Surface Water Quality	204
20.1.3	Soil Quality.....	204
20.1.4	Groundwater Flows	204
20.1.5	Groundwater Quality.....	204
20.1.6	Archaeological Studies	205
20.2	Regulatory Requirements	205
20.2.1	Environmental Impact Assessment	205
20.2.2	Permits & Approvals	205
20.3	Indigenous Groups & Local Communities	206
20.3.1	Indigenous Groups	207
20.3.2	Local Communities	210
20.4	Government Agencies Consultation & Engagement	211
20.5	Reclamation & Closure Plan	211
20.6	Greenhouse Gases (GHGs)	212
20.6.1	Sequestration of Carbon Dioxide with Mine Tailings	212
20.6.2	GHG Reduction Opportunity through Fleet Electrification	213
21.0	Capital & Operating Costs	215
21.1	Capital Cost Estimate	215
21.1.1	Mining	215

21.1.2	On-Site Infrastructure & Process Plant	216
21.1.3	Off-Site Infrastructure	217
21.1.4	Waste / Tailings Management Facilities (TMF).....	218
21.2	Operating Cost Estimate.....	220
21.2.1	Staffing Numbers.....	220
21.2.2	Mining	222
21.2.3	Concentrator	223
21.2.4	Off-site Charges	223
21.2.5	General & Administration (G&A) Costs	223
21.2.6	Tailings Management Facility	223
22.0	Economic Analysis	224
22.1	Introduction	224
22.2	Returns Summary	224
22.3	PEA Base Case Assumptions & Inputs	226
22.3.1	General	226
22.3.2	Nickel & Cobalt Pricing.....	226
22.3.3	Ore Production & Processing.....	226
22.3.4	Concentrate Terms & Transportation Costs.....	228
22.3.5	Site Operating Costs	228
22.3.6	Capital Costs	229
22.3.7	Royalties	230
22.3.8	Taxes	230
22.3.9	Working Capital	230
22.4	Cash Flow	230
22.4.1	Annual Cash Flow Summary.....	230
22.4.2	Unit Cash Flow Summary.....	233
22.5	Sensitivity Analysis.....	233
23.0	Adjacent Properties	243
23.1	Kutcho Copper-Zinc-Silver-Gold Deposit	243
23.2	Eaglehead Copper-Molybdenum-Gold Deposit.....	243
24.0	Other Relevant Data & Information	244
25.0	Interpretation & Conclusions	245
25.1	Geology & Mineral Resources	245
25.2	Mining.....	246
25.3	Metallurgical Testing	246
25.4	Recovery Methods	247
25.5	Tailings & Water Management	247
25.6	Power Supply	247
25.7	Economic Analysis.....	247

25.8	Opportunities & Risks	247
25.8.1	Risks	247
25.8.2	Opportunities	249
26.0	Recommendations	252
26.1	Introduction	252
26.2	Geology & Mineral Resources	252
26.3	Mining.....	252
26.3.1	Plant Throughput & Metal Recoveries	252
26.3.2	Increased Production Rate with Mine Resource Expansion.....	252
26.3.3	Geotechnical & Hydrogeological Risks	253
26.4	Metallurgical Testing	253
26.5	Recovery Methods	253
26.6	Project Infrastructure & Tailings Management Facility	254
26.7	Power Line	255
26.8	Environmental Baseline Studies, Permitting & Social or Community Impact.....	255
27.0	References	256
Attachment 1: Qualified Person Certificates		261
Attachment 2: Units of Measure, Acronyms & Abbreviations		i
	Units of Measure	i
	Abbreviations/Acronyms.....	iii

Tables

Table 1.1:	Mineral Resource Estimate	16
Table 1.2:	Scheduled In-pit Material	19
Table 1.3:	Project Initial/Expansion Capital Cost Summary	23
Table 1.4:	Project Sustaining Capital & Closure & Reclamation Cost Summary	23
Table 1.5:	Unit Operating Cost Summary	24
Table 1.6:	Returns Summary	24
Table 1.7:	PEA Base Case Key Economic Outputs.....	25
Table 1.8:	Pre-feasibility & Early Environmental Works Study Budget (now to mid-2022)	26
Table 2.1:	Persons Who Prepared or Contributed to this Technical Report	28
Table 4.1:	Mineral Claim Details	34
Table 5.1:	Location of Meteorology Stations.....	39
Table 10.1:	Summary of Drill Programs	63
Table 10.2:	Drill Hole Collars, Location & Orientation.....	64
Table 10.3:	Summary of Significant Assay Results for pre-2018 Drill Holes.....	74
Table 10.4:	Drill Intercepts from the Metallurgical Infill Program	76

Table 10.5: Drill Intercepts from the Infill Program.....	77
Table 13.1: Grindability Data from the Turnagain Project.....	88
Table 13.2: HPGR Data.....	89
Table 13.3: Modal Abundance from QEMSCAN Analysis of 34 Samples Studied by XPS in 2018 & 2019	91
Table 13.4: Typical Conditions used in Closed Circuit Flotation Testing at BCR.....	94
Table 13.5: Summary of Locked Cycle Test Data using Optimised Treatment Schemes	95
Table 13.6: Correlation Coefficients between Four Candidate Geometallurgical Parameters & Nickel Recovery (R-squared)	98
Table 13.7: Cleaner Stage Recoveries from Five Recent Locked & Super Cycle Tests	101
Table 13.8: Average Assay of 39 Elements in Five LCT Concentrates.....	102
Table 14.1: List of Analysis Elements & Method.....	107
Table 14.2: Lithology Codes & Descriptions for Statistical Grouping	109
Table 14.3: Statistics for Nickel, Cobalt & Sulphur	110
Table 14.4: Composite Statistics Weighted by Length	121
Table 14.5: Bulk Density Statistics by Zone.....	123
Table 14.6: Variography for Nickel, Cobalt & Sulphur by Zone	125
Table 14.7: Variography for Platinum & Palladium by Zone	126
Table 14.8: Search Ellipse Parameters for the Turnagain Deposit	129
Table 14.9: Sensitivity Analyses of Global Tonnage & Grades at Various Ni% Cut-off Grades	133
Table 14.10: Open Pit Mineral Resource Statement ^(1,2,3,4,5) for the Turnagain Project. Base Case Estimate at 0.1% Nickel Cut-off Grade.....	133
Table 14.11: Comparison of 2019 & 2011 Consolidated Mineral Resource Statement ^(1,2,3,4,5) for the Turnagain Project	139
Table 16.1: Schedule In-pit Material	141
Table 16.2: Preliminary Design Parameters for Optimised Pit	144
Table 16.3: Optimised Pit Shells (Cut-off on \$0.01/t Milled MHV Value)	146
Table 16.4: Updated Design Parameters for Optimised Pit – Base Case.....	147
Table 16.5: Base Case Optimised Pit – Updated Cost Parameters.....	148
Table 16.6: Horsetrail Pit Potential Resource	154
Table 16.7: Scheduling MHV Material Cut-off Grades.....	155
Table 16.8: Potential Resource by Horsetrail Pit Phases	157
Table 16.9: Production Forecast	159
Table 16.10: Strip Ratio – Actual & Effective by Grouped Periods.....	161
Table 16.11: Major Mine Equipment Fleets	161
Table 17.1: Key Process Design Criteria	165
Table 20.1: Government & Stakeholder Consultation & Engagement Completed to Date	211
Table 21.1: Project Initial/Expansion Capital Cost Summary	215
Table 21.2: Project Sustaining Capital & Closure & Reclamation Cost Summary	215
Table 21.3: Mine Capital Cost Estimate.....	216
Table 21.4: Mining Sustaining Cost Estimate	216
Table 21.5: On-site Infrastructure & Process Plant Direct Capital Cost	217

Table 21.6: Electrical Supply Capital Cost	217
Table 21.7: Electrical Supply Sustaining Capital Cost	218
Table 21.8: TMF Capital Costs	218
Table 21.9: TMF Sustaining Capital & Closure & Reclamation Costs	218
Table 21.10: Unit Operating Cost Summary	220
Table 21.11: Mine Operations Staffing – Average for Periods	221
Table 21.12: Processing Staffing Numbers	221
Table 21.13: Mine Operating Cost Estimate	222
Table 21.14: Concentrator Operating Costs (Steady State)	223
Table 22.1: Returns Summary	224
Table 22.2: PEA Base Case Key Economic Outputs	225
Table 22.3: Average Production Statistics	226
Table 22.4: Concentrate Terms & Transportation Costs	228
Table 22.5: Site Operating Cost per Tonne of Mill Feed Summary	228
Table 22.6: Project Initial/Expansion Capital Cost Summary	229
Table 22.7: Project Sustaining Capital & Closure & Reclamation Cost Summary	229
Table 22.8: PEA Base Case Cash Flow Summary – Years 1 to 29	231
Table 22.9: PEA Base Case Cash Flow Summary – Years 30 to 38	232
Table 22.10: Unit Cash Flow Summary	233
Table 22.11: NPV Pre-Tax @ 8% Sensitivity to Nickel Price & USD/CAD Exchange Rate	239
Table 22.12: NPV After-Tax @ 8% Sensitivity to Nickel Price & USD/CAD Exchange Rate	239
Table 22.13: IRR Pre-Tax Sensitivity to Nickel Price & USD/CAD Exchange Rate	240
Table 22.14: IRR After-Tax Sensitivity to Nickel Price & USD/CAD Exchange Rate	240
Table 22.15: NPV Pre-Tax @ 8% Sensitivity to Nickel Price & Nickel Payable %	241
Table 22.16: NPV After-Tax @ 8% Sensitivity to Nickel Price & Nickel Payable %	241
Table 22.17: IRR Pre-Tax Sensitivity to Nickel Price & Nickel Payable %	242
Table 22.18: IRR After-Tax Sensitivity to Nickel Price & Nickel Payable %	242
Table 25.1: Mineral Resource Estimate	245

Figures

Figure 1-1: Nickel Recovery to Concentrate as a Function of Sulphur Head Grade	18
Figure 1-2: Horsetrail Pits & Mine Infrastructure General Arrangement	20
Figure 4-1: Turnagain Project Location Overview Map	30
Figure 4-2: Turnagain Project Relative to Traditional Territories of Kaska Dena & Tahltan Nation	31
Figure 4-3: Turnagain Project Area Relative to Land Management Areas	32
Figure 4-4: Turnagain Project Claims	33
Figure 5-1: Turnagain Project Location & Access	38
Figure 5-2: Turnagain River at Project Location & Airstrip (looking Northeast)	41
Figure 5-3: Hard Creek flowing into Turnagain River (looking Northwest)	42

Figure 5-4: Turnagain Project Area & Access (Transport Trucks on Boulder Trail, looking South)	45
Figure 5-5: Turnagain Project General Setting (Exploration Drill Hole, looking Northwest)	46
Figure 7-1: Regional Structural Setting – Turnagain Property	50
Figure 7-2: Property Geology	52
Figure 9-1: 2007 Geological Mapping	59
Figure 9-2: Map of Geochemical Sampling	61
Figure 9-3: Map of 2004 Airborne Electromagnetic Survey	62
Figure 10-1: Drill Hole Location Plan	64
Figure 11-1: Nickel Performance of Standard Reference Materials	83
Figure 11-2: Cobalt Performance of Standard Reference Materials	84
Figure 13-1: Nickel Speciation in 23 Samples Tested during 2019	90
Figure 13-2: Link between Primary Grind size & Nickel Recovery to Final Concentrate by Locked Cycle Test	93
Figure 13-3: Nickel Concentrate Grades & Recoveries per Cycle in the Talc 2-3 Super Cycle Test at BCR	95
Figure 13-4: Link between Sample S Assay & Ni as Ni(s) Assay as determined by Ammonium Citrate Method	97
Figure 13-5: Regression Analysis of Feed Sulphur Grade & Nickel Rougher Recovery from Five Variability Studies	99
Figure 13-6: Algorithms Fitting S Head Grade vs. Ni Rougher Recovery from the Five Variability Studies	100
Figure 13-7: Sulphur Grade vs. Nickel Recovery to Final Concentrate	101
Figure 13-8: Cobalt Recovery vs. Nickel Recovery	103
Figure 13-9: Relationship between Ni Grade & Fe/MgO Ratio	103
Figure 14-1: Plan View of Turnagain Drill Holes & Model Limits	108
Figure 14-2: Box Plot of Nickel Composites by Lithology	112
Figure 14-3: Box Plot of Cobalt Composites by Lithology	112
Figure 14-4: Box Plot of Sulphur Composites by Lithology	113
Figure 14-5: Box Plot of Nickel Composites for Dunite, Green Dunite, Wehrlite, Serpentinite	113
Figure 14-6: Box Plot of Cobalt Composites for Dunite, Green Dunite, Wehrlite, Serpentinite	114
Figure 14-7: Box Plot of Sulphur Composites for Dunite, Green Dunite, Wehrlite, Serpentinite	114
Figure 14-8: Box Plot of Nickel Composites by Lithology Unit	115
Figure 14-9: Box Plot of Cobalt Composites by Lithology Unit	115
Figure 14-10: Box Plot of Sulphur Composites by Lithology	116
Figure 14-11: Plot of Nickel-to-Sulphur Ratio vs. Nickel Grade by Lithology Unit	116
Figure 14-12: Plan View of Turnagain Deposit Geology Domains & Drill Holes	117
Figure 14-13: Assay Interval Lengths	118
Figure 14-14: Histogram of Nickel Composite Grades in Zones	119
Figure 14-15: Histogram of Cobalt Composite Grades in Zones	119
Figure 14-16: Histogram of Sulphur Composite Grades in Zones	120
Figure 14-17: Probability Plot of Nickel Composites within the Wh-Du-Sp Zone	122

Figure 14-18: Probability Plot of Nickel Composites within the Wh-Du-Sp Zone	122
Figure 14-19: Dimensions for the Turnagain Block Model.....	127
Figure 14-20: Origin & Orientation for the Turnagain Block Model.....	128
Figure 14-21: Plan View of Ni% Blocks & Drill Holes along with Surface Features and Turnagain River Location	134
Figure 14-22: Section View of Lithology Coded Blocks & Drill Holes for the Block Model.....	135
Figure 14-23: Section View of Ni% & Drill Holes for the Block Model	136
Figure 14-24: Section View of Classification of Blocks & Drill Holes.....	137
Figure 16-1: Horsetrail Scheduled Pit Shells – Plan View	142
Figure 16-2: Waste Disposal & Mineralisation Stockpile General Arrangement	143
Figure 16-3: Sensitivity of Contained In-Pit Resource & Respective Strip Ratios.....	147
Figure 16-4: Plan View of Updated Base Case Shell Outline compared to PEA Selected Planning Shells.....	149
Figure 16-5: Horsetrail & Ultimate Pit Shell Outlines with Reference Lines	150
Figure 16-6: Block Model MHV Values – Strike Section A Looking NE	150
Figure 16-7: Block Model Ni Values – Strike Section A Looking NE	151
Figure 16-8: Block Model S Values – Strike Section A Looking NE	151
Figure 16-9: Block Model MHV Values – Cross-section B Looking NW.....	152
Figure 16-10: Block Model MHV Values – Cross-section C Looking NW	152
Figure 16-11: Block Model MHV Values – Cross-section D Looking NW	153
Figure 16-12: Scheduled Ultimate Shell Grade & Tonnage Relationships.....	156
Figure 16-13: Horsetrail Pit with Mining Phases – Plan View.....	157
Figure 17-1: Process Flow Diagram – Crushing Circuit.....	166
Figure 17-2: Process Flow Diagram – Grinding Circuit.....	167
Figure 17-3: Process Flow Diagram – Flotation Circuit	168
Figure 18-1: Potential Access Road along North Side of Turnagain River.....	173
Figure 18-2: Final Waste Dump Footprint.....	174
Figure 18-3: TMF General Arrangement.....	176
Figure 18-4: TMF Starter Embankment	178
Figure 18-5: Plant Site Layout.....	184
Figure 18-6: Proposed Transmission Line	188
Figure 19-1: Consumption of Nickel in Stainless Steel by Nickel Product Type	192
Figure 19-2: Nickel Demand for Non-Stainless Steel Uses	192
Figure 19-3: Global Nickel Consumption by Region	193
Figure 19-4: Long-term Nickel Supply & Demand	194
Figure 19-5: Nickel Price Forecast.....	196
Figure 19-6: HPAL Incentive Price.....	196
Figure 19-7: Global Cobalt Supply/Demand Balance	198
Figure 19-8: Cobalt Price	199
Figure 19-9: Global Nickel Concentrate Treated & Net Required	200
Figure 20-1: Turnagain Project Relative to Traditional Territories of Kaska Dena & Tahltan ..	208
Figure 20-2: GHG Reduction Opportunity through Fleet Electrification (tCO ₂ e per year).....	214

Figure 22-1: Life-of-Mine Production Plan	227
Figure 22-2: Mill Processing Schedule.....	227
Figure 22-3: NPV Pre-Tax @ 8% Sensitivity	234
Figure 22-4: NPV After-Tax @ 8% Sensitivity	235
Figure 22-5: IRR Pre-Tax Sensitivity.....	236
Figure 22-6: IRR After-Tax Sensitivity.....	237
Figure 22-7: NPV Discount Rate Sensitivity.....	238

1.0 SUMMARY

1.1 Introduction

This report has been compiled by Hatch Ltd. (Hatch) for Giga Metals Corporation (Giga Metals) with input from the following independent consultants:

- Blue Coast Metallurgy Ltd. (Blue Coast)
- Kirkham Geosystems Ltd. (Kirkham)
- Kerr Wood Leidal Ltd. (KWL)
- Knight Piésold Ltd. (KP)
- Wood Mackenzie (WM)

The project is based on a 90,000 t/d capacity nickel-sulphide flotation plant that is scheduled to commence production at 50% capacity (45,000 t/d) and expand to full capacity after Year 5. The current mine life is 37 years.

This report is compliant with National Instrument 43-101 (NI 43-101) disclosure standards for mineral projects in Canada.

1.2 Project Location

The Turnagain Project is located in northern British Columbia (BC), Canada, 1,350 km northwest of Vancouver and 65 km east of the Township of Dease Lake. Current access is by paved road to Dease Lake and then light aircraft to site, landing at a coarse gravel strip adjacent to the exploration camp. A seasonal exploration trail provides vehicular access to the site; this trail will require significant upgrades to meet project requirements. Current power supply for the exploration camp is by diesel generators.

1.3 History

After the initial discovery of nickel and copper sulphides in the Turnagain River in 1956, Falconbridge Nickel Mines Ltd. (Falconbridge) acquired the property in 1966 and conducted various geophysical, geochemical and exploratory drilling programs up until 1973. Between 1973 and 1996, minimal exploration work was carried out and what was done focused more on platinum group elements (PGEs).

Bren-Mar Resources Ltd (Bren-Mar) optioned the property in 1996 and conducted further exploration work and some preliminary metallurgical testwork in the period 1996 to 1998, resuming exploration activities after the name change to Canadian Metals Exploration Limited (CME) in 2002.

In 2004 after a change of management, CME became Hard Creek Nickel Corporation (HNC) and from then until 2010, several exploration programs were conducted, including mapping, soil and

sediment sampling, geophysical surveys, metallurgical studies, diamond drilling, and environmental baseline studies. Until 2010, 79,351 m in 320 holes had been completed.

In 2017, after a period of relative dormancy, HNC changed its name to Giga Metals Corporation (Giga Metals), and in 2018 drilled 10,835 metres in 40 drill holes and restarted metallurgical and environmental baseline studies.

To date, 90,635 m in 362 holes have been completed.

The first resource estimate for the property was produced in 2003 by N.C. Carter. Several have since been produced by Ron Simpson of Geosim, including updates dated May 2009 and December 2011. For this report Garth Kirkham of Kirkham Geosystems has prepared an updated resource estimate current to the 2018 drilling year.

Four previous Preliminary Economic Assessments have been prepared for the property, two by AMEC of Americas Ltd. (AMEC) in 2006 and 2008; a third by Wardrop Engineering Inc. (Wardrop) in 2010; and a fourth by AMC Mining Consultants (Canada) Ltd. (AMC) in December 2011.

1.4 Geology & Mineralisation

The Turnagain ultramafic Alaskan-type complex comprises a central core of dunite with bounding units of wehrlite, olivine clinopyroxenite, clinopyroxenite, representing crystal cumulate sequences, hornblende clinopyroxenite, and hornblendite. The complex is elongate and broadly conformable to the northwesterly-trending regional structural grain.

The ultramafic rocks are generally fresh to mildly serpentinised; however, more intense serpentinisation and talc-carbonate alteration are common along faults and restricted zones within the complex. The central part of the ultramafic body is intruded by granodiorite to diorite, and hornblende–plagioclase porphyry dikes and sills.

The sulphide mineralisation, which is unusual for an Alaskan-type deposit, is thought to be associated with meta-sediment wall-rock inclusions which provided the sulphur source. The sulphides are mainly pentlandite and pyrrhotite with minor amounts of chalcopyrite and pyrite, and trace bornite. Anomalous levels of platinum and palladium are also present, however, they are not considered economic at this time.

1.5 Resource Estimate

The mineral resources were estimated in conformity with generally accepted Canadian Institute of Mining and Metallurgy's (CIM) "Estimation of Mineral Resources and Mineral Reserves Best Practices Guidelines" (December, 2019) and are reported in accordance with NI 43-101 guidelines.

The 362 drill holes in the database were supplied in electronic format by Giga Metals, 307 of which had assay values. For the purpose of the resource estimation, 240 drill holes are used which lie within the study area. The primary economic contributor is shown to be nickel (Ni%)

content, and the secondary is cobalt (Co%). Sulphur (S%) has similarly been analysed and estimated on a block-by-block basis. Assay values were composited to 4.0 m within the mineralised domains: (1) Du-Wh-Sp (dunite, wehrlite, serpentinite); (2) cPx-oPx (clinopyroxenite, olivine, magnetite and hornblende clinopyroxenite); (3) volcanics; (4) dykes; (5) overburden.

An evaluation of the probability plots for nickel and sulphur composites suggests that no outlier values could result in an overestimation of resources.

The chosen block size was 15 m x 15 m x 15 m, roughly reflecting the drill hole spacing which is spaced at approximately 50 m centres. The resource estimation plan includes the coding of lithological zones code in each block and the estimation of nickel, cobalt, and sulphur grades using ordinary kriging. The search criteria of the estimation process were the utilisation of a 150 m omni-directional ellipse, a minimum of four composites per block, maximum of 16 and a maximum of 4 composites per drill hole.

Mineral resources are classified under the categories of measured, indicated and inferred according to CIM guidelines. Mineral resource classification was based primarily on drill hole spacing and on continuity of mineralisation. Measured resources were defined at Turnagain as blocks with a distance to three drill holes of less than ~40 m to nearest composite and an average of 80 m and occurring within the estimation domains. Indicated resources were defined as those with a distance to three drill holes of less than ~60 m and an average distance of 100 m. Inferred resources were defined as those with an average drill hole spacing of less than ~150 m and meeting additional requirements. Final resource classification shells were manually constructed on sections.

This estimate is based upon the reasonable prospect of eventual economic extraction based on continuity of an optimized pit, using estimates of operating costs and price assumptions. The “reasonable prospects for eventual economic extraction” were tested using floating cone pit shells. The Horsetrail, Northwest, Hatzl and Duffy zones of the deposit are all included within the Horsetrail reasonable prospects pit shells. The pit optimization results are used solely for testing the “reasonable prospects for eventual economic extraction” and do not represent an attempt to estimate mineral reserves.

The Turnagain resource model includes the southern portions of the Horseshoe zone that abut and underlie the Turnagain River, and the Hatzl zone south of the river. These zones are potentially exploitable with a diversion of a relatively short section of the Turnagain River, which remains a potentially viable option. These zones are not included in the current mine plan, as the diversion of the river is not currently contemplated from a mining perspective within this PEA, however, it is still considered as a potential option eventually.

The differences between the previous resource estimate as described in a 2011 Preliminary Economic Assessment by AMC Consultants of Vancouver, BC is the inclusion of an additional 36 infill drill holes totalling 8,940 m drilled in 2018 in the areas of the conceptual open pit and updated geological modelling.

Using a cut-off grade of 0.1% Ni, the Turnagain property contains an estimated 1,073 Mt of measured and indicated resources at 0.220% Ni and 0.013% Co. An additional 1,142 Mt grading 0.217% Ni and 0.013% Co is classified as inferred. The resource estimate is presented in Table 1.1.

Table 1.1: Mineral Resource Estimate

Resource Category	Kilotonnes	% Ni (T)	% Co (T)
Measured	360,913	0.230	0.014
Indicated	712,406	0.215	0.013
Measured & Indicated	1,073,319	0.220	0.013
Inferred	1,142,101	0.217	0.013

Notes: **(1)** All mineral resources have been estimated in accordance with Canadian Institute of Mining and Metallurgy and Petroleum ("CIM") definitions, as required under National Instrument 43-101 ("NI 43-101"). **(2)** Mineral resources are reported in relation to a conceptual pit shell in order to demonstrate reasonable expectation of eventual economic extraction, as required under NI 43-101; mineralisation lying outside of these pit shells is not reported as a mineral resource. **Mineral resources are not mineral reserves and do not have demonstrated economic viability.** **(3)** Open pit mineral resources are reported at a cut-off grade of 0.1% Ni. Cut-off grades are based on a price of US \$7.50 per pound, nickel recoveries of 60%, mineralized material and waste mining costs of \$2.80, along with milling, processing and G&A costs of \$7.20. **(4)** Inferred mineral resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. However, it is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated. **(5)** Due to rounding, numbers presented may not add up precisely to the totals provided and percentages may not precisely reflect absolute figures.

1.6 Metallurgical Testing

Numerous phases of testing have been conducted on Turnagain samples over the past two decades. Earlier mineral processing work focused on developing a low-grade concentrate suitable for on-site hydrometallurgical processing; however, a breakthrough on concentrate cleaning in 2011 created an opportunity to make flotation concentrates for direct sale. Since then, work has focused on the production of high-grade nickel-sulphide concentrates. The initial work mostly used material drilled from the south end of the Horsetrail Zone, whereas more recent work has been conducted on samples from the Horsetrail and Northwest zones.

Samples from the Turnagain deposit have undergone extensive grindability testing (i.e., at least 77 Bond work index tests, 12 semi-autogenous grinding (SAG) mill comminution tests, 5 Bond rod mill work index tests, 5 abrasion tests and 5 crusher work index tests). In addition, piston press testing has been conducted to evaluate the response of the material to comminution by high-pressure grinding rolls (HPGRs).

Turnagain material is hard, with a mean Bond ball mill work index of 19.8 kWh/t, SAG milling Axb of 27.1 and Bond rod mill work index of 18.6 kWh/t. The SAG Axb hardness of the 15th percentile material is 23.0, which indicates the Turnagain material is highly resistant to SAG milling. This makes HPGR a favourable alternative comminution technology for the project.

Nickel occurs in both sulphide and non-sulphide form. More than 99% of the sulphide nickel is hosted in pentlandite, with pyrrhotite hosting less than 1% of the nickel. Non-sulphide nickel is mostly hosted in olivine and serpentine. There is considerable variability in nickel deportment

within pentlandite and in non-sulphide form; this is the primary driver behind nickel recovery to concentrate. The pentlandite grain size is also quite widely distributed. There is an appreciable content of fine-grained pentlandite that is only adequately liberated at grind sizes (P_{80}) of well below 100 μm .

The host rock is comprised of serpentine (median = 42%), olivine (29%) and clinopyroxene (12%). Talc was essentially absent from about 95% of the samples analysed, with the median content being 0.01%.

The flotation flowsheet adopted for this study includes primary grinding to 80% passing 85 μm , rougher flotation, and three or four stages of cleaner flotation. Residence times in rougher flotation and the first stage of cleaner flotation testing are 30 minutes and 15 minutes, respectively. Using an industry standard scale up factor of 2.2, the residence time in rougher flotation and the first stage of cleaner flotation used for plant design is 67, and 27 minutes, respectively. The use of reagents, including isopropyl xanthate collector (SIPX) (78 g/t), a dispersant (Calgon) (115 g/t) and methyl isobutyl carbinol (MIBC) frother (40 g/t), is conventional for nickel flotation. Dilute pulps have been shown to aid in the rejection of gangue in cleaning.

Although there is more pyrrhotite than pentlandite in the resource, pentlandite tends to float well, while pyrrhotite floats poorly, so good selectivity is achieved between pentlandite and pyrrhotite. This is a key reason why high-grade concentrates can be achieved. The other reason is the paucity of floatable gangue, so while Calgon is useful as a means of countering gangue interference in pentlandite flotation, gangue depressants are usually not needed.

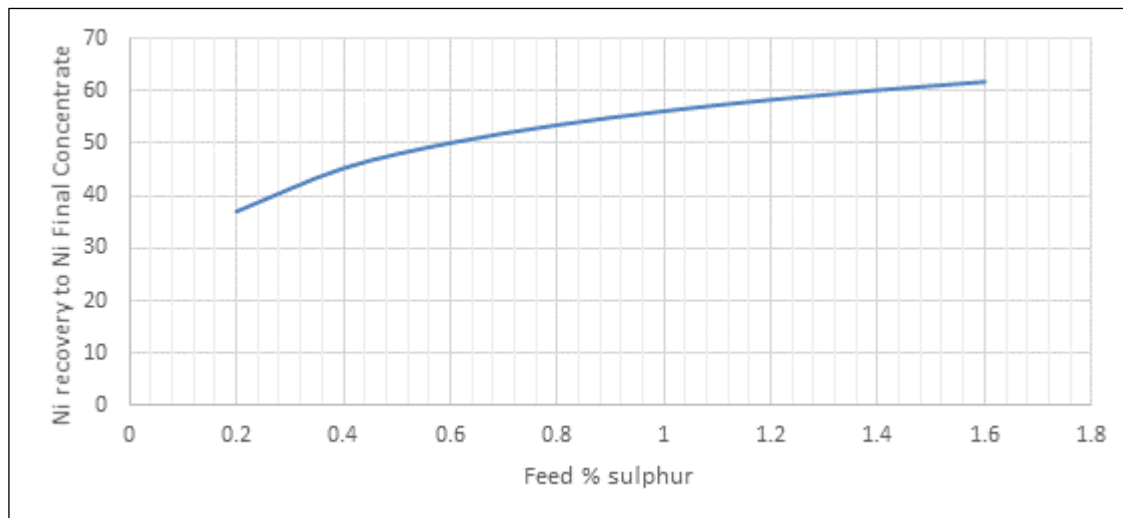
Numerous locked cycle tests have been conducted on Turnagain samples. Ten such tests that used slight variants of the optimum flowsheet yielded concentrate grades ranging from 15.3% to 21.4% nickel, averaging 19.3% nickel. Nickel recoveries have averaged 57.8%. On average, based on five multi-element analyses of locked cycle concentrates, the samples contained 1.2% cobalt, 2 g/t palladium, 1.2 g/t platinum, 32% iron and 4.4% magnesium.

Five different variability studies have been conducted on project samples since 2009. Each of these studies revealed a link between rougher nickel recovery and sulphur head grade, so these have been used to build a basic geometallurgical model for the project. Cleaner and locked cycle data have been used to convert rougher recoveries to expected recoveries to final concentrates, still as a function of sulphur head grade. This is shown in Figure 1-1.

Further work is required to refine the flowsheet. This includes investigating the use of regrinding in concentrate cleaning and determining how to tailor the production of concentrates for specific markets.

Additional work is also needed on lower sulphur-bearing samples. To date, development work has focused on samples assaying over 1.1% sulphur; however, the life-of-mine (LOM) sulphur grade is closer to 0.7%, so work is needed to confirm whether these materials can still be floated to produce premium grade nickel concentrates, and to explore if the drop in recovery with lower sulphur-bearing feeds can be better addressed (Figure 1-1).

Figure 1-1: Nickel Recovery to Concentrate as a Function of Sulphur Head Grade



Source: Blue Coast Metallurgy Ltd., 2020.

1.7 Recovery Methods

The process plant will consist of:

- one primary crusher followed by two trains of secondary crushing and HPGRs
- two grinding trains, each comprising two ball mills in series
- four banks of rougher flotation, utilising 630 m³ tank cells
- two parallel lines of three-stage cleaner circuits and concentrate filtration

This circuit lends itself to simple modification for the first five years at a lowered capacity, reducing to one comminution train and two rougher banks with appropriate modifications to the cleaner circuit.

1.8 Mining Methods

The Turnagain deposit will be mined using open pit mining methods, employing high volume trucks and shovels. The use of large mining equipment will achieve high mining rates and ensure the lowest possible mine operations unit costs. The waste and mineralised rock will require blasting and typical grade control methods using blast-hole sampling.

For the purpose of this study, the Horsetrail Pits are scheduled for a 37-year mine life. This includes the Horsetrail and Northwest mineralised zones, combined into one primary pit and a smaller pit located just outside the periphery to the northeast (Figure 1-2). Previous evaluations have indicated a potential open pit resource in the Hatzl Zone located on the east side of the Turnagain River, but this is not included in the scope of this study. The Turnagain River is fish-bearing and is considered a wildlife corridor. As such, any underlying mineralised material has been excluded.

The material contained and scheduled in the Horsetrail Pits is summarised in Table 1.2. These pits form the basis of the mine plan and production schedule in this study.

Table 1.2: Scheduled In-pit Material

Description	Mineralisation (kt)	Ni (%)	Co (%)	S (%)
Measured	249,200	0.23	0.01	0.80
Indicated	550,551	0.22	0.01	0.62
Measured & Indicated	799,751	0.220	0.013	0.68
Inferred	322,225	0.223	0.013	0.41
Total Stripping (kt)	207,880			
Total Strip Ratio (t:t)	0.19			

Notes: Includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

Figure 1-2 shows a plan view of the scheduled pit shells and basic general arrangement of mine infrastructure. The annual mill steady-state feed rate for the plant Phase 1, Years 1 through 5, is set at 45 kt/d (16.4 Mt/a) and for the balance of the mine life, Years 6 through 37, 90 kt/d (32.9 Mt/a). The resource will be processed for 37 years at these rates.

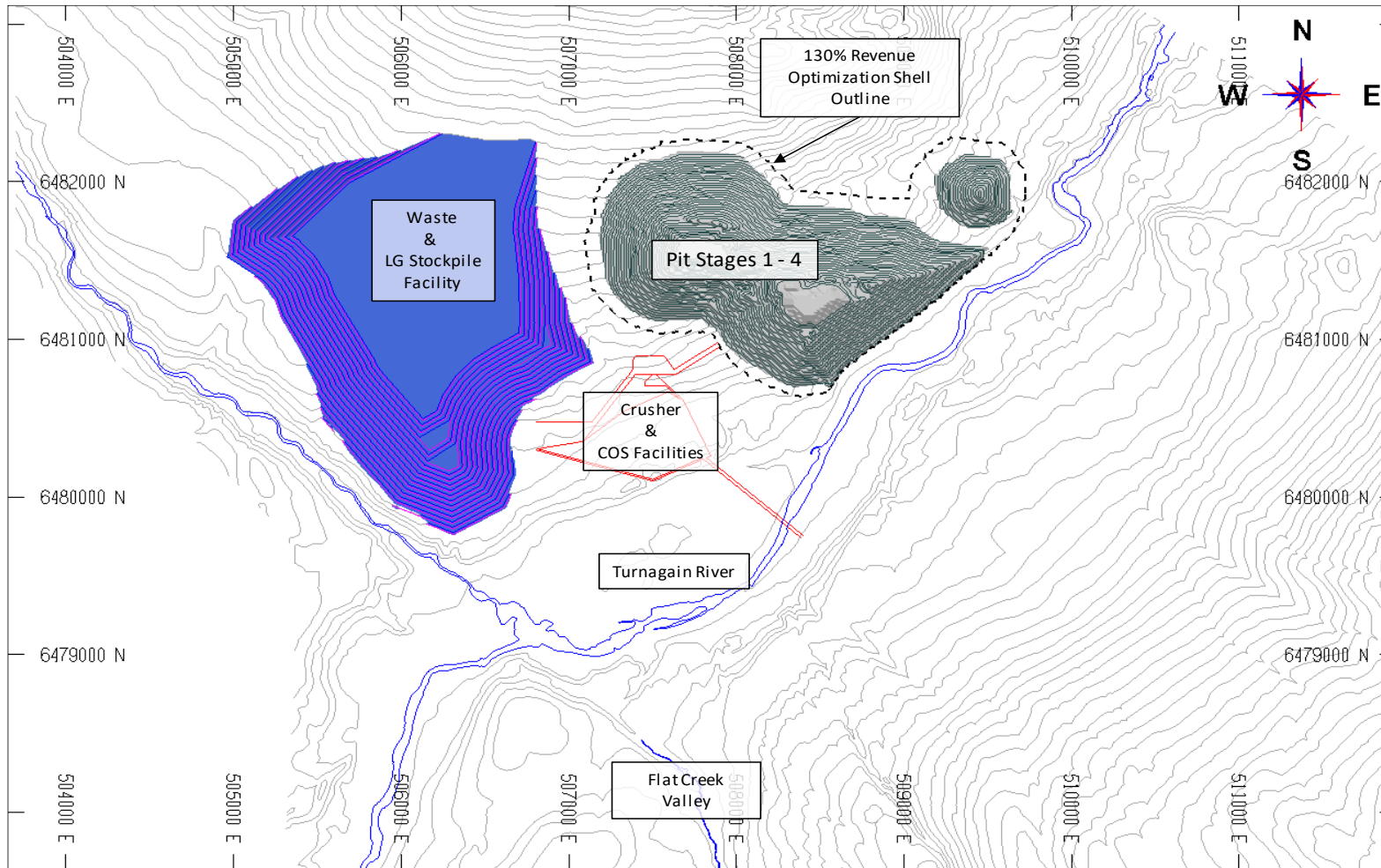
To access the most economic mineralisation in the early years and provide a smooth strip ratio throughout the life of mine, mineralisation production from the Horsetrail Pits is scheduled from five mining phases. Stage 1 will commence at the centre of the primary pit, where the highest mineralisation grade and lowest strip ratio will be encountered.

Elevated cut-off grades will be employed in the initial production and through most of the mining life to enhance the economics of the project. Mineralisation lower than the elevated cut-off grades will be sent to stockpile in a joint waste and low-grade (LG) stockpile facility to the west of the crusher and coarse ore storage (COS) facilities. Mineralisation below the high-grade (HG) cut-off but above the respective LG cut-offs will be stockpiled. Stockpiled material will be reclaimed at the end of the mine life or blended with the run-of-mine feed when the opportunity occurs.

Pit waste material will be hauled to the waste and LG facility. Current geochemistry data suggests that there is insignificant acid generating potential in the waste rock. Further studies will be undertaken to confirm that the waste rock will have minimum long-term environmental impact.

Figure 1-2 also shows the conceptual waste dumping and low-grade mineralisation stockpiling layout.

Figure 1-2: Horsetrail Pits & Mine Infrastructure General Arrangement



Source: Hatch, 2020.

1.9 Infrastructure

On-site and off-site infrastructure is required to support a fly-in, fly-out mining operation, as described in Section 18. The two largest infrastructure requirements are related to power supply and waste/tailings management.

1.9.1 Power Supply

Since the 2011 PEA, BC Hydro completed the Northwest Transmission Line (NTL) from Terrace to Bob Quinn. In addition, the NTL Extension was built to Tatogga Lake to provide power for the Red Chris Mine, and a 25 kV line was built to serve the community of Iskut. The plan for power supply is to connect the proposed Turnagain Mine to the BC Hydro system with a ~160 km long (powerline route) 287 kV powerline from the existing operating BC Hydro 287 kV substation at Tatogga Lake.

1.9.2 Waste / Tailings Management

The major proportion of the waste is expected to be non-reactive and will be stored in conventional sub-aerial dumps adjacent to the open pit.

From studies to date, the relatively small volume of potentially reactive waste is not expected to be acid generating, but could be neutral metal leaching. In any case, it will be encapsulated in the non-reactive waste—which is known to have high neutralisation potential—and appropriate water collection and control measures will be implemented as described in the next section.

Various tailings management options were assessed in previous studies. The preferred option in Flat Creek has been presented in this study, as it offers good storage efficiency in terms of the ratio of capacity to embankment volume and has a relatively small catchment area.

Construction of the tailings management facility will commence with an initial starter dam to provide up to three years storage at the initial production rate of approximately 45,000 t/d and will be raised in stages using centreline construction throughout the approximately 37-year mine life. The tailings facility staging will accommodate the production rate increase to approximately 90,000 t/d in Year 6.

1.10 Environmental Considerations

The project is expected to be subject to both provincial and federal reviews of an environment impact assessment (EIA), which should be conducted in one review process through a substitution agreement between the provincial and federal agencies. This process will involve consultations with the public and First Nations, as well as detailed studies of baseline environmental settings and an assessment of potential project impacts. Once the EIA review is successfully completed, a number of environmental conditions stipulating preventive and mitigative measures will be mandated before allowing the project to proceed.

Baseline environmental studies to support the EIA process were initiated in 2004 and are ongoing. Additional studies will include air quality, background noise levels, vegetation, wildlife, soil quality, groundwater, and archaeology, with special emphasis on aquatic habitat and aquatic life, particularly in Flat Creek.

Water and waste management measures will be directed towards achieving the following key objectives:

- adequate storage and containment in the tailings management facility (TMF) of process tailings, process water and storm runoff
- interception and diversion of clean waters to the extent possible
- collection and control of mine-affected waters including appropriate waste dump and low-grade stockpile design with collection ponds and re-use and/or treatment of these runoff waters
- optimisation of the storage and usage of water over the entire site with regard to environmental, operational and economic criteria

Based on the diesel and electricity consumption for mining and processing activities, the carbon intensity for the operations is estimated to average 74,428 tCO₂e per year; this decreases to 23,080 tCO₂e per year if an electrified fleet is used. The average project carbon intensity is estimated to 2.24 tCO₂e/t Ni for the base case and 0.69 tCO₂e/t Ni for the electrified case. Giga Metals continues to support research into mineral carbonation by the host rock of the Turnagain deposit, with an ultimate goal of better defining the quantity of CO₂ that can be sequestered and optimal tailings management strategies.

The project is located within the traditional territories of the Tahltan Nation and the Kaska Dena. Giga Metals has established positive engagements with the Tahltan Central Government and Kaska Dena Council via its member nation, Dease River First Nation, and will continue these respectful and ongoing engagements. Giga Metals will seek First Nations participation in ongoing baseline studies, the environmental assessment, and development of environmental and social mitigation and management plans. Giga Metals will also work in partnership with First Nations to optimise employment, training, and procurement opportunities through the project life cycle.

The reclamation and closure plan will minimise any adverse environmental and social impacts associated with the mine development and seek to return disturbed site areas to conditions consistent with an approved end-use plan. Preliminary closure planning will be carried out concurrently with the various stages of project development and design in order to integrate the post-closure objectives into the design, construction, and operation of all mine infrastructure and facilities. The closure and reclamation plan will be developed in consultation with the Giga Metals project team, local stakeholders, and the appropriate regulatory authorities.

1.11 Capital & Operating Costs

The mine initial, expansion, and sustaining capital costs were estimated for the mine from the mine schedule and fleet requirements. For the processing plant, major equipment items were budget priced and a factored initial and expansion capital cost estimate was prepared. Sustaining capital was also factored. Infrastructure elements were taken from recent similar projects. As a check, the capital cost estimates were benchmarked against similar projects.

Knight Piésold provided TMF, site-wide surface water management, and reclamation/closure costs. Off-site electrical powerline costs were provided by Kerr Wood Leidal.

Project capital costs are summarised in Table 1.3.

Table 1.3: Project Initial/Expansion Capital Cost Summary

Item	Units	Phase 1	Phase 2	Life of Mine
Mine Directs	US\$M	133	45	178
Process Plant Directs	US\$M	307	245	551
Tailings Storage Facility Directs	US\$M	87	20	107
On-site Infrastructure Directs	US\$M	77	-	77
Indirects	US\$M	204	104	308
Contingency	US\$M	191	99	290
Owner's Cost & EA	US\$M	63	20	83
Electrical Supply	US\$M	278	-	278
Site Access Road	US\$M	42	-	42
Total Initial/Expansion Capital	US\$M	1,381	532	1,913

Project sustaining capital costs, as well as closure and reclamation costs, are summarised in Table 1.4.

Table 1.4: Project Sustaining Capital & Closure & Reclamation Cost Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mine	US\$M	0	348	148	496
Process Plant	US\$M	31	165	187	384
Tailings Storage Facility	US\$M	107	377	335	819
On-site Infrastructure	US\$M	8	23	26	57
Electrical Supply (Tariff Supplement 37)	US\$M	90	82	-	172
Total Sustaining Capital	US\$M	236	996	697	1,928
Closure & Reclamation	US\$M	38	15	18	72
Total	US\$M	274	1,011	715*	2,000

Note: * Includes \$2.8 M in TMF and closure costs in Year 38.

The overall operating costs are summarised in unit cost terms in Table 1.5.

Table 1.5: Unit Operating Cost Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mining	US\$/t milled	3.52	2.89	2.46	2.72
Processing & Site Infrastructure	US\$/t milled	4.90	4.39	4.38	4.42
G&A	US\$/t milled	1.13	0.68	0.68	0.71
Electrical Supply O&M	US\$/t milled	0.08	0.04	0.04	0.04
Total	US\$/t milled	9.63	7.99	7.56	7.89

1.12 Economic Evaluation

The preliminary economic assessment is preliminary in nature. It includes inferred mineral resources that are too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that the preliminary economic assessment will be realised.

The PEA base case is based on the long-term nickel and cobalt prices provided by Wood Mackenzie, US\$7.50/lb Ni and US\$22.30/lb Co, and does not achieve a positive NPV at an 8% discount rate. The returns are shown in Table 1.6.

Table 1.6: Returns Summary

Item	Unit	PEA Base Case: Wood Mackenzie Long-Term Price US\$7.50/lb Ni
Pre-Tax NPV @ 8%	US\$M	(269)
Pre-Tax IRR	%	6.3%
Pre-Tax Payback	years	13.7
After-Tax NPV @ 8%	US\$M	(443)
After-Tax IRR	%	4.9%
After-Tax Payback	years	14.8
Nickel Price	US\$/lb	7.50
Cobalt Price	US\$/lb	22.30
Exchange Rate	USD/CAD	0.77

*Inverse of 1.30 CAD/USD applied.

The nickel price applied is the long-term average forecast by Wood Mackenzie. The PEA base case economic outputs are summarised in Table 1.7.

Table 1.7: PEA Base Case Key Economic Outputs

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	LOM
Project Economics					
NPV@ 8% Before Tax	US\$M	-	-	-	(269)
NPV@ 8% After Tax	US\$M	-	-	-	(443)
IRR Before Tax	%	-	-	-	6.3%
IRR After Tax	%	-	-	-	4.9%
Payback Period Before Tax	years	-	-	-	13.7
Payback Period After Tax	years	-	-	-	14.8
Market Drivers					
Nickel Price	US\$/lb	7.50	7.50	7.50	7.50
Cobalt Price	US\$/lb	22.30	22.30	22.30	22.30
Exchange Rate	USD/CAD	0.77	0.77	0.77	0.77
Nickel Payable %	%	78%	78%	78%	78%
Cobalt Payable %	%	35%	35%	35%	35%
Physicals					
Effective Strip Ratio (incl. stockpile)	t:t	0.50	0.56	0.24	0.40
Mill Throughput: Annual Average	Mt/a	15.3	32.7	32.6	30.3
Nickel Head Grade	%	0.260%	0.220%	0.216%	0.221%
Cobalt Head Grade	%	0.016%	0.013%	0.013%	0.013%
Recovery: Nickel and Cobalt	%	57.3%	51.6%	46.5%	49.6%
Nickel Recovered	kt	114	557	558	1,229
Cobalt Recovered	kt	7	33	32	73
Financial					
Revenue	US\$M/a	317	517	456	462
Mining Cost	US\$/t milled	3.52	2.89	2.46	2.72
Processing and Site infrastructure	US\$/t milled	4.90	4.39	4.38	4.42
G&A	US\$/t milled	1.13	0.68	0.68	0.71
Electrical Supply O&M	US\$/t milled	0.08	0.04	0.04	0.04
Site Operating Costs	US\$/t milled	9.63	7.99	7.56	7.89
Site Operating Costs	US\$/lb Ni recovered	2.93	3.20	3.41	3.27
Concentrate Shipping	US\$/lb Ni recovered	0.31	0.31	0.31	0.31
Cobalt Credit	US\$/lb Ni recovered	(0.47)	(0.47)	(0.45)	(0.46)
Net Operating Cost	US\$/lb Ni recovered	2.77	3.04	3.27	3.12
Construction Capital Cost	US\$M	1,381	532	-	1,913
Sustaining Capital & Closure Cost	US\$M	274	1,011	715	2,000

1.13 Conclusions & Recommendations

The key elements in this update are additional resource drilling and metallurgical work, the future potential of non-stainless steel demand, and the increased certainty of power supply to northern British Columbia.

Based on an updated resource estimate and the metallurgical recovery models resulting from the testwork, a production schedule base case has been developed with an elevated cut-off grade strategy and a phased approach to capacity to deliver a 37-year mine life. The processing route is a conventional comminution and flotation plant.

Opportunities exist to prove up additional resources, including those containing anomalous levels of platinum and palladium, and to further enhance the geometallurgical knowledge base and metallurgical efficiencies, although a concomitant risk is that the geometallurgical variability may prove greater than expected. There is also an opportunity for full mine-to-product (including tailings) project optimisation as better information becomes available in the next phase of study.

This PEA indicates the Turnagain property generates an internal rate of return below the applied discount rate on the estimated N.I. 43-101 compliant resource at base case scenario modelling parameters. The project economics could improve with the opportunities noted in Section 25.8. It is recommended that Giga Metals carry the project forward to the pre-feasibility stage in accordance with the budget in Table 1.8. Recommendations by study area for the next phase are summarized in Section 26.

Table 1.8: Pre-feasibility & Early Environmental Works Study Budget (now to mid-2022)

Item	US\$000s
Coordinating-Design Engineer	1,280
Power Studies	240
Marketing Studies	80
Metallurgical Development	600
Geotechnical	1,200
CO ₂ Sequestration	80
ARD/ML	160
Tailings	200
Environment	1,720
Community Program	160
Resource/Reserve Program	3,040
Government Bonding for works	160
Field Support Costs	520
Total PFS & Early Environmental Studies	9,440
Total All Activities	12,440

2.0 INTRODUCTION

This Preliminary Economic Assessment (PEA) report has been prepared by Hatch as an update to the previous PEA prepared by AMC in December 2011. The principal reasons for this update are to include the results of additional drilling, resource modelling and metallurgical testwork and updating cost, revenues and economics for 2020.

The following independent consultants have contributed to this report:

- Hatch
- Kirkham Geosystems Ltd.
- Knight Piésold Ltd. (KP)
- Kerr Wood Leidal (KWL)
- Blue Coast Metallurgy Ltd.
- Wood Mackenzie (WM)

Site visits are shown in Table 2.1.

A list of the qualified persons (QPs) responsible for each section of this report is provided in Table 2.1, and their QP certificates are appended to the back of this report.

All the qualified persons listed in Table 2.1 are independent of Giga Metals.

Table 2.1: Persons Who Prepared or Contributed to this Technical Report

Qualified Person	Employer	Date of Site Visit	Sections of Report
Ian Thompson, P.Eng.	Hatch	October 9 to10, 2018	1.1, 1.2, 1.3, 1.8, 1.9, 1.11, 1.12, 1.13, 2, 3, 4.4, 5.1, 5.4, 15, 16, 18.3, 21 (except for 21.1.2, 21.1.3.1, 21.1.4, 21.2.3, 21.2.6), 22, 24, 25.2, 25.7, 25.8.1.2, 25.8.2.2, 26.1, 26.3 and 27
Persio Rosario, P.Eng.	Hatch		1.7, 17, 21.1.2, 21.2.3, 25.4, 25.8.1.3, 25.8.2.4, 26.5
Evan Jones, P.Eng.	Hatch		1.10, 4.3, 5.2, 5.3, 5.6, 20, 25.8.1.5, 25.8.2.7 and 26.8
Gerald (Gerry) Schwab, P.Eng.	Hatch		5.5, 18,1, 18.5.5, 18.5.6, 18.5.7, 18.6, 18.7, 18.9, 18.10, 25.8.1.4, 25.8.2.5 and 26.6
Garth Kirkham, P.Geo.	Kirkham Geosystems	October 9 to10, 2018	1.4, 1.5, 4.1, 4.2, 6, 7, 8, 9, 10, 11, 12, 14, 23, 25.1, 25.8.1.1, 25.8.2.1 and 26.2
Daniel Friedman, P.Eng.	Knight Piésold Ltd.	September 7, 2005 and June 16, 2009	1.9.2, 18.2, 18.4, 18.5.1, 18.5.2, 18.5.3, 18.5.4, 21.1.4, 21.2.6 and 25.5
Ron Monk, P.Eng.	Kerr Wood Leidal		1.9.1, 18.8, 21.1.3.1, 25.6, 25.8.2.6 and 26.7
Chris Martin, C.Eng., MIMMM	Blue Coast Metallurgy		1.6,13, 25.3, 25.8.2.3 and 26.4
Andrew Mitchell, PhD, C.Eng.	Wood Mackenzie		19

3.0 RELIANCE ON OTHER EXPERTS

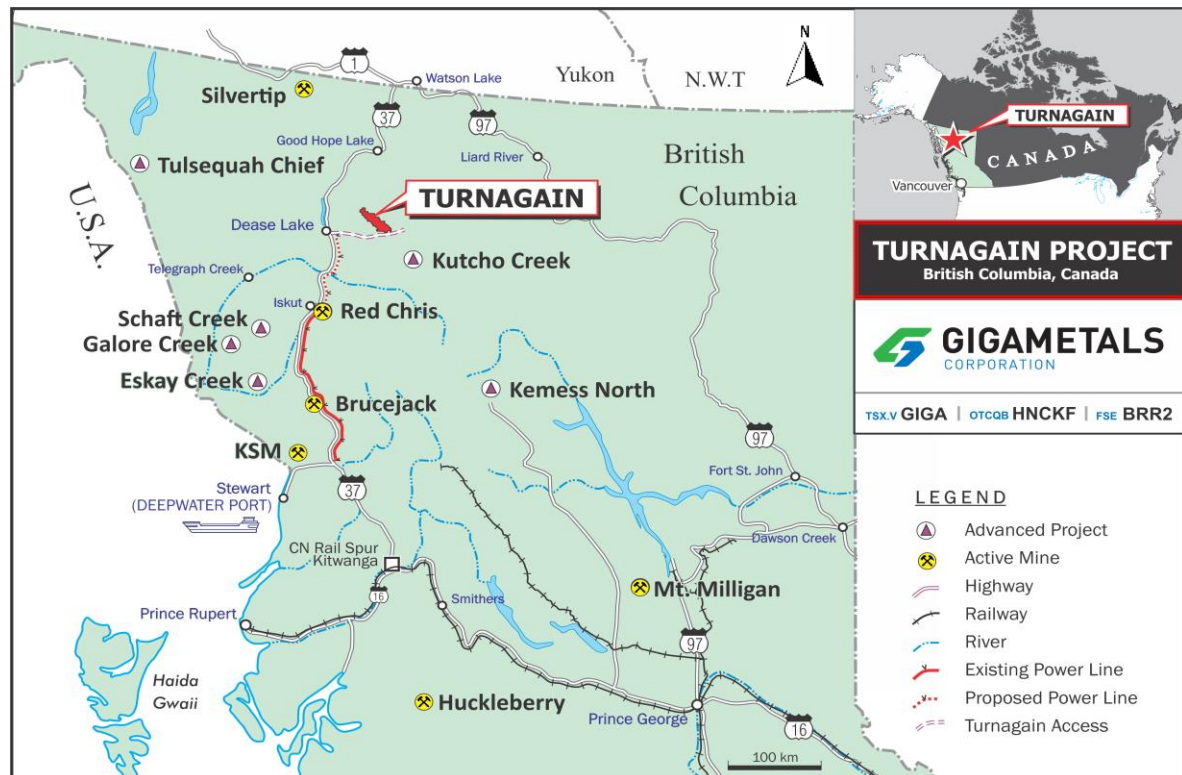
Not applicable.

4.0 PROPERTY DESCRIPTION & LOCATION

4.1 Location

The project is located approximately 65 km east of Dease Lake in the Liard Mining Division of northwestern British Columbia (Figure 4-1). The deposit is approximately centred at UTM NAD83 Zone 9 coordinates 508,000 m E and 6,481,000 m N (58°28'10"N latitude and 128°51'46"W longitude). In the central claims, elevations range from about 1,000 metres above sea level (masl) along the Turnagain River to 1,800 masl at an unnamed summit in the central property area. The property is accessible via a 900 m gravel airstrip and a seasonal exploration trail from Highway 37, which is suitable for off-highway vehicle use during summer months.

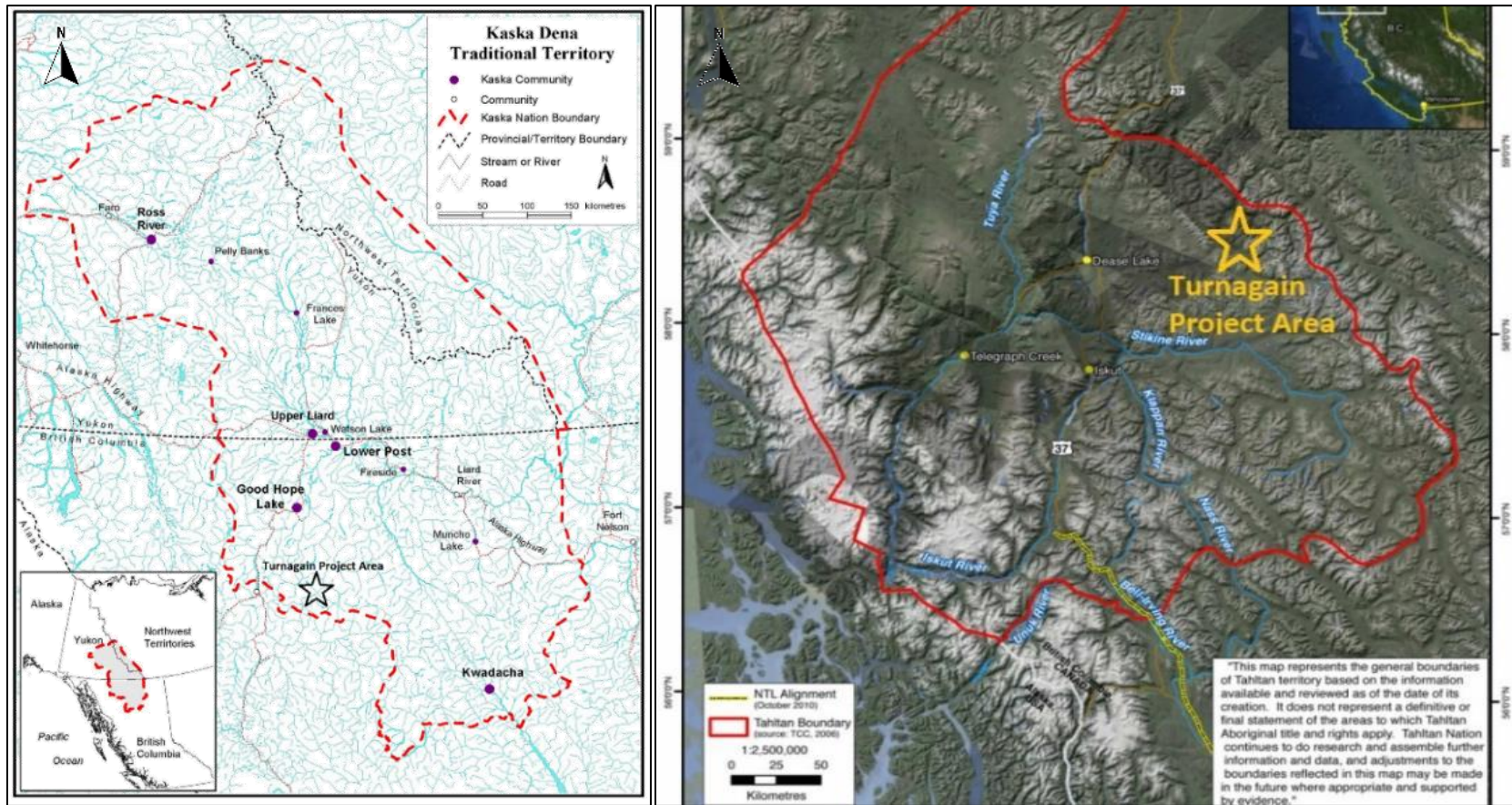
Figure 4-1: Turnagain Project Location Overview Map



Source: Giga Metals, 2020.

The closest community to the project is the community of Dease Lake (unincorporated), which is a town of approximately 335 people (BC Census Data, 2016) located on Highway 37 at the south end of Dease Lake. Other local communities include Telegraph Creek, Iskut, and Good Hope Lake. There are no residences near the mine site. The property lies within the traditional territorial claims of the both the Tahltan Nation and Kaska Dena (Figure 4-2).

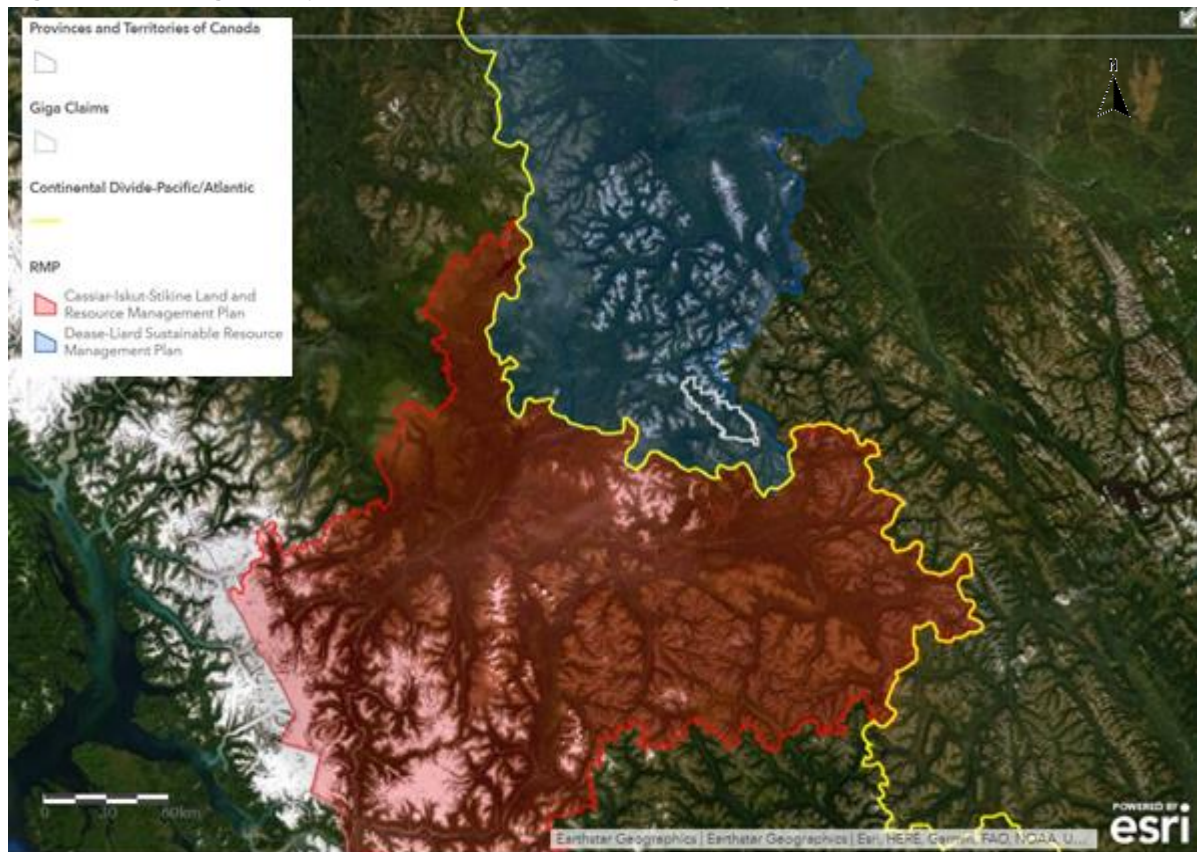
Figure 4-2: Turnagain Project Relative to Traditional Territories of Kaska Dena & Tahltan Nation



Source: Giga Metals, 2020.

The project is located within the Liard River watershed on the Arctic side of the Pacific-Arctic continental divide (yellow line), as shown in Figure 4-3.

Figure 4-3: Turnagain Project Area Relative to Land Management Areas



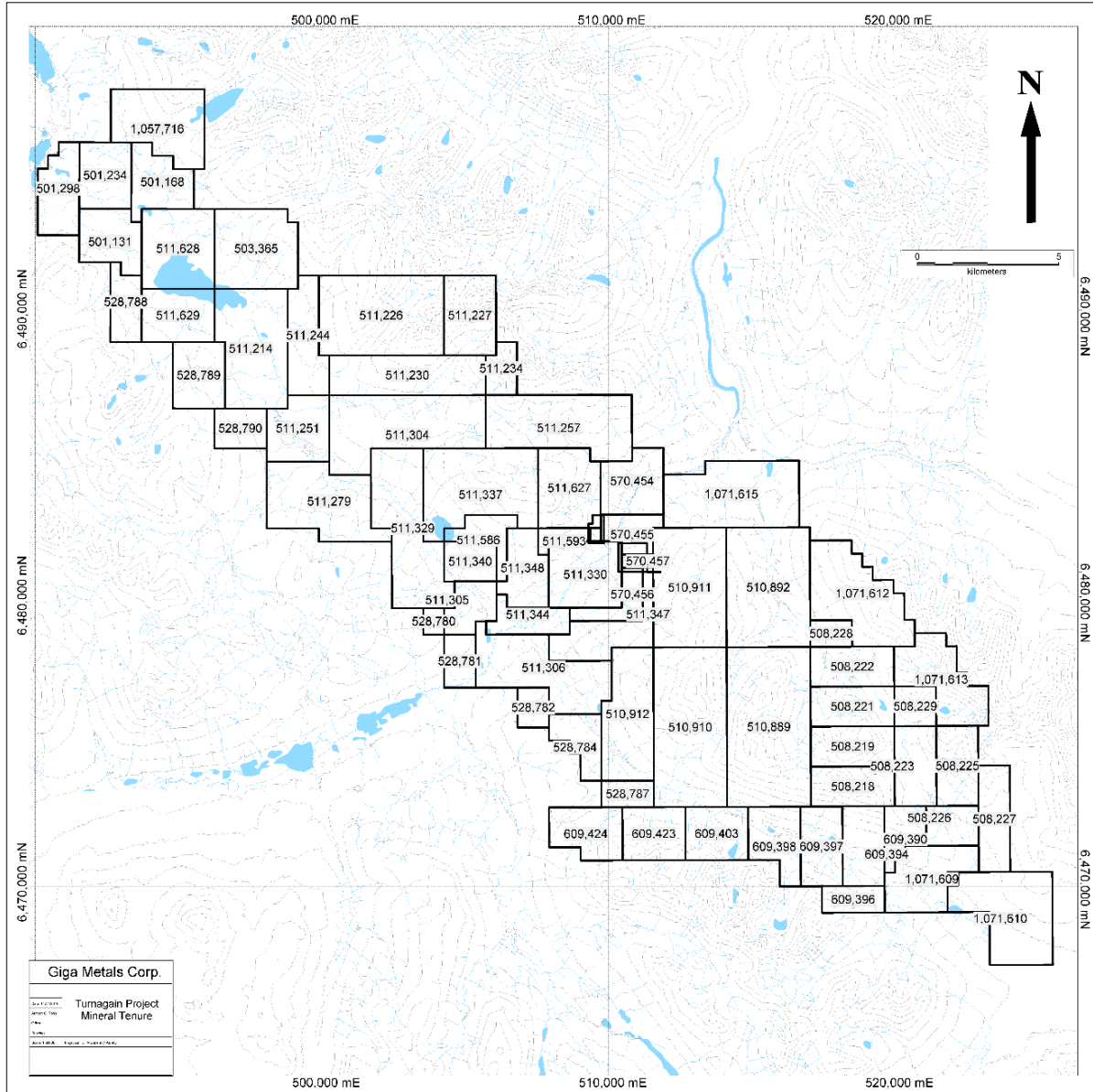
Source: Giga Metals, 2020.

The Turnagain property is found within the Dease-Liard Sustainable Resource Management Plan (BC MSRM 2004, 2012), while the access trail also passes through the Cassiar Iskut-Stikine Land and Resource Management Plan (LRMP) (BC MSRM 2000).

4.2 Mineral Claims

The Turnagain Project is wholly owned by Giga Metals and consists of 71 mineral claims covering an area of approximately 38,000 ha (Figure 4-4). All claims are contiguous and occur within the BC Liard Mining Division in the Stikine region of northwest BC. The configuration of the various mineral claims is illustrated in Figure 4-4, which incorporates information plotted on BC Mineral Titles Reference Maps M104I-036 to -38, -045 to -047, -055 to -057, and 065. Details are listed in Table 4.1.

Figure 4-4: Turnagain Project Claims



Source: Giga Metals, 2020.

Table 4.1: Mineral Claim Details

Tenure Number	Claim Name	Original Legacy Name(s)	Tenure Type	Good to Date	Area /ha
407627	PUP 4		Mineral	Dec-01-2029	500
501131	Drift 1		Mineral	May-01-2027	422
501168	Drift 2		Mineral	May-01-2027	421.8
501234	Drift 3		Mineral	May-01-2027	421.7
501298	Drift 4		Mineral	May-01-2027	421.8
503365		Hard 2	Mineral	May-01-2027	793.3
508218	Dinah 1		Mineral	May-01-2027	407.2
508219	Dinah 2		Mineral	May-01-2027	407.1
508221	Dinah 3		Mineral	May-01-2027	406.9
508222	Dinah 4		Mineral	May-01-2027	406.7
508223	Dinah 5		Mineral	May-01-2027	407.1
508225	Dinah 6		Mineral	May-01-2027	407.1
508226	Dinah 7		Mineral	May-01-2027	254.6
508227	Dinah 8		Mineral	May-01-2027	407.3
508228	Dinah 9		Mineral	May-01-2027	135.5
508229	Dinah 10		Mineral	May-01-2027	203.4
510889		Flat 10, 13, 15	Mineral	May-01-2027	1627.9
510892		Flat 2, 6	Mineral	Dec-01-2029	1219.3
510910		Flat 9, 12, 14	Mineral	Dec-01-2028	1424.3
510911		Flat 1, 5	Mineral	Dec-01-2029	1066.9
510912		Flat 8, 11	Mineral	May-01-2027	779.9
511214		Hard 4, 6	Mineral	May-01-2027	979.9
511226		Hill 1, 2	Mineral	May-01-2027	1216.1
511227		Hill 3	Mineral	May-01-2027	506.7
511230		Hill 4, 5	Mineral	May-01-2027	760.5
511234		Hill 6	Mineral	May-01-2027	185.9
511244		Hard 5, 7	Mineral	May-01-2027	489.9
511251		Hard 8	Mineral	May-01-2027	473.4
511257		Hill 9, 10	Mineral	Dec-01-2029	1014.4
511279		Hard 9, 10	Mineral	Dec-01-2029	896.7
511304		Hill 7, 8	Mineral	Sep-01-2029	1149.7
511305		Hound 3	Mineral	Dec-01-2029	271
511306		Turn 2, Flat 7	Mineral	Dec-01-2029	881.2
511329		Hound 1, 2	Mineral	Feb-01-2029	1015.4
511330		Cub	Mineral	Oct-01-2029	592.6
511337		Cub 10, 18, Pup 1	Mineral	Oct-01-2029	1065.8
511340		Cub 17	Mineral	Dec-01-2029	253.9
511344		Turn 1, Bear 2	Mineral	Dec-01-2029	271
511347		Flat 3, 4	Mineral	Dec-01-2029	474.3
511348		Cub 2	Mineral	Oct-01-2029	389.4
511586		Pup 2	Mineral	Dec-01-2029	236.9
511593		Pup 3	Mineral	Oct-01-2029	101.5
511627		Cub 11	Mineral	Dec-01-2029	592.1

Tenure Number	Claim Name	Original Legacy Name(s)	Tenure Type	Good to Date	Area /ha
511628		Hard 1	Mineral	May-01-2027	709
511629		Hard 3	Mineral	May-01-2027	472.9
528780	T1		Mineral	Dec-01-2028	67.7
528781	T2		Mineral	Dec-01-2028	203.3
528782	T3		Mineral	May-01-2028	152.6
528784	T4		Mineral	May-01-2028	288.3
528787	T5		Mineral	May-01-2027	169.6
528788	T6		Mineral	May-01-2027	270.2
528789	T7		Mineral	May-01-2027	422.5
528790	T8		Mineral	May-01-2028	253.6
570454		Bear 1	Mineral	Dec-01-2029	456.8
570455		Bear 19, Bear 21 to 28	Mineral	Dec-01-2029	237
570456		Bear 3 to 18	Mineral	Dec-01-2029	220.2
570457		Bear 20	Mineral	Dec-01-2029	16.9
609390	FLAT 7		Mineral	May-01-2027	254.6
609394	FLAT 6		Mineral	May-01-2027	407.4
609396	FLAT 8		Mineral	May-01-2027	203.8
609397	FLAT 5		Mineral	May-01-2027	407.4
609398	FLAT 4		Mineral	May-01-2027	407.4
609403	FLAT 3		Mineral	May-01-2027	407.3
609423	FLAT 2		Mineral	May-01-2027	407.3
609424	FLAT 1		Mineral	May-01-2027	424.2
1057716	NWMAG		Mineral	Aug-01-2023	741.9
1071609	BLICK 1		Mineral	Oct-04-2020	560.3
1071610	BLICK 2		Mineral	Oct-04-2020	900.1
1071612	FAULKNER 1		Mineral	Oct-04-2020	897.5
1071613	FAULKNER 2		Mineral	Oct-04-2020	627
1071615	FAULKNER 3		Mineral	Oct-04-2020	1032.1

Mineral claims staked in 1996 by J. Schussler and E. Hatzl were subsequently optioned to Bren-Mar Resources Ltd. (Bren-Mar), a predecessor company of Canadian Metals Exploration Ltd. (CME), Hard Creek Nickel Corp. (HNC) and Giga Metals. The original option agreement gave Bren-Mar the right to earn a 100% interest in the mineral claims in exchange for 200,000 shares and incurring property expenditures of C\$1 M within five years of acquisition. The 100% interest was earned subject to a 4% net smelter royalty (NSR) on possible future production from the mineral claim 511330. Giga Metals retains the right to purchase all or part of this royalty for C\$1 M for each 1% of the royalty.

On November 28, 2002, HNC entered into an agreement with Schussler and Hatzl to acquire an additional 34 mineral claims adjacent to the Turnagain property in exchange for an aggregate of 100,000 common shares.

Between November 2003 and October 2019, additional claims were staked at various times, some of which were subsequently forfeited by way of the BC Ministry of Energy and Mines online map selection process, enlarging the Turnagain property to its current configuration of 71 claims covering approximately 38,000 ha.

Twenty-nine of the original four-post mineral claims (now termed legacy claims) northwest of the Turnagain River were converted to cell mineral claims in April 2006. This conversion process ensured greater security of mineral title by effectively eliminating the possibility of internal and external fractions within or adjacent to the various mineral claims. Accumulated assessment work credits were also retained under the conversion system.

One four-post claim and 27 two-post claims located adjacent to and partially within the central part of the property holdings (but outside of the prospective ultramafic rocks) were the subject of a legal dispute between HNC and Mr. Weise. On July 10, 2006, the Supreme Court of British Columbia ordered that these claims be transferred to HNC. The transfer has been completed and the claims have been included in the Turnagain property. Mr. Weise subsequently filed a Notice of Appeal of the Order; the appeal was dismissed by the British Columbia Court of Appeal on April 30, 2007. All subsequent claim acquisitions for various exploration and access considerations were made using BC Ministry of Energy and Mines online map selection process. Most recently, in 2019, five additional claims contiguous with the Turnagain Property totalling 4,017 ha were staked in the southeastern portion of the project area in the Blick and Faulkner creek valleys.

4.3 Permits & Environmental Liabilities

Exploration work on mineral properties in BC requires a Notice of Work and Reclamation to be filed with the Ministry of Energy and Mines. Obtaining a permit to facilitate such work may require a reclamation security to be posted. The value of Giga Metals' Turnagain Project reclamation security is C\$232,000, although this could be amended.

The project will require several permits, approvals, and authorisations from provincial and federal agencies, which are summarised in Section 20.

Environmental studies within the property area have been ongoing since 2003. These studies include hydrological measurements on tributary creeks, water quality sampling from creeks and drill holes, wildlife observations and determination of fish species, and the collection of meteorological site data. Multi-element analyses of soil samples have provided useful information regarding background concentrations of major and trace elements. The meteorological station was moved and upgraded in 2009 and further upgraded in-place in 2018 and 2019.

There is no knowledge of any specific environmental liabilities to which the various mineral claims are subject. The Turnagain property is situated in an area where mining-related activities have been underway for more than 75 years.

4.4 Royalties

A 4% NSR on possible future production from one mineral claim (511330) is held by the original property vendors J. Schussler and E. Hatzl. Giga Metals retains the right to purchase all or part of this royalty for C\$1 million per each 1% of the royalty.

A 2% NSR on all future metal production is held by Conic Metals Corp. Giga Metals has a one-time option to repurchase 0.5% of the 2% royalty for US\$20 million prior to the 5th anniversary of the NSR Agreement (i.e., July 12, 2023), which would leave Conic with a 1.5% NSR. Conic will have a right of first refusal on any future sale by Giga Metals of a royalty or product stream or similar instrument.

5.0 ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE & PHYSIOGRAPHY

5.1 Accessibility

The nearest airport to the project is at Dease Lake, 65 km by air to the west of the project. Dease Lake has scheduled airline service by Northern Thunderbird Air. Flight frequency generally depends on the prevailing demand and economic conditions. Fixed-wing charter flights are also available from Whitehorse (430 km northwest), Terrace and Smithers (440 km south and 425 km south-southeast, respectively), and Prince George (630 km southeast).

A 900 m coarse gravel airstrip immediately adjacent to the Turnagain exploration camp, constructed by Falconbridge in 1967, was upgraded by HNC in 2007 and has been used regularly as recently as summer 2019.

An exploration trail, known as the Boulder Trail, extending east from Highway 37 8 km south of Dease Lake has been used by large, articulated four- and six-wheel drive vehicles to convey equipment to mining and exploration operations in the region. The length of Boulder Trail plus 5 km spur to the Turnagain Camp is approximately 78 km, for a total distance from Dease Lake of 86 km. (Figure 5-1).

Figure 5-1: Turnagain Project Location & Access



Source: Giga Metals, 2020.

Trail access is not suitable for regular vehicle traffic. The Boulder Trail is also the primary access trunk to the Boulder City placer camp (10 km southwest), Kutcho Copper (40 km southeast) and

District Copper (immediately west) properties, as well as several jade operations in the vicinity. The BC government has recently convened a multi-stakeholder group to work together on Boulder Trail permitting, maintenance, and upgrades.

5.2 Climate

The climate of the area is generally characterised by cold winters, warm summers, and reasonably consistent precipitation throughout the year, although the summer months are the wettest. The nearest Government of Canada weather station is located at Dease Lake.

Climate monitoring commenced with the installation of the TURNMET climate station, a Campbell Scientific automated weather station installed at the east end of the site airstrip on August 11, 2004; climate data are available from that date until September 9, 2009. The station was then relocated several hundred metres west-southwest of the Hard Creek campsite and renamed TURNMET2. Several of the instruments were replaced and a new total precipitation gauge and solar radiation sensor were installed. TURNMET2 recorded average hourly and daily wind direction, wind speed, temperature, precipitation, and relative humidity. The station functioned well, but approximately one year of temperature and relative humidity data were lost from June 20, 2005 to August 24, 2006 due to damage to the station caused by a moose. The climate station was overhauled in mid-2018 and renamed “BC400972”. The installation utilised the existing 10 m tower, but included the addition of new instrumentation, including barometric pressure and snow depth. The upgraded station also included GOES satellite telemetry, with data accessible through a web-based portal and updated hourly. Finally, a Class A evaporation pan was installed in 2019 and integrated with the station instrumentation. The geographical coordinates of the meteorological station are shown in Table 5.1.

Table 5.1: Location of Meteorology Stations

Station Name	Year	Easting	Northing	Elevation (masl)
BC400972	2018-Present	508064	6480139	1,020
TURNMET2	2009-2011	5080644	6480139	1,020
TURNMET	2004-2009	508386	6480221	1,015
Dease Lake	1957-Present	440983	6476843	802

Notes: The geographical coordinates are approximate location based on the text from the reports reviewed. NAD 1983 UTM Zone 9N

The estimated mean annual temperature for the period of record (as of the 2011 PEA report) is -2.0°C and the mean monthly temperatures range from a high of 11.1°C in July to a low of -18.0°C in January. The temperature at the project site is approximately 2°C cooler than Dease Lake, which is to be expected given the higher elevation (1,020 masl vs. 802 masl).

As part of the 2011 PEA (AMC, 2011), concurrent months of precipitation from the Dease Lake climate station were compared with project site data to estimate the long-term average precipitation. The average ratio of precipitation between the project site and Dease Lake was 1.5, indicating that the project site receives approximately 50% more precipitation than Dease Lake.

On average, Dease Lake has 381 mm of precipitation annually, so the long-term average precipitation for the project site is estimated to be 571 mm.

Mean monthly wind speeds range from 1.67 m/s in March to 0.73 m/s in July, as reported in the 2011 PEA (AMC, 2011). The overall mean wind speed for the period of record is 1.08 m/s with a maximum hourly wind speed record of 7.15 m/s recorded on September 27, 2004. The monthly wind direction data for the project site indicate that the predominant wind direction is from the southwest, which is expected due to the orientation of the Turnagain River valley at the project site. Wind speeds are expected to be higher at elevated sections of the project site.

The mean monthly relative humidity ranges from 84.1% in October to 50.5% in July, and the overall mean annual relative humidity is 70.6%, as reported in the 2011 PEA (AMC, 2011).

The mean annual lake evaporation for the project site is estimated to be 291 mm at 1,020 masl.

5.3 Hydrology

The project is located near the headwaters of the Turnagain River, which flows generally east and north to join the Kechika River, a tributary of the Liard River, which itself is a tributary of the Mackenzie River, which empties into the Arctic Ocean. Several small creeks flow into the Turnagain River at or near the project site, including Hard Creek, Flat Creek, and Faulkner Creek. Figure 5-2 and Figure 5-3 show Turnagain River near the existing airstrip and Hard Creek just before the confluence with the Turnagain River.

Annual flow patterns are typically characterised by a very pronounced period of high flows in the spring due to snowmelt and rainfall, followed by declining flows through the summer and fall, and low flows throughout the winter.

Hydrometric (streamflow) monitoring stations have been operated in the project area. Continuous monitoring has been done at these stations for the following periods:

- Lower Hard Creek – September 2005 to August 2008, July 2011 to July 2012 and 2018 to present (instantaneous manual flow measurements are ongoing for this site)
- Upper Hard Creek – August 2006 to October 2009 (but not ongoing)
- Farthest Hard Creek – September 2008 to August 2011 (but not ongoing)
- Faulkner Creek – August 2006 to August 2011 and June 2018 to present
- Flat Creek – August 2006 to August 2011 and June 2018 to present
- Turnagain River – September 2008 to August 2011 and June 2018 to present.

Figure 5-2: Turnagain River at Project Location & Airstrip (looking Northeast)



Source: Giga Metals, 2020.

Figure 5-3: Hard Creek flowing into Turnagain River (looking Northwest)



Note: Red dot represents Lower Hard Creek. Source: Giga Metals, 2020.

Installed dataloggers and pressure transducers record water level and temperature at 15-minute intervals, and environmental technicians complete monitoring activities that build the relationship between water level in the streams and flow. The most complete and continuous datasets are for the Faulkner Creek and Flat Creek stations, where over six complete years of data had been collected as of 2011. Unfortunately, periods of data were lost at both the Upper and Lower Hard Creek sites due to instrument failures.

Estimates of long-term average monthly and annual unit runoff for basins in the project area were generated by correlating short-term site data with long-term regional records in the 2011 PEA (AMC, 2011). The results indicate a mean annual unit runoff of approximately 16 L/s/km² and monthly values ranging from a low of 2.6 L/s/km² in March to a high of 54.1 L/s/km² in June. It is apparent from the estimated mean distribution that nearly 50% of the total annual flow occurs during the months of June and July, and that approximately 90% of annual flows occur between the non-freezing months of May and October.

5.4 Local Resources

An exploration camp built on the property in April 2003 can accommodate approximately 35 people. The camp consists of 17 walled tents, three trailers, and drill core logging and storage facilities. Power is provided by an on-site diesel generator and a backup generator.

On-site communications include satellite telephone and internet connections.

There are approximately 36 km of exploration trails on the property, constructed from the late 1960s to the present.

5.5 Infrastructure

Dease Lake (population 335) offers some supplies and services. The cities of Terrace (population 15,700) and Smithers (population 10,600), 580 and 600 km to the south of Dease Lake, respectively, offer the best range of supplies and services which can be trucked to Dease Lake via Highway 37. The closest deep-water port is the bulk terminal at Stewart. There is no rail link within the Cassiar district, although there is a rail bed between Dease Lake and Takla Landing to the south. The closest railhead for the Canadian National Railway is at Kitwanga, approximately 485 km south of Dease Lake.

At present, the Cassiar district is not serviced by the provincial electricity grid. The 3 MW Hluey Lakes Hydro Project, supplemented by diesel generators, produces electricity for Dease Lake. In 2014, BC Hydro completed the extension of the provincial transmission grid to Tatogga, approximately 100 km south of Dease Lake. This line is powered at 287 kV and includes interconnections to run-of-river hydro projects in western BC at Forest Kerr, McLymont Creek and Volcano Creek.

5.6 Physiography

The data on physiography of the Stikine region are taken from the Integrated Land Management Bureau (2007). Between Dease Lake and the property, topography comprises mountains and wide river valleys of the Stikine Ranges. Ridges, plateaus, and summits lower than 1,800 m are rounded while higher summits are rugged. Valley bottoms are 1,000 to 1,350 m elevation, while the highest peak (King Mountain) is about 15 km south of the Turnagain property at 2,425 m elevation. Plateau surfaces are at about 1,500 m.

The valley bottoms and lower elevation slopes are covered with glacial drift. Esker and drumlin formations are numerous and extensive. The ranges are characterised by the occurrence of flat-topped tuyas, which are steep-sided volcanoes that erupted on the plateau surface under the ice sheet during the Pleistocene glaciations.

Boreal white spruce and lodgepole pine forest occur on valley bottoms, where they are interspersed with wetlands. At higher elevations, the boreal forest gives way to sub-alpine fir and scrub birch in open forests and woodlands. In areas of cold-air ponding and in upper elevation exposed areas, the forest gives way to sub-alpine shrub and grassland and scrub vegetation. Alpine shrub-land, heath, and tundra occur above the tree line. Bedrock is reasonably well exposed in the areas above the tree line and along drainage divides.

Several species of large mammal including grizzly bear, black bear, wolf, moose, caribou, mountain goat, and sheep can be found in the Cassiar Mountains. Bird species noted in the mountains include gyrfalcon, golden eagle, willow ptarmigan, least sandpiper, red-necked phalarope, snow bunting, and Smith's longspur.

The Turnagain Project straddles the Turnagain River near its confluence with Hard Creek. The project area covers north-, south-, east-, and west-facing slopes northwest and southeast of the Turnagain River and alpine terrain above the tree line. Elevations range from about 1,000 m along the Turnagain River in the central claims area to 1,800 m at an unnamed summit in the central property area. The general site topography and environmental setting are shown in Figure 5-4 and Figure 5-5.

Figure 5-4: Turnagain Project Area & Access (Transport Trucks on Boulder Trail, looking South)



Source: Giga Metals, 2020.

Figure 5-5: Turnagain Project General Setting (Exploration Drill Hole, looking Northwest)



Source: Giga Metals, 2020.

6.0 HISTORY

The description of the property exploration history is based on work by Nixon (1998) and Baldys et al., (2006), as reported in prior Turnagain studies.

Nickel and copper sulphides were first recognised in rusty weathering exposures at the Discovery zone on the Turnagain River in about 1956. Falconbridge Nickel Mines Ltd. (Falconbridge) acquired the property in 1966 and, during the period 1966–1973, completed an airborne geophysical survey, ground geophysical surveys, geological mapping, geochemical surveys, and 28 wide-spaced diamond holes (2,895 m). The work identified several sulphide “showings”. The exploration program tested many of the mineralised outcrops by “packsack” drilling; the Discovery outcrop was not successfully drilled.

During the early 1970s, adjacent claims were investigated with a geochemical survey by Union Minière Exploration and Mining Corporation Ltd. (UMEX). Once the Falconbridge and UMEX claims expired, several of the showings were re-staked and tested with short, small diameter core holes by an unnamed party. Three EX-sized core holes, totalling 55.5 m, were drilled on the west bank of the Turnagain River in 1977. No significant intersections were reported and the collars have not been located. In 1979, S Bridcut drilled a single drill hole (17 m) near the east bank of the Turnagain River and intersected unmineralised quartz diorite.

The commodity focus for exploration shifted to platinum group elements (PGEs) in the mid-1980s. A geochemical survey for PGEs was conducted for Equinox Resources Ltd. in 1986, and Bridcut re-sampled the Falconbridge core in 1988.

In 1996, Bren-Mar optioned the Cub claims from Schussler and Hatzl. From 1996 to 1998, Bren-Mar completed an airborne magnetic survey over 45 km² (400 line-km of survey), 19 diamond drill holes (3,889 m), geological prospecting and sampling, down-hole pulse electromagnetic surveys in four of the 1997-1998 drill holes, and preliminary metallurgical testwork on drill core composite samples.

Bren-Mar changed its name to Canadian Metals Exploration Limited (CME), and resumed exploration in 2002 with an induced polarisation (IP) and ground magnetic survey followed by 1,687 m of diamond drilling in seven holes. Drilling continued in 2003, with 23 holes (including deepening of one of the 2002 drill holes) completed for 8,769 m. Additional exploration included geological mapping and prospecting, as well as bedrock, stream sediment, and soil sampling. In 2004, CME changed its name to Hard Creek Nickel Corporation and recommenced work on the property, including:

- geological mapping
- bedrock, stream sediment, and soil sampling
- surface, borehole, and airborne geophysical surveys
- mineralogical, metallurgical, and analytical studies
- 172 diamond drill holes for 41,502 m of drilling.

6.1 2006-2008

In 2006, HNC reported a measured and indicated resource estimate inside a 0.2% sulphide nickel grade shell. Only the sulphide minerals were considered recoverable into a saleable product; therefore, the 2006 resource estimate was reported in terms of sulphide nickel. Sulphide nickel was determined using an ammonium citrate hydrogen peroxide partial extraction procedure. The estimate was completed by Geosim of Vancouver (Simpson, 2006).

Later in 2006, HNC reported results of the first Preliminary Economic Assessment (PEA) on the project. A key assumption of the PEA was that a 0.10% sulphide nickel analysis cut-off was economically reasonable for the project. This cut-off was determined based on parameters selected for pit optimisation. Resources in the PEA were reported in terms of sulphide and total nickel.

In 2007, HNC reported a new measured and indicated resource estimate in terms of sulphide and total nickel inside a 0.10% sulphide nickel grade shell. This estimate was completed by Geosim and resulted in a significant increase in the tonnes of the deposit (Simpson, 2007).

Resource estimates reported in 2006 and March 2007 were constrained using sulphide nickel grade shells. The restriction on grade shells was appropriate given that no geological domains had been defined at that time.

In January 2008, AMEC completed a second PEA, which included an updated resource estimate constrained by lithologic domains based on the nearest-neighbour interpolation of geology from drill logs. At the time the resource estimate was carried out, results from the 2007 drill program were not available.

In June 2008, AMEC released an interim resource estimate that included results of all 2007 drill holes. In the same year, HNC completed an additional 16 core holes totalling 4,105 m.

6.2 2009-2011

In April 2010, Wardrop released another PEA, based on an updated resource that included the results of the 70 holes (21,099 m) drilled in late 2007 and 2008, as well as additional metallurgical work (production of a bulk flotation concentrate to feed a hydrometallurgical treatment plant). The project scope at that time consisted of an 87,000 t/d flotation plant employing the Outotec nickel chloride leach process to produce 35,000 t/a LME grade nickel metal and 2,000 t/a cobalt as a hydroxide.

In 2010, HNC completed two core holes totalling 384 m to recover 3,530 kg of core for metallurgical testing.

In 2010-2011, a metallurgical testwork program at SGS Vancouver led to a breakthrough in reagent selection, resulting in repeatable recovery of high-grade flotation concentrates, with concentrate grades over 18% nickel and recoveries of total nickel in the 50% to 65% range.

In 2011, AMC completed a PEA based on a two-phase facility culminating in an 87,000 t/d flotation plant producing high-grade nickel concentrate (>18% nickel).

6.3 2012-2019

In 2017, HNC changed its name to “Giga Metals Corporation” to reflect the company’s intent to become a mineral firm providing nickel, cobalt, and potentially other raw materials for use in electric vehicles (EV) and battery energy storage markets. Giga Metals is a publicly traded company, headquartered in Vancouver, BC (a registered BC company), and listed on the TSX Venture Exchange.

In 2018, a diamond drilling program (40 holes, 10,835 m) was completed, along with a metallurgical test program and engineering studies (see Sections 10, 11, 12, 14).

The 2018 metallurgical program, overseen by Blue Coast Metallurgy, was focused on a master composite created from five lithology composites originating from Hole 10-266, which was a horizontal drill hole, drilled through the southwest portion of the Horsetrail resource, dissecting what is likely to be the heart of the early production resource. The comprehensive program included a suite of comminution tests, mineralogy, and detailed flotation testing. Hole 10-266 was drilled in 2010; fresh drill core was not available for this study.

In 2018, Hatch completed a conceptual engineering study looking at replacing the semi-autogenous grinding step of prior PEA studies with more energy-efficient, high-pressure grinding rolls.

Engineering, resource evaluation, and metallurgical works were continued in 2019. Hatch conducted a process plant site location trade-off study. Blue Coast Research began a detailed flotation study, on fresh material, examining a wider range of variability samples and targeting the production of a bulk concentrate for marketing purposes.

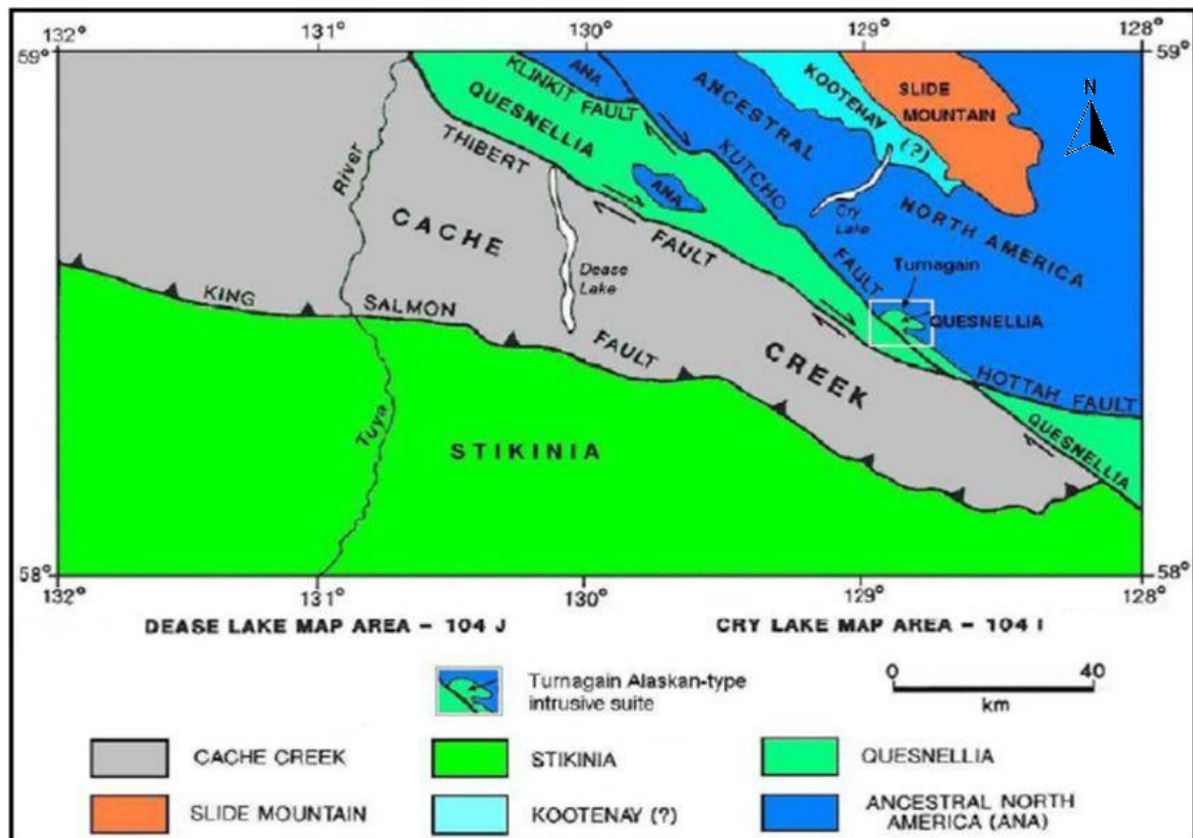
7.0 GEOLOGICAL SETTING & MINERALISATION

7.1 Regional Geology

The regional geology of the Turnagain property has been described by Nixon (1997, 1998), Scheel et al. (2005), and in Technical Reports by Geosim (2006, 2007), AMEC (2006) and AMC (2011). The regional description provided here is based on work by Scheel et al. (2005), Scheel (2007), and Nixon (1998). The geological understanding of the region and the setting of the deposit continues to be refined with additional information from drilling and exploration programs.

The property encompasses the Turnagain ultramafic complex and its host rocks, and the ultramafic rocks may be hosted within either the Yukon-Tanana terrane or the Quesnel terrane. The Turnagain complex is fault-bounded, has dimensions of about 3.5 km x 8 km, and lies to the north of two major fault systems, the Kutcho and Thibert-Hottah Faults (Figure 7-1). Neither fault system is exposed on the property.

Figure 7-1: Regional Structural Setting – Turnagain Property



Source: Modified from Gabrielse (1998).

The western, northern, and eastern margins of the complex abut rocks attributed to the Lower Ordovician Road River Formation and the Mississippian Earn Group (Figure 7-2). The Road River and Earn Group rocks comprise graphitic phyllite, which can be strongly pyritic and graphitic near the Turnagain complex intercalated with lesser quartz-rich and calc-silicate tuff layers. The graphitic phyllite in the vicinity of the property remains directly and biostratigraphically undated. Metamorphism in the phyllites regionally reaches greenschist facies. No contact hornfelsing has been mapped adjacent to the northern or eastern contacts with the Turnagain complex.

A series of undated sedimentary rocks, possibly volcanoclastic, lies south of the Turnagain complex. This series may represent rocks of the Lay Range assemblage of the Quesnel terrane (Figure 7-2). On the south side of the Kutcho Fault, dioritic to granodioritic rocks from the early Jurassic Eaglehead Pluton crop out.

The regional setting and method of emplacement of the Turnagain complex is still being established. Gabrielse (1998) postulates that the Turnagain complex intrudes rocks of the miogeoclinal margin of ancestral North America, indicating that a supra-subduction setting was operational at the cratonic margin at the time of emplacement. An alternative view (Scheel et al., 2005; Nixon, 1998) places the Turnagain complex within an imbricated set of rocks that was thrust eastward onto the margin of the North American craton.

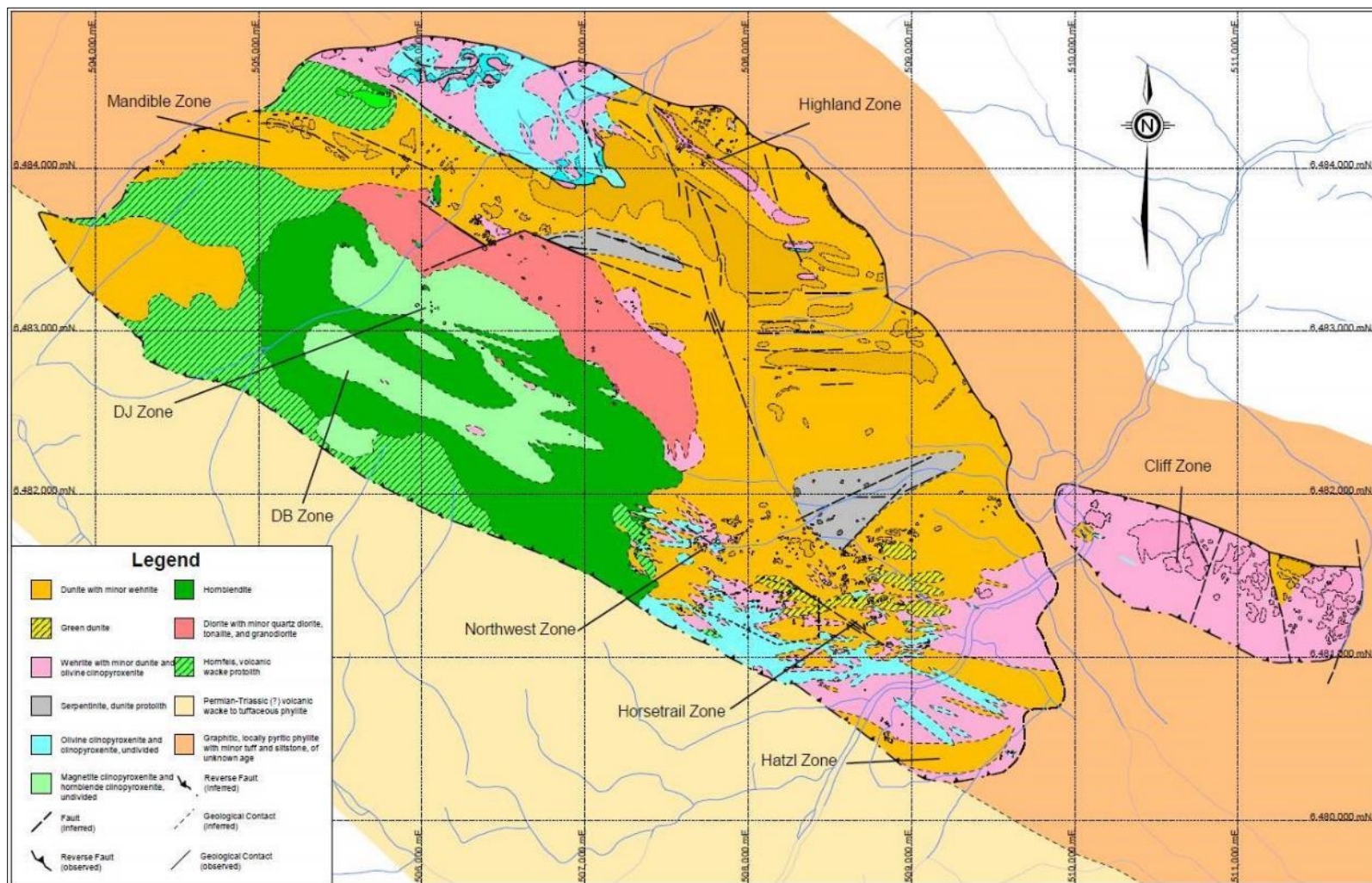
7.2 Property Geology

The Early Jurassic (190 ±1 million years ago (Scheel, 2007)) Turnagain complex comprises a central core of dunite with bounding units of wehrlite, olivine clinopyroxenite, clinopyroxenite, representing crystal cumulate sequences, hornblende clinopyroxenite and hornblendite (Figure 7-2). The complex is elongate and broadly conformable to the northwesterly trending regional structural grain.

The ultramafic rocks are generally fresh to mildly serpentinised; however, more intense serpentinisation and talc-carbonate alteration occur along faults and restricted zones within the complex. The central part of the ultramafic body is intruded by granodiorite to diorite, and hornblende–plagioclase porphyry dikes and sills.

Primary layering in clinopyroxene-rich cumulates, reflecting variations in the modal abundance of olivine and pyroxene, is visible in outcrop. The layering has variable dips and is truncated by the faulted eastern boundary of the complex. Despite localised zones of well-developed cumulate layering, way-up direction indicators are inconclusive and the internal structure of the Turnagain complex is poorly understood (Nixon, 1998).

Figure 7-2: Property Geology



Source: Sheel, 2007.

The descriptions of lithologies in the following subsections are modified from Scheel et al. (2005).

7.2.1 Dunite

Dunite is primarily found in the eastern and central portions of the complex. It is mainly composed of cumulus olivine, minor amounts of chromite and pyroxene, and trace amounts of primary phlogopite. Dunite commonly hosts grains of poikilitic green diopside, either as discrete, centimetre-scale crystals or elongate aggregations. The latter are interpreted to be small dikes resulting from the escape of trapped liquid.

Millimetre-to centimetre-scale layering in the dunite core is evident locally where concentrations of chromite crystals have accumulated. These chromitite horizons are discontinuous and commonly remobilised and intruded by thin dunite dikes.

Serpentinisation volumes are highly variable, but generally are no more than about 10% of the rock by volume. The degree of overall serpentinisation is higher in the Horsetrail, Northwest, and Hatzl zones. Secondary magnetite is abundant where serpentinisation is pervasive. Some dunite that is proximal to massive sulphide mineralisation commonly contains some alteration to grey tremolite.

Contacts between wehrlite and dunite are sharp to gradational over short distances, represented by a slight change in the size and modal abundance of clinopyroxene, and may reflect magmatic layering.

7.2.2 Wehrlite

Two different wehrlite types have been identified. On the west side of the Turnagain River, the wehrlite is mainly composed of cumulus olivine with a sizable proportion of interstitial clinopyroxene and minor amounts of cumulus clinopyroxene. On the east side of the river, and in the far northwest of the intrusion, cumulus clinopyroxene reaches approximately 40% by volume of the rock mass, cumulus clinopyroxene is typically prismatic and finer grained than coexisting olivine. Both types of wehrlite commonly contain abundant serpentine up to 85% of the rock by volume.

7.2.3 Olivine Clinopyroxenite & Clinopyroxenite

These rock types mostly crop out in the northwestern part of the intrusion and commonly comprise around 85% cumulus clinopyroxene and smaller amounts of cumulus olivine. These rocks are also common along the southern margin of the Horsetrail and Northwest zones. Depending on location within the complex, the clinopyroxenites can be either an original magma differentiate or an intrusive; in the northwestern portion of the complex, they appear to be related to the original magma; further to the east, they are brecciated and intrusive in nature. Pegmatitic clinopyroxenite dikes are commonly found adjacent to the cumulate clinopyroxenite or intruding more olivine-rich lithologies in the Horsetrail and Northwest zones. These latter intrusions are interpreted to be late-stage injections of trapped liquid through olivine-rich cumulates.

7.2.4 Hornblende Clinopyroxenite & Clinopyroxenite

These rock types are generally restricted to the west-central portion of the Turnagain intrusion and coincide with a copper-platinum-palladium soil anomaly. They are very poorly exposed and their relationships to other units in the Turnagain complex are not well defined. Some of these rocks contain angular, altered clasts of former dunite and wehrlite.

7.2.5 Magmatic Hornblendite & Hornblende Clinopyroxenite

Generally found in the southwestern portion of the complex, these rock types contain amphibole crystals that typically range from less than one centimetre to up to three centimetres in length. The crystals appear to be cumulus, but in some cases, they replace pyroxene. Most hornblende-bearing ultramafic rocks in the Turnagain complex are associated with large amounts of magnetite that is interpreted to be cumulus in origin.

7.2.6 Hornblende Diorite

A 2 km x 300 m elongate hornblende diorite to granodiorite body, offset by an east-northeast striking fault, intrudes hornblendite and dunite in the central part of the intrusive suite. Narrow porphyritic granitic dikes, about 1 m to 2 m wide and clearly post-mineral, have been noted cutting wehrlites and clinopyroxenites in drill core. Some dikes may be up to 20 m wide and all dikes are spatially associated with the large hornblende diorite intrusion.

7.2.7 Metasediments

Numerous inliers, xenoliths and small inclusions of hornfelsed, calc-silicate metasedimentary rocks, like those seen marginal to the ultramafic intrusion, are present within the ultramafic intrusive rocks. These inclusions are thought to be the sulphur source responsible for the sulphide mineralisation in the Turnagain intrusion and are sourced from the wall rocks.

7.3 Mineralisation

Showings of semi-massive and massive sulphides have been identified by work to date. These semi-massive and massive zones, plus broad zones of disseminated sulphides, are generally hosted by dunite and wehrlite near the southern and eastern margins of the ultramafic body. The central and northern dunite is largely devoid of sulphide minerals although their highly magnesian olivine is more enriched in nickel (up to 0.20 to 0.30 weight percentage) than the olivine in the peridotites and pyroxenites of the Horsetrail and Northwest zones, which may be nickel-depleted in areas of sulphide mineralisation. Nixon (1998) suggests that these features are further evidence of fractional crystallisation of the ultramafic magma.

Primary sulphide minerals consist of pyrrhotite with lesser pentlandite (iron-nickel sulphide) and minor chalcopyrite. Some bornite has been reported. Interstitial and blebby sulphides, with grain sizes ranging from 1 to 4 mm, are evident in widespread disseminated zones seen in drill cores. With increasing concentrations, these intercumulus sulphide grains coalesce to form net-textured

sulphides. Semi-massive and massive sulphides, and rare sulphide matrix breccias, were also noted in drill cores over intervals not exceeding a few tens of centimetres.

Narrow fracture-filling sulphide lenses, commonly featuring chalcopyrite and minor pentlandite along with the more prevalent pyrrhotite, appear to be products of remobilisation of primary sulphides adjacent to dikes, altered xenoliths, and serpentinised areas.

Secondary nickel and copper sulphides, including violarite and valleriite, have been noted in serpentinised zones and both primary and secondary sulphides are associated with graphite (Nixon, 1998). Microscope and microprobe studies of drill core samples from the Horsetrail Zone (Kucha, 2005) have identified additional nickel sulphide minerals including mackinawite, heazlewoodite, godlevskite, and millerite. Platinum group element minerals identified to date include vysotskite, a palladium-iron-nickel sulphide, and sperrylite, a platinum arsenide mineral.

The principal mineral zones identified to date on the Turnagain property include the following:

- The Horsetrail Zone and surrounding area have been the focus of most of the historic and recent diamond drilling. Results to date suggest a northwest to west-northwest trend for these zones, which consist of broadly dispersed, disseminated to intercumulus sulphide mineralisation in both dunite and wehrlite and serpentinised equivalents. Sulphide grains range in size from 0.5 to 5 mm and commonly occupy interstices between olivine grains. Drill core samples from the Horsetrail Zone have a median of 0.23% total nickel with grades ranging from 0.01% to 4.89% total nickel. Total cobalt grades range from 0.001% to 0.480% with a median of 0.013% Co. There appears to be a spatial relationship between graphitic xenoliths, increasing clinopyroxene content in the ultramafic host rocks and the incidence of sulphide mineralisation. Where present, chalcopyrite occurs along the margins of pyrrhotite and in narrow veinlets. Relatively unaltered dunite adjacent to the Horsetrail Zone may contain total nickel values of 0.20% to 0.30%, virtually all of which is in the crystal lattices of the silicate mineral olivine and consequently is not of economic importance.
- The Northwest Zone is contiguous with, and lies northwest of, the Horsetrail Zone. This zone has mineralisation styles and grades similar to the Horsetrail Zone, but is intruded by several mafic and felsic dikes which dilute the overall grade. Drill core samples from the Northwest Zone have a median grade of 0.20% total nickel with grades ranging from 0.01% to 2.86%. Total cobalt grades range from 0.001% to 0.166%. The Horsetrail and the Northwest Zones form a zone approximately 2,000 m long in the east-west direction, and 550 m wide from north to south and have been tested by 251 drill holes.
- The Hatzl Zone mineralisation consists of disseminated and net textured pyrrhotite and pentlandite hosted by dunite and wehrlite. This mineralisation is similar to, and may be continuous with, the Horsetrail Zone. The Turnagain River flows between the two zones and the region below the river has not been sufficiently drill tested to exclude the potential of additional mineralisation. The Hatzl Zone is 1,150 m long in a

northeast direction and 300 m wide in a northwest direction and has been tested by 17 drill holes.

- The Duffy Zone mineralisation lies 500 m northeast of the Horsetrail Zone and consists of disseminated sulphides similar to those within the Horsetrail Zone. Grades range from 0.014% to 0.525% total nickel. The Duffy Zone is 300 m in diameter and does not crop out. It was discovered by exploration drilling in 2006. The zone has been tested by six drill holes.

Other mineralised zones are exploration targets include:

- Bench, DJ, and DB prospects, which host platinum group element (PGE) mineralisation
- Mandible, Davis, Highland, and Discovery prospects, which host Ni-Co mineralisation
- Cliff and Central area prospects, which host Ni-Co and PGE mineralisation.

8.0 DEPOSIT TYPES

The Turnagain deposit is a magmatic sulphide resource hosted by an Alaskan-type intrusion. Alaskan-type intrusions are a recognized class of ultramafic intrusion that occurs along convergent plate-margin settings. The principal minerals in these ultramafic rocks are olivine, clinopyroxene, magnetite and hornblende. Orthopyroxene and plagioclase are extremely rare. Assemblages of these minerals generally form the crudely zoned rock types dunite, wehrlite, olivine clinopyroxenite, clinopyroxenite and hornblendite.

While Turnagain exhibits these Alaskan-type characteristics, it is unusual in that it hosts magmatic sulphide mineralisation in appreciable abundance. Nixon (1998) concluded that the iron-nickel-copper (Fe-Ni-Cu) sulphides in the Turnagain complex are primary and magmatic (as opposed to having resulted from a post-emplacement process), and that wall rock inclusions which have been observed in drill core may have provided a mechanism for sulphur saturation and precipitation of Fe-Ni-Cu sulphides. This has been confirmed by sulphur and lead isotope results reported by Scheel (2007).

Disseminated and rare net-textured mineralisation at Turnagain is hosted in dunite, wehrlite, olivine clinopyroxenite and clinopyroxenite and serpentinitised equivalents. Sulphides include pyrrhotite, pentlandite, chalcopyrite, and trace bornite. Valleriite is sometimes present where serpentinitisation is intense.

9.0 EXPLORATION

Section 6 of this report summarises the early exploration work carried out between 1957 and 1995 and presents an overview of work completed by Giga Metals and its predecessor companies since acquisition of the project in 1996. This section presents more detail on exploration since 1996.

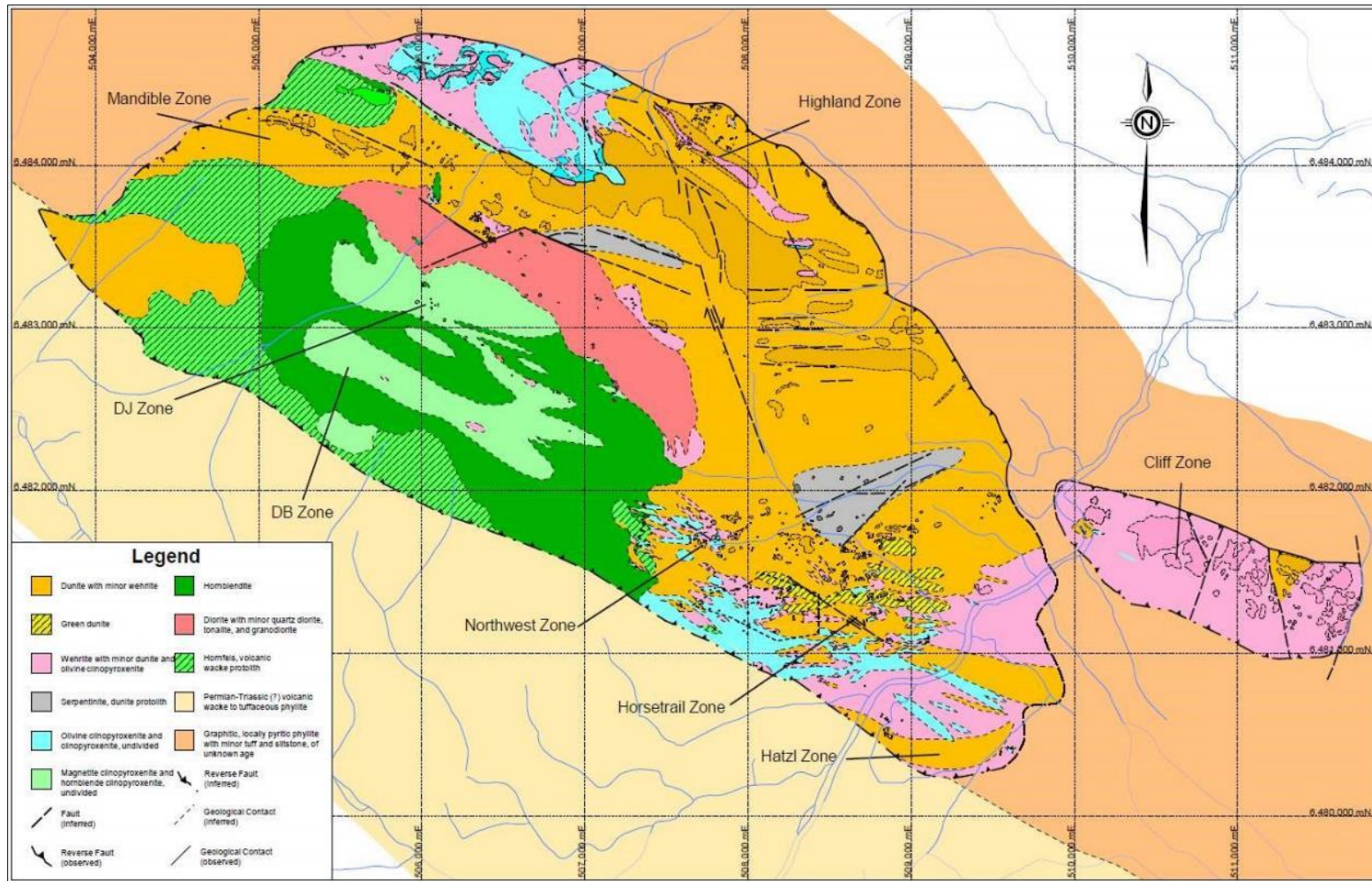
9.1 Geological Mapping

Sulphide-bearing outcrops of the Davis, Horsetrail, Discovery, and Cliff zones were relocated, and then prospected and mapped in 1996.

In 1998, a global positioning survey (GPS) was undertaken by Bren-Mar personnel using a Trimble Geoexplore 2 instrument to locate drill holes, claim posts, and other geographical positions.

Detailed geological mapping was undertaken by Clark (1976) at various scales from 1:50 (inches to feet) to 1:1,000 as part of his Ph.D. thesis work. Additional mapping, as shown in Figure 9-1, was completed by Giga Metals' geologists and Scheel (2007) at metric scales ranging from 1:1,000 to 1:10,000.

Figure 9-1: 2007 Geological Mapping



Source: Scheel, 2007

9.2 Geochemical Surveys

The following discussion, modified from Carter (2005), is considered thorough. It is believed to reasonably represent the surface geochemical soil sampling programs completed on the property.

Of importance are the results of a 1971 soil geochemical survey conducted by UMEX over mineral claims contiguous with Falconbridge claims, and covering the northeastern margin of the ultramafic complex and the Cliff Zone east of Turnagain River. More than 800 samples were collected from B and C soil horizons at 200 ft (61 m) intervals along grid lines spaced 400 ft (122 m) apart. The samples were analysed for nickel, copper, and cobalt. Values greater than 650 ppm nickel and 300 ppm copper were considered anomalous; cobalt values were erratic. The best results were obtained from a 900 m x 450 m area west of the Discovery Zone where anomalous nickel values ranged from 800 ppm to 2000 ppm.

A geochemical sampling program carried out in 2003 consisted of the collection and analysis of 250 soil samples at a 100 m spacing along four topographic contour lines between 1,300 m and 1,460 m elevation, northwest and upslope of the principal mineralised zones. An analysis and interpretation of the results obtained from these samples was undertaken by Dr. Colin E. Dunn, P. Geo. on behalf of Giga Metals in early 2004 (Carter, 2005).

Results for copper, nickel, cobalt, and platinum + palladium were kriged and contoured at 90th, 80th, 70th and 50th percentiles. Coincident high copper, cobalt, and platinum + palladium values are concentrated within a poorly explored area between 3 km and 4 km west-northwest of the Horsetrail Zone. Elevated nickel values in soils are more widespread and are coincident with the Horsetrail Zone and immediately northwest of the copper, cobalt, and platinum + palladium anomalies.

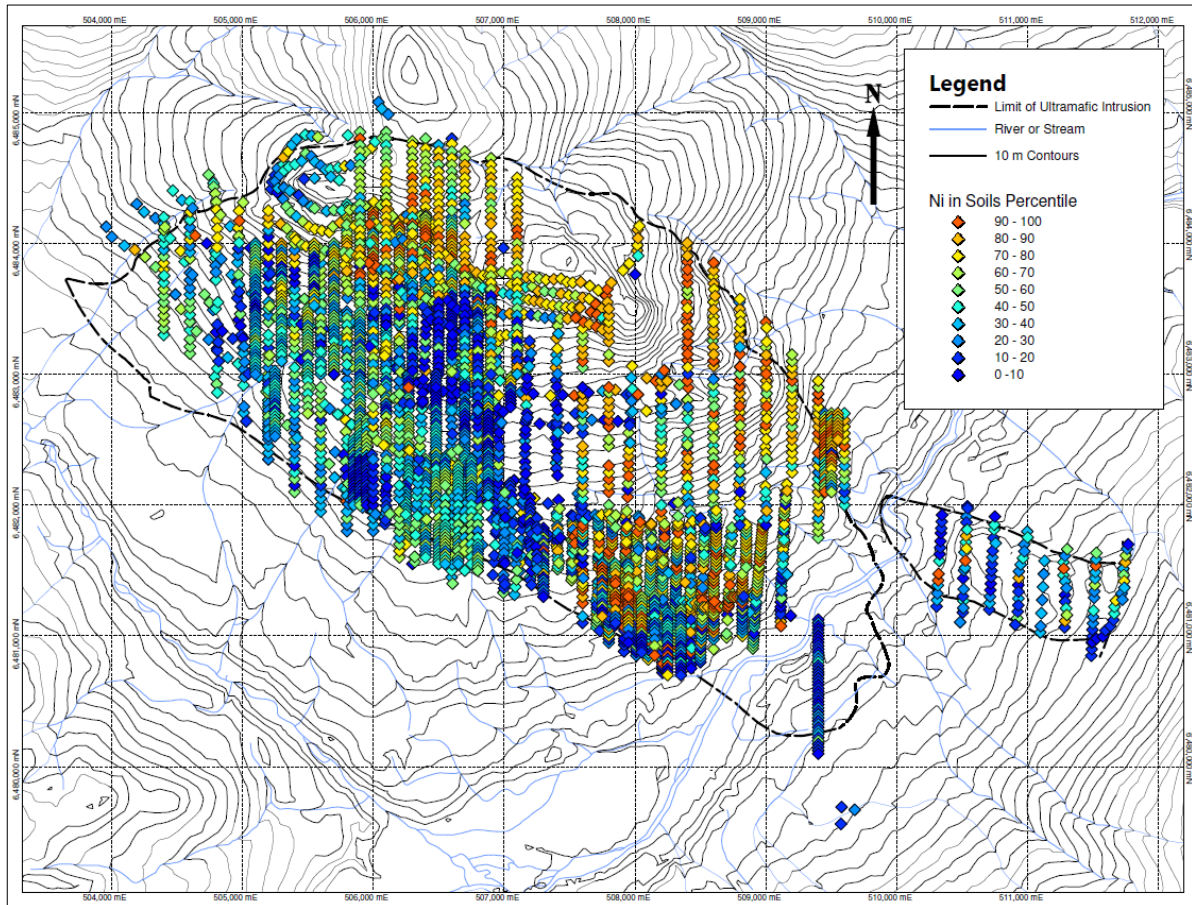
More than 2,000 soil samples during the 2004 and 2005 programs were collected at 50 m intervals along survey lines spaced 200 m apart within an area of 15 km². More detailed sampling at 25 m intervals on lines spaced 50 m apart was undertaken in areas yielding anomalous base and precious metals results. Results of this survey highlighted two strong copper-in-soil anomalies 2.5 km northwest of the Horsetrail Zone with values exceeding 430 ppm copper with peaks to 3,219 ppm copper over areas of 1,500 m x 1,100 m and 900 m x 600 m. These anomalous areas flank the hornblende diorite-granodiorite intrusion within ultramafic rocks in this area. Anomalous platinum + palladium values in soils, in part coincident with the DJ zone, extend from the northern part of the larger copper-in-soils anomaly. Anomalous nickel values in soils are widespread over the northern part of the Turnagain ultramafic intrusion and within and adjacent to the Horsetrail Zone. The geochemical interpretation requires that anomalous nickel values in soils are paired with copper so that the highly mobile nickel originating from olivine can be screened. Copper occurs only in sulphide minerals, and when present in ultramafic rocks with nickel can be used successfully to indicate nickel anomalies of exploration significance.

The 2004 geochemical program also included the collection and analysis of 330 rock float and 243 bedrock samples from within, and adjacent to, the soil geochemical grid. Results for total nickel and platinum + palladium indicated significant total nickel results (>0.20% to a maximum

of 1.9%) in both float and bedrock samples, which are mainly clustered in the area of the Horsetrail Zone and in a smaller area north of the DJ zone.

A map of the combined geochemical samples is shown in Figure 9-2.

Figure 9-2: Map of Geochemical Sampling



Source: Giga 2020.

9.3 Geophysical Surveys

The following discussion, modified from Carter (2005), is considered thorough and reasonably representative of the geophysical survey programs completed on the property.

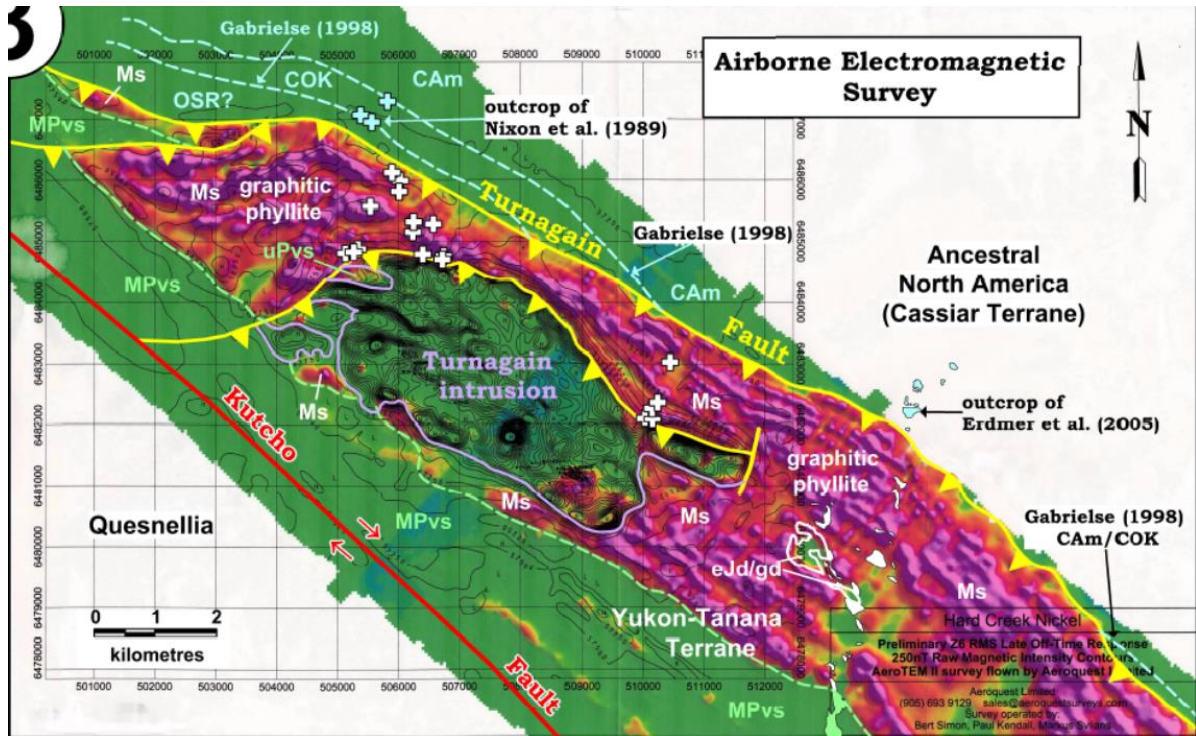
9.3.1 Airborne Surveys

An airborne geophysical survey was completed over the Turnagain property by AeroQuest Ltd. (AeroQuest) in late September 2004. The AeroQuest survey utilised a helicopter borne AeroTEMII time-domain electromagnetic system and a high sensitivity caesium vapour

magnetometer. Continuous readings on both instruments were obtained from northeast-southwest oriented survey lines at 100 m to 200 m spacing. Precise locations were established using a GPS.

Two geophysically anomalous areas within the ultramafic rocks were surveyed along lines on 50 m spacings (Figure 9-3). Terrain clearance was 30 m and the survey totalled 1,866 line-km. The AeroQuest magnetic response confirmed the results of earlier surveys, accurately outlining the limits of the Turnagain ultramafic intrusion. Magnetic data ranged from lows of 55,000 nanoteslas (nT) to highs of 63,000 nT; the average background was 57,800 nT. The AeroQuest survey also highlighted electromagnetic anomalies within the ultramafic intrusion.

Figure 9-3: Map of 2004 Airborne Electromagnetic Survey



Source: Nixon et al., 2017.

10.0 DRILLING

The Turnagain drill hole database contains 362 drill holes totalling 90,635 m of drilling. The previous technical report (AMC, 2011) reported on all drilling completed up to, and including, 2010. No drilling took place from 2011 to 2017. In 2018, Giga Metals completed 40 drill holes totalling 10,835 m. Of the 362 drill holes, 307 have assay data and 240 are within the resource estimation study area which is the subject of Section 14 of this report. Table 10.1 summarizes the drill holes completed by year and operator. Hole locations within the defined resource are shown in Figure 10-1.

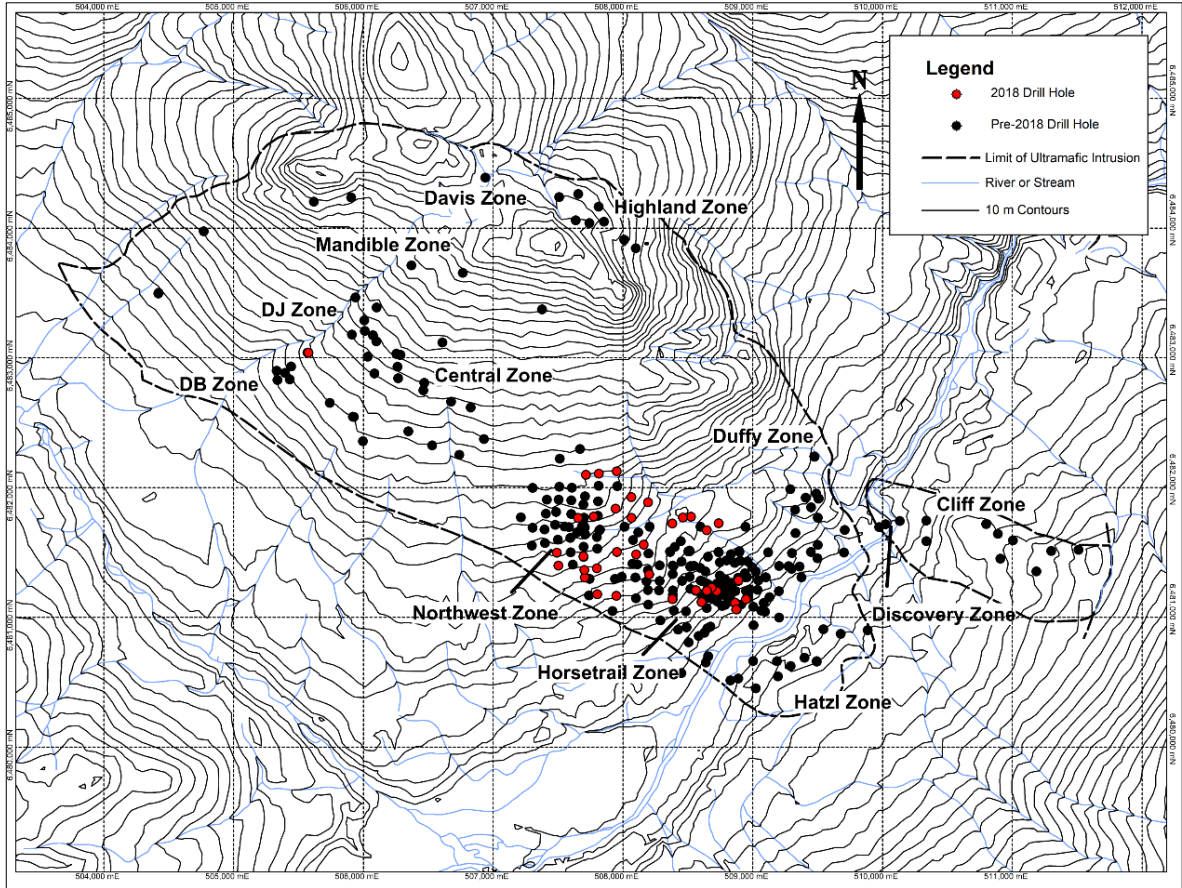
Table 10.1: Summary of Drill Programs

Year*	Operator	No. Holes	Metres**
1967	Falconbridge	13	1,310
1970	Falconbridge	15	1,457
1996	Bren-Mar	5	793
1997	Bren-Mar	9	1,855
1998	Bren-Mar	5	1,264
2002	Canadian Metals	7	1,938
2003	Canadian Metals	22	8,419
2004	Hard Creek Nickel	49	7,633
2005	Hard Creek Nickel	37	7,541
2006	Hard Creek Nickel	68	19,173
2007	Hard Creek Nickel	74	23,928
2008	Hard Creek Nickel	16	4,105
2010	Hard Creek Nickel	2	384
2018	Giga Metals	40	10,835
Total		362	90,635

Notes: *Five holes were extended in subsequent years. Extension metres in this table listed under the year of holes' original collaring. ** Rounding to nearest metre may occur.

Most of the holes drilled to date have been moderately to steeply inclined. Since 2004, contractor DJ Drilling (2004) Ltd. has recovered NQ (47.6 mm) core. Part of the 2007 drill program included PQ (85 mm) core collected for metallurgical purposes. Core recoveries are excellent, averaging 95%. Prior to 2006, most drill core sample intervals were 2 m. Since 2006, core sampling has been completed predominantly on 4 m intervals. The 2018 drilling was performed using NQ (47.6 mm) core.

Figure 10-1: Drill Hole Location Plan



Source: Kirkham 2020.

Table 10.2 lists the drill holes along with location and orientation.

Table 10.2: Drill Hole Collars, Location & Orientation

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH02-01	509329.3	6481650	1070	203.3	0	-90
DDH02-02	508737.5	6481501	1130	213.1	0	-85
DDH02-03	508737.5	6481501	1130	318.21	180	-50
DDH02-04	508737.5	6481501	1130	149	0	-50
DDH02-05	508512	6481514	1160	152.4	0	-90
DDH02-06	508512.31	6481513.43	1162.68	485.2	181.82	-50.43
DDH02-07	508507	6481510	1160	416.4	225	-50
DDH03-01	508515	6481510	1160	501.7	240	-50
DDH03-02	508117.1	6481656	1230	532.2	225	-45
DDH03-03	507601.7	6481902	1302	462.1	180	-50
DDH03-04	507601.6	6481902	1302	334.4	180	-70
DDH03-05	508654.78	6481467.3	1138.29	590.7	168.93	-47.53

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH03-06	508563.8	6481206.63	1104.66	523	180	-50
DDH03-07	508583.25	6480856.29	1036.14	434.4	169.45	-47.07
DDH03-08	509447.08	6481503.95	1027.51	477.3	206.08	-56.43
DDH03-09	509447.38	6481504.58	1027.51	252.1	200	-85
DDH03-10	508503.89	6481506.83	1162.67	577.9	197	-51.73
DDH03-11	508502.8	6481508	1160	249.9	0	-55
DDH03-12	508730	6481199.11	1086.75	349.6	350.63	-76.1
DDH03-13	508560.64	6481206.26	1104.27	322	6.75	-49.75
DDH03-14	508560.59	6481205.13	1104.23	261.6	6.75	-84.17
DDH03-15	508484.38	6481045.69	1090.17	508.1	21.78	-64.95
DDH03-16	508690.89	6481140.65	1079.91	369.1	34.52	-49.28
DDH03-17	508832.99	6481251.47	1083.42	296.6	41.4	-51.05
DDH03-18	508890.97	6481301.36	1082.83	242.95	50.83	-50.3
DDH03-19	508862.34	6481113.97	1058.1	303.3	43.57	-49.72
DDH03-20	508975.32	6481214.47	1061.59	214.6	45.65	-46.8
DDH03-21	508605.95	6481280.83	1117.19	333.75	32.17	-46.77
DDH03-22	508382.53	6481398.5	1167.89	281.9	53.15	-48.62
DDH04-23	508744.58	6481183.8	1085.01	413.3	46.15	-49.75
DDH04-24	508789.59	6481215.51	1083.65	370.65	46.4	-46.9
DDH04-25	508954.57	6481309.43	1081.56	221.3	40.72	-49.53
DDH04-26	508950.95	6481308.42	1081.88	178.6	28.8	-49.23
DDH04-27	508888.25	6481299.62	1082.97	264	29.67	-47.97
DDH04-28	508727.68	6481198.15	1086.84	233.15	5.03	-43.37
DDH04-29	508824.15	6481132.97	1063.56	245.7	45.32	-46.35
DDH04-30	508907.97	6481098.29	1044.31	215.2	39.47	-45.1
DDH04-31	508784.37	6481168.53	1077.37	113.7	52.87	-50.22
DDH04-32	508841.5	6481206.01	1078.79	115.8	51.72	-50.37
DDH04-33	508948.04	6481140.95	1048.16	135.95	43.2	-48.12
DDH04-34	508646.17	6481208.47	1094.97	120.4	349.28	-47.63
DDH04-35	508789.37	6481280.96	1090.38	166.4	355.8	-49.3
DDH04-36	508722.854	6481259.948	1098.507	120.7	354.37	-50
DDH04-37	508722.39	6481259.19	1098.07	117.65	176.67	-49.35
DDH04-38	508192.22	6481363.82	1189.48	120.7	45.32	-49.43
DDH04-39	507938.03	6481297.05	1178.66	148.2	48.98	-49.33
DDH04-40	508546.41	6481397.69	1145.26	118.9	48.28	-53.7
DDH04-41	509359.38	6481391.57	1028.07	96.32	22	-50
DDH04-42	506927.578	6482375.041	1371.506	76.5	0	-90
DDH04-43	506826.179	6482617.075	1401.576	158.8	0	-90
DDH04-44	506674.127	6482662.745	1411.06	124.1	0	-90
DDH04-45	506460.975	6482749.722	1423.752	186.25	0	-90
DDH04-46	506468.861	6482806.906	1436.257	145.4	0	-90
DDH04-47	506267.563	6482843.425	1425.672	184.4	0	-90
DDH04-48	506254.412	6483031.55	1459.441	166.75	0	-90
DDH04-49	506254.439	6483032.547	1459.557	75.3	180	-50
DDH04-50	506254.229	6483030.535	1459.82	169.15	0	-60
DDH04-51	506284.205	6483023.234	1462.76	153.9	0	-60
DDH04-52	506073.263	6483173.319	1456.806	112.15	0	-90
DDH04-53	506073.364	6483174.533	1456.413	114.3	0	-50

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH04-54	506100.176	6483128.014	1453.201	149.95	180	-50
DDH04-55	506280.841	6483021.702	1462.377	60.05	0	-90
DDH04-56	506084.006	6482880.609	1414.473	100	0	-90
DDH04-57	506263.32	6482932.592	1440.86	111.85	0	-90
DDH04-58	506010.275	6483207.197	1454.881	111.25	35	-80
DDH04-59	506006.854	6483289.47	1462.932	110.95	0	-80
DDH04-60	507822.68	6481676.69	1252.38	201.8	44.28	-48.67
DDH04-61	507816.43	6481669.74	1252.84	114.3	226.6	-47.02
DDH04-62	507817.31	6481670.61	1252.68	67.95	231.8	-85.88
DDH04-63	508398.42	6481542.92	1181.64	181.35	43.67	-47.88
DDH04-64	508444.72	6481587.21	1175.77	138.7	43.57	-47.27
DDH04-65	508363.16	6481504.35	1185.19	135.95	41.75	-43.45
DDH04-66	508684.02	6481176.52	1087.79	179.2	7.63	-48.08
DDH04-67	508686.65	6481232.12	1099.81	145.1	1.9	-48.82
DDH04-68	508787.18	6481096.41	1062.72	90.2	45.05	-50.22
DDH04-69	509003.72	6481081.96	1025.14	196.9	45.53	-50.2
DDH04-70	509275	6481395	1043	132.9	22	-50
DDH04-71	508724.67	6481123.5	1073.92	221.3	48.18	-47.98
DDH05-100	508276.8	6481207.62	1153.87	190.8	180.16	-49.97
DDH05-101	505395.456	6482884.279	1336.749	184.7	40.83	-65
DDH05-102	506345.951	6482434.504	1366.166	337.4	219.3	-51.4
DDH05-103	508192.1	6481210.66	1163.27	400.8	180.67	-49.2
DDH05-104	508181.06	6481277.02	1178.39	233.2	175.5	-46.83
DDH05-105	508281.93	6481280.63	1174.16	288.1	189.41	-47.7
DDH05-106	508648.65	6481259.3	1110.69	257.25	184.72	-49.53
DDH05-107	508519.47	6481219.64	1112.16	199.35	179.5	-47.3
DDH05-108	508962.95	6481146.32	1047.28	217.65	192.5	-50.18
DDH05-72	508721.87	6481143.62	1076.71	186.4	181	-63.42
DDH05-73	508288.23	6480976.89	1100.23	152.4	218.63	-48.33
DDH05-74	508829.11	6481127.35	1063.48	223.7	171.35	-48.18
DDH05-75	508938.42	6481338.89	1087.44	217.7	48.82	-49.62
DDH05-76	508513.13	6481312.23	1128.21	223.7	183.87	-47.63
DDH05-77	508382.7	6481333.23	1162.41	223.7	182.43	-47.65
DDH05-78	508099.23	6481147.15	1148.45	147.5	220	-49.12
DDH05-79	507989.59	6481312.85	1180.23	211.3	228.73	-50.5
DDH05-80	507741.69	6481296.02	1192.71	199.4	32.08	-50.22
DDH05-81	507213.487	6481770.476	1284.038	181.4	44.91	-50
DDH05-82	507213.487	6481770.476	1284.038	62.2	224.91	-50
DDH05-83	506528.861	6482326.024	1352.83	172	224.5	-52
DDH05-84	505995.658	6482358.196	1350.069	189.6	46.68	-52
DDH05-85	507741.07	6484040.09	1676.198	140.2	232.21	-52.5
DDH05-86	507508.732	6484239.893	1656.923	129	225.51	-53.25
DDH05-87	506938.064	6484389.522	1665.308	143.25	48.44	-49.75
DDH05-88	505395.456	6482884.273	1336.379	172.2	40.55	-50.5
DDH05-89	505925.463	6482544.446	1356.583	166.1	40.77	-50.75
DDH05-90	508363.05	6481504.93	1185.44	193.55	224.25	-49.37
DDH05-91	509023.24	6481351.37	1081.62	217.95	49.67	-49.57
DDH05-92	508995.35	6481385.63	1082.8	205.75	51.23	-47.48

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH05-93	508910.18	6481099.06	1044.86	202.7	182	-51.13
DDH05-94	508910.17	6481099.84	1044.78	245.7	191.92	-80
DDH05-95	508763.68	6481087.3	1062.85	240.5	182.5	-50
DDH05-96	508659.52	6481150.19	1088.31	211.85	174.75	-49
DDH05-97	508382.48	6481141.45	1136.57	185.3	180.58	-49.2
DDH05-98	508383.52	6481207.3	1143.95	199.65	187	-48.25
DDH05-99	508383.77	6481171.7	1140.03	187.2	183.17	-49.6
DDH06-109	509301.8	6481495.9	1049.7	324.9	180	-84.06
DDH06-110	509117.8	6481501.7	1078.3	285	180	-84
DDH06-111	508897.7	6481503.7	1115.6	297.2	180	-84.07
DDH06-112	508596.4	6481697.9	1175.1	260.9	180	-85.2
DDH06-113	508095.2	6481307.3	1176.6	276.15	195.35	-50.14
DDH06-114	508109.6	6481408.4	1197.4	193.55	193.23	-49.42
DDH06-115	508281.4	6481401	1190.3	243	168.53	-50.37
DDH06-116	508195.3	6481491.6	1202.5	202.7	183.88	-48.16
DDH06-117	508204.4	6481699.7	1224.3	202.7	176.14	-47.57
DDH06-118	508205.1	6481698.7	1224.3	217.95	358.7	-50.2
DDH06-119	508506.3	6480807.9	1041.3	187.45	180.77	-48.1
DDH06-120	508011.5	6481697.8	1239.1	175.25	179.49	-50.11
DDH06-121	507504	6481907.6	1304.8	297.7	183.78	-49.81
DDH06-122	507694.3	6481870.7	1306.4	301	177.1	-49.9
DDH06-123	508489.7	6480922.8	1065.8	265.2	177.78	-48.43
DDH06-124	507606.1	6482000.1	1313.5	230.15	181.54	-48.92
DDH06-125	507812.4	6482013.8	1312.6	381.9	180.39	-50.03
DDH06-126	507593.5	6481612.7	1259.1	501.4	178.23	-48.74
DDH06-127	507476.5	6481712.7	1276.8	367.3	180.49	-49.97
DDH06-128	507695.6	6481544.7	1242.8	92.95	176.9	-47.8
DDH06-128A	507695.6	6481544.6	1242.1	297.2	177.78	-58.8
DDH06-129	509474.651	6482238.889	1094.762	227.1	40.33	-60.7
DDH06-130	509475.448	6482237.402	1096.448	214.9	85.73	-49.9
DDH06-131	509448.9	6481848	1093	388.6	39.78	-50.47
DDH06-132	509504.4	6481915.1	1088.6	266.85	39.31	-49.93
DDH06-133	509507.6	6481917	1088.7	208.8	156.76	-49.16
DDH06-134	509407.4	6481921.6	1101.5	343.5	34.4	-85.78
DDH06-135	507635.672	6484060.985	1676.879	197.2	221.22	-49.9
DDH06-136	507654.31	6484263.878	1652.724	196.9	43.06	-48.6
DDH06-137	507811.303	6484165.356	1647.189	219.74	38.2	-48.5
DDH06-138	507853.055	6484049.305	1651.67	224.65	217.76	-48.2
DDH06-139	508009.612	6483910.46	1607.373	212.45	220	-48.5
DDH06-140	508097.717	6483845.603	1573.11	233.65	219.99	-48.9
DDH06-141	504420.795	6483501.092	1276.527	255.1	30.55	-50
DDH06-142	504419.585	6483496.857	1275.62	245.95	210.55	-50
DDH06-143	504769.638	6483975.363	1402.336	340.45	31.98	-50
DDH06-144	507511.9	6482223.7	1343.7	194.4	40	-83.9
DDH06-145	507668.8	6482297	1355.3	161.6	40	-85.2
DDH06-146	506738.64	6482253.57	1341.3	251.45	179.67	-49.3
DDH06-147	505937.98	6483466.01	1475.38	377.05	40	-50.9
DDH06-148	506101.49	6483388.7	1483.54	139.3	40	-50

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH06-149	505911.96	6483180.07	1435.8	315.45	41.88	-49.5
DDH06-150	506032.27	6483009.63	1428.63	257.6	44.7	-49.8
DDH06-151	509493.5	6480658.8	1058.7	292.55	166.63	-50.19
DDH06-152	509492.2	6480661.7	1058.8	324.6	347.79	-50.27
DDH06-153	509492.3	6480661	1058.6	233.8	347.79	-85.68
DDH06-154	509193	6480544.3	1070.9	298.1	190.54	-63.53
DDH06-155	509543	6480907.8	1040.7	303.9	173.95	-50.2
DDH06-156	509884.5	6480901.4	1081.4	298.1	178	-61.5
DDH06-157	509677.4	6480873.1	1059.1	260.6	178.15	-63.76
DDH06-158	509023.1	6480453.7	1037	161.35	175.6	-57.3
DDH06-159	509186.9	6480661.9	1040.9	330.9	172	-58.6
DDH06-160	505442.82	6482934.05	1349.18	309.4	41.49	-49.1
DDH06-161	505431.81	6482833.59	1338.16	285	41.41	-48.5
DDH06-162	507395.1	6481677.5	1267.2	358.15	178.45	-50.47
DDH06-163	507497	6481599.8	1255.2	339.85	187.67	-49.46
DDH06-164	507596.8	6481501.8	1235.2	349	178.72	-48.83
DDH06-165	507801.4	6481529.4	1232.8	379.45	164.16	-50.01
DDH06-166	507412.8	6481908.2	1300.7	305.7	176.63	-49.17
DDH06-167	507699.7	6481768.5	1277.9	352.65	175.54	-47.93
DDH06-168	509326.3	6481829.4	1090	520	184.42	-84.58
DDH06-169	509288.1	6481988	1118.6	199.95	177.7	-85.55
DDH06-170	509202.1	6481395.4	1052.1	434.5	175.56	-51.5
DDH06-171	507583.8	6481695.2	1269.4	333.75	175.36	-50.02
DDH06-172	509100.8	6481308.1	1052.1	409.95	179.04	-50.31
DDH06-173	509292	6480624.9	1049.6	330.7	183.3	-59.01
DDH06-174	509398	6480688.4	1045.3	349	173.4	-58.2
DDH06-175	509003.1	6480663.9	1020	337.4	181.5	-62
DDH07-176	508837.2	6481189.1	1076.7	337.1	175.1	-47.8
DDH07-177	508513.7	6481311	1128.3	361.8	353.6	-59.3
DDH07-178	508888.8	6481280.3	1083.6	483.1	180.3	-57.6
DDH07-179	508518.3	6481389.8	1145.2	423	179.1	-49.8
DDH07-179a	508519.448	6481394.787	1158.876	0	180.8	-60
DDH07-180	509022.6	6481354	1081.5	419.1	181.4	-48.4
DDH07-181	508634.2	6481354.8	1125.1	394.7	178.9	-48.6
DDH07-182	509299.6	6481374	1031	336.5	182.2	-50.7
DDH07-183	509200.9	6481201.5	1018.8	365.45	170.1	-60.4
DDH07-184	508362.3	6481506.9	1185.2	537.95	178.4	-48.3
DDH07-185	509005.1	6480939.7	1011.7	468.8	175.7	-50.7
DDH07-186	508072.8	6481413.2	1196.5	366.05	180.7	-50.5
DDH07-187	509202.1	6480998	1008	492.55	180.4	-58.8
DDH07-188	508194.909	6481098.062	1148.764	0	179.45	-50
DDH07-189	509500.3	6481557	1029.6	379.5	176.6	-58.5
DDH07-190	508077	6481596.8	1222.8	363.95	174.3	-48.2
DDH07-191	509498.1	6481455.1	1026.9	420.3	175.1	-59.3
DDH07-192	507798.5	6481620.5	1249.7	400.8	178.3	-49
DDH07-193	509702.698	6481499.295	1022.007	0	177.33	-60
DDH07-194	509489.2	6481953.4	1092.9	382.85	38.6	-49.7
DDH07-195	507707.6	6481640.6	1260.1	458.7	177.8	-54.8

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH07-196	507613.3	6481406.9	1220.5	218.85	180.2	-49.3
DDH07-197	507397.6	6481573	1256.3	240.2	177.6	-47.4
DDH07-198	507302.8	6481997.3	1312.3	166.1	177.3	-47.4
DDH07-199	507509.3	6482006.9	1315.4	366.65	179	-47.7
DDH07-200	509500.1	6481767.6	1066.5	312.75	179.6	-59.4
DDH07-201	508735.6	6481504.2	1132.2	666.6	185.9	-67.2
DDH07-202	507405.1	6481798.8	1283.9	341.7	172.4	-48.6
DDH07-203	509707.6	6481672.6	1025.8	453.25	177.6	-59.9
DDH07-204	507484.2	6481813	1287.9	499.25	180.6	-48.4
DDH07-205	507601.5	6481795.6	1285.1	438.4	180	-50.4
DDH07-206	509974.136	6481695.047	1017.406	358.75	69.83	-57.4
DDH07-207	505919.144	6482546.345	1357.219	311.8	189.34	-49.9
DDH07-208	508945.321	6481308.01	1083.107	58.5	180	-75
DDH07-209	505740.869	6482652.644	1354.576	394.1	40	-49.8
DDH07-210	505337.937	6482829.584	1323.158	413	45.75	-50.1
DDH07-211	505337.416	6482829.353	1323.364	276.15	45.75	-68.3
DDH07-212	508671.1	6481246.8	1105.4	137.15	177.3	-70.9
DDH07-213	508865.518	6481203.695	1079.977	56.7	168.3	-60
DDH07-214	505331.921	6482901.219	1325.874	348.7	44.69	-49.1
DDH07-215	508835.8	6481265.9	1084.1	413.3	180.1	-50.1
DDH07-216	506607.846	6483119.019	1506.123	245.05	180	-49
DDH07-217	507955.3	6482011.7	1295.3	403.55	178.6	-49.4
DDH07-218	508605	6481119.6	1088.8	400.5	181.1	-44.8
DDH07-219	507808.2	6481894	1313.3	424.9	180.6	-48.6
DDH07-220	508787.111	6481293.113	1091.48	119.2	180	-59.3
DDH07-221	508787.4	6481293	1092.1	410.85	177	-50.7
DDH07-222	508450.5	6481429.5	1154	412.4	179.5	-50.4
DDH07-223	507706.6	6481932.8	1311.1	403.55	177.8	-49.4
DDH07-224	508832	6481487	1121.7	42.65	180.54	-85
DDH07-225	508832	6481486.3	1122	675.15	178.8	-58.8
DDH07-226	507303	6481691	1267.6	330.1	180.1	-48.7
DDH07-227	508597.8	6481283.9	1117.5	358.75	184.1	-48.8
DDH07-228	507696.4	6481465.5	1225.9	330.1	177.7	-46.4
DDH07-229	508602.3	6481177.3	1095	266.4	182.8	-50.1
DDH07-230	505618	6484204	1630	239.6	180	-60
DDH07-231	505905.246	6484236.244	1633.723	245.05	180	-60
DDH07-232	506369	6483714	1586.92	223.4	180	-60
DDH07-233	507376	6483374	1575	224.95	225	-60
DDH07-234	506765	6483656	1627.7	246.3	180	-70
DDH07-235	507376	6483374	1575	207.5	45	-60
DDH07-236	511185	6481355	1170	230.85	180	-85
DDH07-237	510889	6481643	1125.23	305.1	180	-58.8
DDH07-238	510889	6481643	1125.23	26.5	180	-70
DDH07-239	510889	6481643	1125.23	167.05	180	-85
DDH07-240	510337	6481587	1050	308.45	180	-60
DDH07-241	507806.4	6481783.2	1284.8	398.35	174.7	-48.6
DDH07-242	508391.1	6481051.4	1101.9	300.85	177.8	-48.6
DDH07-243	508942.8	6481698.2	1147.6	416.05	355.2	-49.8

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH07-244	508455.4	6481281.9	1137.7	355.1	179.6	-47.9
DDH07-245	508645	6481071.2	1078.2	286.4	184.4	-45.8
DDH07-246	509042.2	6481284.8	1062.9	351.45	181.8	-52.1
DDH07-247	508895.2	6481509.6	1116.4	355.1	359.2	-49.9
DDH07-248	509036.9	6481211.6	1047.9	352.65	182.3	-48.4
DDH08-249	511004.622	6481593.399	1149.571	370.35	180	-50
DDH08-250	510798.399	6481718.991	1130.682	181.95	181.39	-50
DDH08-251	510337.404	6481745.664	1041.766	0	179.93	-85
DDH08-252	511298.952	6481511.305	1165.016	254.8	178.63	-50
DDH08-253	510907.369	6481451.983	1137.353	273.7	180.48	-50
DDH08-254	508860.4	6481419.5	1103.7	318.5	181.5	-47.9
DDH08-255	508797.2	6481439.3	1114.7	358.15	181.4	-50.7
DDH08-256	508745.6	6481424.7	1122.8	327.65	180.9	-49.7
DDH08-257	508901.4	6481435.9	1103.2	273.4	181.3	-49.5
DDH08-258	508959.7	6481431.4	1092	275.85	180.5	-51.6
DDH08-259	508941.6	6481309.7	1082.6	300.85	180.9	-47.3
DDH08-260	508745.5	6481322.5	1104.9	333.75	178.6	-50.2
DDH08-261	508595.342	6481381.69	1130.513	419.1	179.7	-50.7
DDH08-262	507844.9	6479426.5	1018.9	20.11	177.18	-90
DDH08-263	509128.7	6481155.4	1022.6	152.1	179.4	-89
DDH08-264	508876	6481060.9	1038.5	245.05	358.3	-4.5
DDH10-265	508877	6481060.9	1038.5	179.85	358.3	-4.5
DDH10-266	508875	6481060.9	1038.5	204.2	358.3	-4.5
DDH18-267	508192.648	6481886.288	1237.4835	126.19	180.3	-50
DDH18-268	508065.329	6481766.371	1242.2328	449.89	179.8	-50
DDH18-269	508202.257	6481330.308	1186.8103	221.59	173.6	-75
DDH18-270	507801.569	6481177.718	1169.5199	251.76	359.9	-50
DDH18-271	508158.435	6481561.245	1211.8988	374.6	179.8	-80
DDH18-272	508100.873	6481485.62	1208.5846	289.26	0.2	-80
DDH18-273	507948.828	6481166.556	1157.8566	102.41	181.2	-60
DDH18-274	507952.732	6481504.278	1214.1073	317.6	179.7	-55
DDH18-275	507704.48	6481306.77	1200	71.6	180	-50
DDH18-276	507701.722	6481364.622	1211.3117	404.47	359.7	-55
DDH18-277	508523.514	6481775.278	1189.9196	99.67	179.9	-50
DDH18-278	508461.379	6481769.414	1192.5322	99.97	179.5	-60
DDH18-279	508645.637	6481672.432	1173.7759	151.49	179.8	-50
DDH18-280	508736.498	6481724.672	1174.8224	151.49	179.8	-50
DDH18-281	507951.011	6482125.106	1308.5202	200.25	179.8	-50
DDH18-282	507798.175	6481378.918	1207.8642	468.17	0.3	-60
DDH18-283	507814.078	6482107.939	1314.8282	224.64	180.2	-50
DDH18-284	507714.718	6482098.915	1320.231	215.49	180	-50
DDH18-285	508064.361	6481926.143	1272.972	450.19	180.2	-60
DDH18-286	508380.249	6481723.453	1193.138	333.76	179.8	-50
DDH18-287	507942.058	6481837.576	1284.8462	599	180	-50
DDH18-288	504245	6486190	1568	319.13	0	-90
DDH18-289	507502.35	6481398.932	1226.1087	114.91	180.2	-50
DDH18-290	507489.694	6481497.544	1238.8894	148.44	179.7	-50
DDH18-291	502950	6484800	1295	455.98	40	-67

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH18-292	508889.996	6481285.312	1084.0467	249.02	180.3	-67
DDH18-293	508862.419	6481111.87	1058.752	196.6	19.9	-70
DDH18-294	508722.665	6481201.768	1087.9228	197.51	359.9	-60
DDH18-295	508683.485	6481228.277	1100.8466	236.83	30.4	-60
DDH18-296	508646.427	6481204.37	1095.6497	188.67	0.2	-83
DDH18-297	508562.847	6481209.363	1105.4211	185.62	50.2	-80
DDH18-298	508380.428	6481141.002	1136.7752	252.07	0.3	-77
DDH18-299	508604.724	6481117.454	1089.6392	322.78	0.2	-85
DDH18-300	508948.001	6481139.352	1048.5672	160.63	42.8	-60
DDH18-301	505568.093	6483040.201	1375.1747	584.3	223.8	-55
DDH18-302	508872.745	6481060.6	1038.1867	391.06	329.9	-4
DDH18-303	505575.687	6483039.499	1375.2562	535.53	313.6	-60
DDH18-304	507773.807	6481776.752	1285.2929	242.93	179.7	-55
DDH18-305	507694.657	6481469.64	1225.7932	249.33	180	-85
DDH18-306	507652.891	6481765.92	1277.736	199.95	180.3	-75
DDH67-01	509065	6481052	1015	152.4	25	-35
DDH67-02	509065	6481052	1015	124.05	25	-60
DDH67-03	509065	6481052	1015	123.44	205	-35
DDH67-04	509084	6481112	1021.51	14.33	205	-40
DDH67-05	509084	6481112	1021.51	21.03	205	-55
DDH67-06	509084	6481112	1021.51	114.3	25	-35
DDH67-07	508948	6481203	1063.25	156.97	25	-35
DDH67-08	508948	6481203	1063.25	136.7	25	-60
DDH67-09	508798	6481220	1085	154.53	25	-35
DDH67-10	508798	6481220	1085	152.4	25	-60
DDH67-11	508774	6481253	1090	110.64	25	-40
DDH67-12	508774	6481253	1090	38.4	25	-35
DDH67-13	508774	6481253	1090	10.67	295	-35
DDH70-14	508828	6480514	1015	139	25	-40
DDH70-15	508828	6480514	1015	87.8	215	-60
DDH70-16	508450	6480570	1032.01	122.83	19	-40
DDH70-17	508425	6480905	1074.13	123.44	212	-60
DDH70-18	508425	6480905	1074.13	15.84	212	-30
DDH70-19	508627	6480881	1035	118.87	34	-40
DDH70-20	508649	6480915	1039.26	106.1	22	-41
DDH70-21	507918	6481049	1132.92	201.5	25	-40
DDH70-22	507738	6481169	1176.12	109.73	25	-40
DDH70-23	507297	6481553	1250	122.83	25	-40
DDH70-24	507646	6481655	1260	60.65	25	-34
DDH70-25	507646	6481655	1260	16.2	25	-65
DDH70-26	507683	6481700	1270	77.1	25	-38
DDH70-27	507705	6481692	1270	61.9	25	-38
DDH70-28	507550	6481700	1270.66	93.3	25	-38
DDH96-01	509375	6481308	1010.61	184.4	22	-45
DDH96-02	508638	6480652	1016.25	178.6	290	-60
DDH96-03	508889	6480528	1019.42	137.5	20	-60
DDH96-04	508889	6480528	1019.42	137.5	200	-60
DDH96-05	508889	6480528	1019.42	154.6	290	-60

Hole	UTM East	UTM North	UTM Elevation	Length (m)	Azimuth (°)	Dip (°)
DDH97-01	511509	6481520	1210	160	45	-60
DDH97-02	507098	6484190	1690	190.5	0	-60
DDH97-03	507094	6484219	1685	133.2	0	-50
DDH97-04	507694	6481716	1270	163.7	210	-50
DDH97-05	507694	6481716	1270	130.1	210	-65
DDH97-06	510022	6481718	1014.26	197.2	45	-65
DDH97-07	510132	6481743	1005.71	166.7	5	-60
DDH97-08	508657	6480699	1015.52	220.7	290	-60
DDH97-09	509094.74	6481042.52	1010.26	493.2	345.02	-45.07
DDH98-01	508791.86	6481213.83	1083.73	288	340.7	-57.07
DDH98-02	508793.1	6481215	1085	184.7	170	-56
DDH98-03	508887.1	6481305	1085	203	355	-56
DDH98-04	508965.06	6481154.48	1047.27	292.6	344.63	-56.43
DDH98-05	508673.34	6480928.77	1036.31	295.7	324.75	-57.83

10.1 Collar & Downhole Surveying

HNC planned drill holes in advance and then spotted the collar in the field using a backpack-mounted Trimble differential global positioning system (DGPS). Because of the high magnetic background, HNC set the direction of drilling using foresights and backsights, which were also spotted by HNC staff using a backpack portable DGPS. After completion of the hole, the collar location was resurveyed using the same backpack Trimble DGPS

A Reflex Maxibor® II unit was used for most downhole surveying from 2004 to 2010. Where casing was intact, 2002 and 2003 holes were re-entered and surveyed with the Maxibor II instrument. A number of holes were not surveyed either because they were initial exploration holes drilled outside of the Horsetrail and Northwest zones, damaged or missing casing prevented re-entry, or the survey tool was not available. Where Maxibor II surveys were not conducted, acid dip tests provided limited control on hole orientation.

Giga Metals planned drill holes in advance and then spotted the collar in the field using a Differential Global Positioning System (DGPS). Because of the high magnetic background resulting in magnetic compass inaccuracy, Giga Metals set the direction of drilling using either foresights and backsights spotted by staff using a DGPS, or using a north-seeking Reflex TN14 GyroCompass. After completion of the hole, the collar location was resurveyed using a DGPS; the collar dip measurement was taken from the down-hole survey measurement nearest to the top of the hole. Most casings remain intact with semi-permanent markers. Many pre-2018 collars have had their location, azimuth, and dip surveyed by Gabriel Aucoin (Commissioned Land Surveyor [CLS]) of Aucoin Surveys Limited. Data in the collar table for holes used in the resource estimate are the best available method for each attribute of each hole.

10.2 Significant Assay Intervals

Table 10.3 provides a selection of significant drill hole intervals from the Turnagain drill hole database. Drill hole intervals are reported as actual core lengths and do not represent the true thickness.

The 2018 drill program was focused on metallurgical infill drill holes and infill drill holes for the purpose of potential resource upgrade purposes as follows:

- 13 metallurgical infill holes totaling 3,073.0 metres within the Horsetrail and Northwest zones of the Turnagain deposit (Table 10.4)
- 23 infill holes totaling 5,866.9 metres sited between the Horsetrail and Northwest zones of the Turnagain deposit (Table 10.5)
- two exploration holes totaling 1,119.8 metres in the platinum-enriched Attic Zone
- two exploration holes totaling 775.1 metres in the MAG zone roughly 5.6 kilometres northwest of the Horsetrail zone

The infill drilling program was conducted with two skid-mounted drill rigs in the Horsetrail and Northwest zones. Although these drill holes provide additional geological and resource modelling information, their primary purpose was to collect material of appropriate characteristics for future metallurgical testing. Drill core samples from this program were one-quarter NQ core.

The Attic zone program was comprised of two drill holes (DDH18-301 and DDH18-303) in the platinum- and palladium-enriched Attic zone roughly 3.5 kilometres northwest of the Horsetrail zone.

DDH18-301 was drilled a few tens of meters below a previously intersected platinum- and palladium-enriched, structurally complex, suite of altered clinopyroxenites. The downhole interval of 238.00 m – 260.00 m returned an average of 316 ppb Pd and 355 ppb Pt at a vertical depth of approximately 185 meters.

DDH18-303 was drilled from the same pad but in an untested northwesterly direction toward, and below, nearby Davis Creek to test a suspected fault for enrichment. DDH18-303 returned no intervals of note.

The MAG zone program was comprised of two drill holes (DDH18-288 and DDH18-291) in an area of sedimentary cover rocks with anomalously high total magnetics approximately 5.6 kilometres northwest of the Horsetrail zone and outside the known Turnagain ultramafic intrusion. Both holes did not penetrate through the sedimentary cover and returned no intervals of note.

Table 10.3: Summary of Significant Assay Results for pre-2018 Drill Holes

Hole		From	To	Interval	Ni	Co	Pd	Pt
		(m)	(m)	(m)	(%)	(%)	(ppb)	(ppb)
DDH02-06		230	485.2	255.2	0.32	0.015	56	54
DDH02-06	including	426	428	2	1.03	0.020	463	429
DDH03-16		9.1	369.1	360	0.28	0.017	31	37
DDH03-16	including	196	198	2	1.51	0.080	99	129
DDH03-18		5	242.95	237.95	0.30	0.015	38	38
DDH03-18	including	113	114	1	2.59	0.060	108	128
DDH03-18	and	118	119	1	1.49	0.040	221	175
DDH03-18	and	119	120	1	2.51	0.060	487	409
DDH03-18	and	120	121.2	1.2	2.46	0.060	464	260
DDH03-18	and	121.2	122	0.8	3.93	0.090	1052	833
DDH03-18	and	122	123.2	1.2	5.15	0.130	1067	964
DDH04-23		3.35	413.3	409.95	0.26	0.016	19	20
DDH04-23	including	75.3	76.36	1.06	1.57	0.120	63	59
DDH04-23	and	381.4	382.4	1	1.30	0.110	124	196
DDH04-23	and	382.4	383.4	1	1.27	0.110	132	213
DDH04-23	and	383.4	384.4	1	1.65	0.140	122	148
DDH04-28		123.65	233.15	109.5	0.29	0.020	5	6
DDH04-28	including	135.5	137.2	1.7	0.60	0.050	28	66
DDH04-28	and	137.2	138.15	0.95	1.38	0.110	125	131
DDH04-28	and	138.15	139.15	1	1.25	0.100	53	73
DDH04-28	and	139.15	140.15	1	0.88	0.070	59	58
DDH04-28	and	140.15	141.2	1.05	1.00	0.080	81	60
DDH04-28	and	141.2	142.15	0.95	0.66	0.050	35	65
DDH04-28	and	142.15	145.15	3	0.26	0.020	0	0
DDH04-28	and	145.15	146.6	1.45	1.65	0.100	0	0
DDH04-36		4	120.7	116.7	0.26	0.013	0	0
DDH04-36	including	107.9	109.5	1.6	1.04	0.020	0	0
DDH04-66		6.65	179.2	172.55	0.33	0.020	0	0

DDH04-66	including	154.55	156	1.45	1.63	0.070	0	0
DDH04-67		6.1	145.1	139	0.22	0.019	7	7
DDH04-67	including	115.8	117.65	1.85	1.05	0.050	149	173
DDH06-174		12.4	340	327.6	0.23	0.012	20	23
DDH06-174	including	236	236.3	0.3	1.53	0.150	21	131
DDH07-180		17.9	419.1	401.2	0.24	0.013	25	29
DDH07-180	including	316	316.5	0.5	1.99	0.150	40	54
DDH07-204		7.85	499.25	491.4	0.22	0.014	24	26
DDH07-204	including	488	492	4	1.16	0.030	108	132
DDH08-256		5.3	327.65	322.35	0.24	0.014	26	29
DDH08-256	including	196	200	4	1.12	0.070	28	82
DDH08-258		5.45	275.85	270.4	0.24	0.013	20	22
DDH08-258	including	128	132	4	1.08	0.030	224	231

Table 10.4: Drill Intercepts from the Metallurgical Infill Program

Hole		From	To	Interval	Ni	Co	Pd	Pt
		(m)	(m)	(m)	(%)	(%)	(ppb)	(ppb)
DDH18-292		3.82	249.02	245.2	0.273	0.017	39	43
	including	110	164	54	0.339	0.02	50	44
	and	176	244	68	0.336	0.02	40	40
DDH18-293		8	196.6	188.6	0.27	0.016	24	18
	including	73.47	114	40.53	0.47	0.023	50	39
DDH18-294		6	197.51	191.51	0.374	0.022	69	51
		48	134	86	0.49	0.027	92	66
DDH18-295		52	236.83	184.83	0.32	0.018	35	31
DDH18-296		8	188.67	180.67	0.344	0.021	28	20
	including	44	152	108	0.392	0.022	33	24
DDH18-297		8	185.62	177.62	0.339	0.017	43	38
	including	5.79	63.2	57.41	0.322	0.017	44	41
	and	124	185.62	61.62	0.45	0.016	67	59
DDH18-298		8	252.07	244.07	0.226	0.015	15	13
DDH18-299		8	322.78	314.78	0.214	0.016	17	13
DDH18-300		10	160.63	150.63	0.297	0.019	31	27
	including	32	67.56	35.56	0.381	0.019	45	40
	and	120	160.63	40.63	0.365	0.02	42	36
DDH18-302		3	391.06	388.06	0.257	0.015	41	35
DDH18-304		6	212	206	0.248	0.012	78	72
	including	90	118	28	0.471	0.13	417	367
DDH18-305		8	249.33	241.33	0.213	0.013	17	15
DDH18-306		8	199.95	191.95	0.221	0.013	18	15

Table 10.5: Drill Intercepts from the Infill Program

Hole		From	To	Interval	Ni	Co	Pd	Pt
		(m)	(m)	(m)	(%)	(%)	(ppb)	(ppb)
DDH18-267		4.35	126.19	121.84	0.233	0.013	2	3
	including	48	80	32	0.28	0.013	1	3
DDH18-268		2.85	449.88	447.03	0.258	0.013	15	17
	including	156	268	112	0.281	0.012	4	8
	and	328	449.88	121.88	0.282	0.012	1	3
DDH18-269		2.9	221.59	218.69	0.266	0.013	10	11
	including	92	192	100	0.293	0.014	14	14
DDH18-270		3.9	138.5	134.6	0.185	0.009	8	7
DDH18-271		4	374.6	370.6	0.276	0.013	4	6
	including	276	330	54	0.31	0.012	2	3
DDH18-272		8	289.26	281.26	0.28	0.013	4	8
		72	128	56	0.304	0.013	5	7
DDH18-274		5.79	160	154.21	0.24	0.013	12	15
	including	169.55	180.2	10.65	0.532	0.025	64	63
DDH18-276		64	203.38	139.38	0.232	0.018	18	14
	and	210	243.8	33.8	0.391	0.014	69	48
	and	243.8	404.47	160.67	0.223	0.012	33	25
DDH18-277		5.18	80	74.82	0.239	0.014	43	42
DDH18-278		4	99.97	95.97	0.189	0.012	4	5
DDH18-279		8	151.49	143.49	0.194	0.014	21	20
DDH18-280		5.6	60	54.4	0.265	0.016	109	120
	and	60	151.49	91.49	0.201	0.014	27	29
DDH18-281		10	200.25	190.25	0.235	0.012	2	4
DDH18-282		1.94	103.3	101.36	0.296	0.012	29	31
	and	103.3	224.73	121.43	0.215	0.011	17	14
	and	253	468.17	215.17	0.284	0.014	38	37
DDH18-283		56.95	114	57.05	0.203	0.013	2	5
	and	114	158.1	44.1	0.285	0.013	14	25

	and	172	221.59	49.59	0.242	0.013	7	10
DDH18-284		9.14	215.49	206.35	0.205	0.012	14	21
	including	132	215.49	83.49	0.252	0.013	27	41
DDH18-285		6	450.19	444.19	0.25	0.013	21	22
	including	52	100	48	0.329	0.014	55	57
DDH18-286		6	333.76	327.76	0.208	0.012	21	20
DDH18-287		0	165.85	165.85	0.261	0.014	28	32
	and	180	288	108	0.209	0.013	17	19
	and	288	492	204	0.307	0.015	24	25
	and	492	599	107	0.267	0.013	15	16
DDH18-289		40	114.91	74.91	0.24	0.014	13	19
	including	44.33	48.14	3.81	0.894	0.046	84	203
DDH18-290		88	128	40	0.201	0.013	12	10

11.0 SAMPLE PREPARATION, ANALYSES & SECURITY

This section provides an overview of the sample preparation, analysis, and security procedures used by Giga Metals. Where available, similar information is also provided for Giga Metals' predecessor companies.

Sample preparation and analysis programs have been undertaken by a variety of operators during various drill campaigns. This section summarises the verification work and practices employed by each of the operators. The independent qualified person (QP) responsible for Section 11 of this report, Garth Kirkham, P. Geo., believes that the sample collection, preparation, analysis and security procedures for all Giga Metals' drilling are consistent with industry standards and best practices. This supports their use in mineral resource and mineral reserve estimation as detailed in this study.

11.1 Security & Chain of Custody

The drill contractor transported drill core from the drill site to the exploration camp for processing. Split core samples were numbered, bagged and sealed, and transported from site by helicopter or fixed-wing airplane to Dease Lake (or similarly by plane to Smithers) in 300 to 350 kg lots. The samples were then shipped by commercial transport to a primary preparation facility as follows:

- Acme Laboratories in Vancouver (2003 to 2005) or Smithers (2006 to 2010)
- ALS in Terrace (2018).

Requisition forms were transmitted to the Giga Metals Vancouver office with the date and number of samples shipped, and Acme notified Giga Metals upon receipt of the samples.

Drill core from holes drilled between 1996 and 2002 is stored in racks at the Boulder camp on Wheaton Creek, 15 km west of the property. Core recovered from the 2003 to 2018 programs is stored in sturdy racks, stacked either in neat rows or cross-stacked near the camp on the Turnagain Property. Sample security and core storage conform to industry standards.

11.2 Sampling Methods

Since 1967, multiple drilling and sampling methods have been used by prior operators and Giga Metals and its predecessors. Sampling and logging methods, as well as quality control measures, have varied over this time.

11.2.1 Geotechnical Data

In 2007, Giga Metals contracted Piteau and Associates Engineering Ltd. (Piteau) to provide geotechnical core logging guidance. Piteau provided Giga Metals' geologists with instructions for recording core rock quality designation (RQD), recovery, joint frequency, joint condition, fracture density and orientation, hardness, and weathering. In addition, Giga Metals' geologists collected

over 7,000 point-load tests on core, following the instructions set out by Piteau. During the 2005 and 2006 drill programs, the geotechnical core logging protocol was designed by Knight Piésold Consulting. Geotechnical logging between 2002 and 2004 included RQD and recovery only.

11.2.2 Geological Data

In 2006, Giga Metals established a core logging and sampling protocol that is posted as a flowsheet in the core shack. Prior to any geological logging, the core is realigned, and driller block measurements are converted to metres. Drill core was sampled at 2 m intervals or less during the 2004 and 2005 programs and predominantly on 4 m intervals since 2006, although sample breaks are often inserted at significant changes in lithology or mineralisation. Following core logging, sample intervals are marked with a red or yellow marker and sample numbers are assigned from a pre-printed analytical laboratories sample tag book. Core is digitally photographed three boxes at a time on the logging rack in the core shack. Core samples are halved by a hydraulic core splitter and/or diamond saw. In most cases, half the core is stored in boxes on site and half is sent for analysis. In the case of 2018; however, 13 core samples from 40 holes were halved, and then one half was again split into quarters. One quarter was sent for analysis; one quarter was stored in the box; and the remaining half of the core was stored for future metallurgical testing.

11.2.3 Sample Preparation and Analyses

No information is available regarding sample preparation, analytical procedures, or quality assurance/quality control (QA/QC) measures in place during the 1967-1998 exploration programs. As none of this data was used in resource estimation, this is not considered significant.

Drill core samples from the 2002 to 2010 programs, received by Acme (now Bureau Veritas) in Smithers and Vancouver, BC, were checked against requisition documents prior to being dried, weighed, crushed, split, and pulverised. They were then subjected to a variety of analytical techniques. Acme is a certified ISO:9000 facility. Drill core samples from the 2018 program were similarly processed almost entirely by ALS Laboratories facilities in Terrace, Kamloops and Vancouver, BC; and two batches by TSL Laboratories in Saskatoon, SK. ALS Laboratories is a certified ISO:17025 facility; however, TSL Laboratories is no longer accredited.

Prior to 2004, samples were analysed for nickel, copper, cobalt, and approximately 20 major and minor elements by aqua regia digestion followed by an inductively coupled plasma emission spectroscopy (ICP-ES) finish. Samples collected from the 2004 to 2018 programs were subjected to a four-acid (HNO₃-HClO₄-HF and HCl) digestion followed by ICP-ES analyses to determine values for total nickel, copper, cobalt, and 22 other elements, including sulphur.

In 2004 and 2005, sulphur content was analysed by the Leco furnace method. In 2006, sulphur content was analysed by ICP-ES after a four-acid digestion. Since 2007, sulphur content has been analysed by both ICP-ES after a four-acid digestion, and Leco furnace.

Some exploration drill holes prior to 2004, and all drill holes since 2004, were analysed for platinum, palladium, and gold by lead-collection fire-assay fusion followed by ICP-ES.

11.2.4 Density

Giga Metals collects bulk specific gravity measurements by water immersion method every 20 samples, using up to 50 cm of unsplit core. A protocol for specific gravity measurements is posted in the logging tent.

Specific gravity is calculated as follows:

$$(SG) \text{ specific gravity} = \text{weight in air} / (\text{weight in air} - \text{weight in water})$$

Prior to 2018, data were recorded manually on paper and later transferred to a digital file. Data entry errors due to transposition of numbers or poor written records were possible. AMEC (2007) recommended double data entry for any manual entry of data into a database and suggested that Giga Metals create a density standard to use periodically to ensure the scale is working properly. Since 2008, mass standards have been used to calibrate the scale at least once each day and immersion water replaced periodically to ensure accuracy of measurements. In 2018, data were entered directly upon measurement into an Access database.

11.3 Quality Assurance / Quality Control

Laboratory quality control since 2004 has been maintained by routinely inserting and analysing internal standards, sample blanks, and duplicate samples. Giga Metals geologists also insert reference sample pulps in the field every 20 samples, and blank samples are inserted every 30 samples. Laboratories are instructed to create and analyse duplicate pulps from crushed core every 30th sample. Pulps from every 10th sample are sent to a check laboratory. In 2018, SGS Laboratories in Burnaby was used as a check laboratory to analyse pulps for total nickel, sulphur, platinum, palladium, and gold, among other elements. From 2007 to 2010, International Plasma Laboratories Ltd. (IPL) in Richmond was used as the check laboratory. Prior to 2007, ALS Chemex in Vancouver was used as a check laboratory. At the times of these analyses, SGS was ISO:17025 certified, IPL was ISO:9001 certified, and ALS Chemex was ISO:9001 certified.

Giga Metals' standard reference materials used from 2004 to 2010 for Ni, Cu, and Co include two Canada Centre for Mineral and Energy Technology (CANMET) reference samples labelled UM-2 and UM-4 (Cameron, 1975). Both were derived from small, lenticular masses of peridotite that occur along a major east-west fault zone in the Werner Lake District of northwestern Ontario. CANMET analysed the material for ascorbic acid-hydrogen peroxide soluble nickel and, by use of four-acid digestion, for total Ni content. The CANMET certification of these materials was completed in 1974; however, it is not supported by current industry standards requiring a round-robin approach using several laboratories.

Giga Metals has two reference materials (05-94 and 05-103) prepared from mineralised drill core from the resource area. These standards were initially certified by Smee & Associates Consulting Ltd. through a round-robin process for total digestion nickel, iron, copper, and sulphur. In 2009, AGORATEK International (AGORATEK) supervised a standard recertification program for all four reference materials.

Five other standard reference materials—PGMS-1, ME-1309, and ME-1310 from CDN Labs; and WGB-1, WMG-1 from Natural Resources Canada—have been used for monitoring platinum and palladium concentrations for exploration purposes. However, platinum and palladium quality assurance and quality control are not detailed in this report, as assay concentrations are not economic at this time and not the subject of this resource estimate reported herein.)

For the 2018 drilling campaign, Giga Metals systematically inserted certified reference materials (standards) and blanks into each batch of samples at regular intervals. Samples were placed in sealed bags and shipped directly to the ALS Minerals preparatory laboratory in Terrace, British Columbia. The 2018 samples reported herein were analysed by either ALS Global of Vancouver, British Columbia (“ALS”), or by TSL Laboratories of Saskatoon, Saskatchewan (“TSL”).

Samples prepared by ALS were by crushing the entire sample to 70% passing 2 mm, riffle splitting of 250 grams and pulverizing the split to better than 85% passing 75 µm. Samples prepared by TSL were by crushing the entire sample to 70% passing 1.70 mm, riffle splitting 250 grams and pulverizing the split to 95% passing 106 µm. The core samples also underwent a duplicate assay program that tests rejects and pulps for reproducibility. Samples were also sent to an umpire lab. Base metal analyses were determined using four-acid digestion method with ICP-AES finish. Precious metal analyses were determined by fire assay method with ICP-AES or ICP-AAS finish. Analytical results are verified with the application of industry standard Quality Assurance and Quality Control (QA/QC) procedures.

The performance of the nickel and cobalt standards cumulatively shown for all years is summarised in Figures 11-1 and 11-2, respectively.

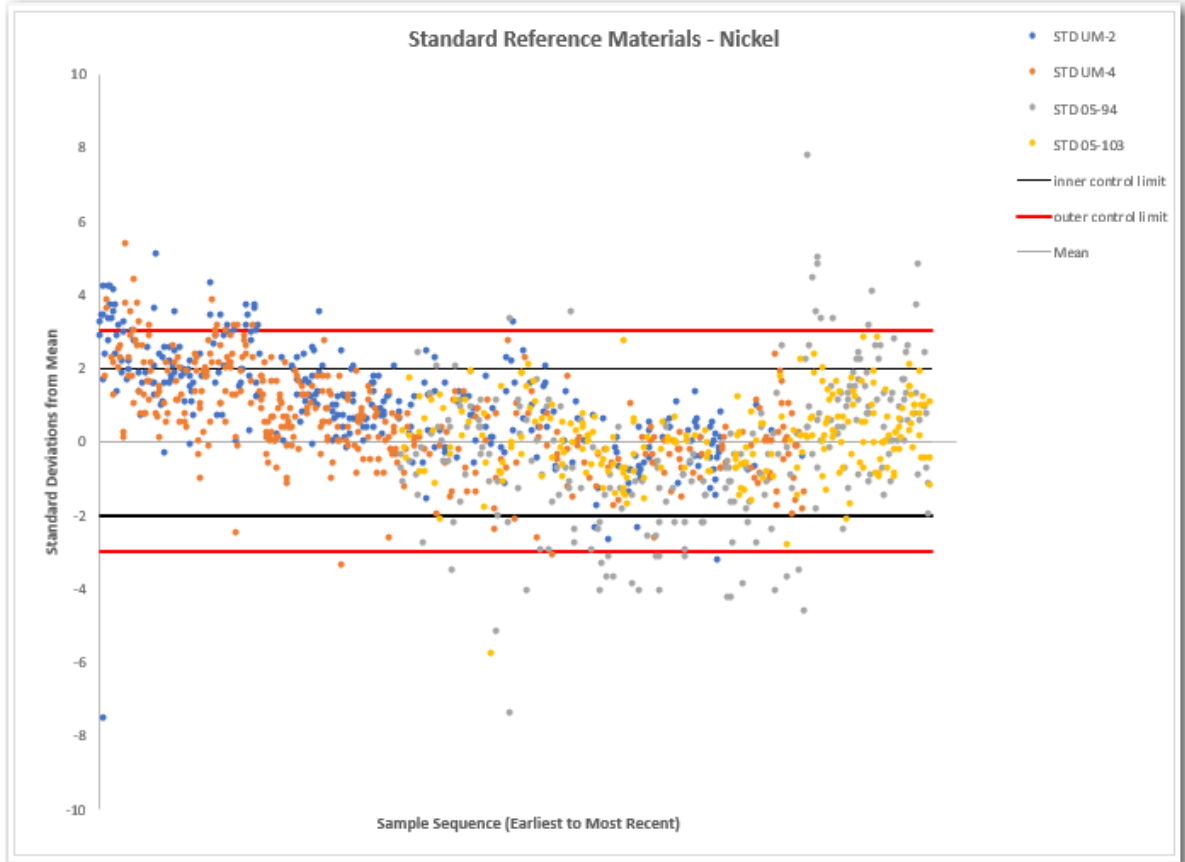
Figure 11-1 shows that early performance of the UM-2 and UM-4 appear to show a high bias that was investigated and resulted in the creation and use of the STD05-94 and STD05-103 standards (which are now the predominant standard). Although there appears to be a high bias, the check lab results during the same period show a correlation of 0.96, which illustrates that the results are repeatable and verifiable. AGORATEK recommended that the 2004, 2005 and 2006 data be adjusted to account for this relatively minor high bias; however, the author believes that this is not warranted and has not applied this arbitrary adjustment to the raw data. The cobalt standards performance shown in Figure 11-2 shows good results, although it is difficult to attain precision due to the very low values that are being measured and the sensitivity of the instrumentation in and around the non-detect ranges.

The source of the field blank used up to, and including, 2005 is not known. The field blank material used from 2006 to 2010 was crushed granite gneiss obtained from Squamish and crushed silica glass. During 2018, a crushed glass blank was used.

11.4 Adequacy Statement

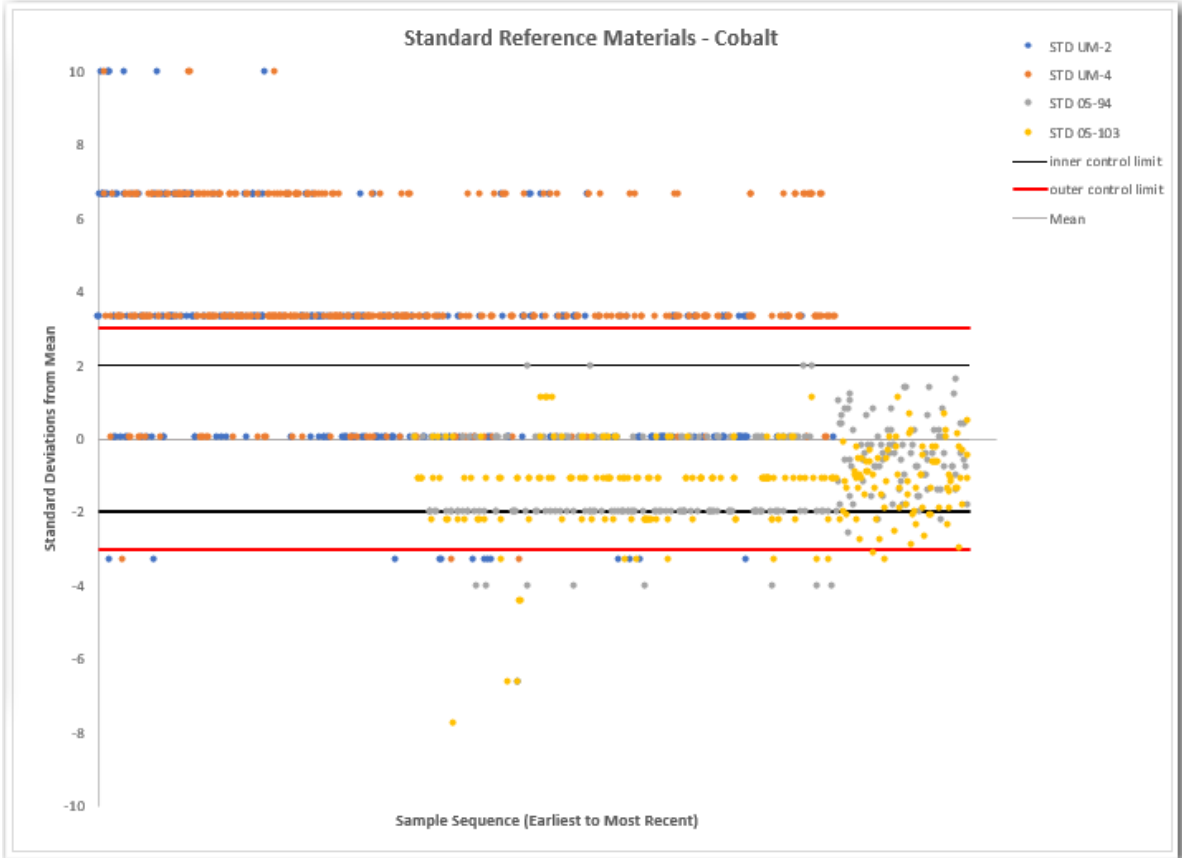
It is the opinion of the QP, Garth Kirkham, P.Geol., that the sampling preparation, security, analytical procedures and quality control protocols used are consistent with generally accepted industry best practices and therefore reliable for the purpose of resource estimation.

Figure 11-1: Nickel Performance of Standard Reference Materials



Source: Kirkham, 2020.

Figure 11-2: Cobalt Performance of Standard Reference Materials



Source: Kirkham, 2020.

12.0 DATA VERIFICATION

12.1 Site Visit & Verification

The qualified person visited the site, facilities and surrounding areas on October 9 to 10, 2018.

The tour of the offices, core logging, and storage facilities showed a clean, well-organised, professional environment. Giga Metals' geological staff and on-site personnel led Kirkham through the chain of custody and methods used at each stage of the logging and sampling process. All methods and processes are to industry standards and best practices, and no issues were identified.

Several complete drill holes were selected by Kirkham and laid out at the core storage area. Site staff supplied the logs and assay sheets for verification against the core and the logged intervals. The data correlated with the physical core and no issues were identified. In addition, Kirkham toured the complete core storage facilities. No issues were identified, and core recoveries appeared to be very good.

The 2018 site visit entailed inspection of the workshops, offices, reclaimed drill sites, the Northwest and Horsetrail mineral resource areas along with the outcrops, historic drill collars, and areas of potential disturbance for potential future mining operations. In addition, the site visit included a tour of the most likely populated area to be affected by any potential mining operation along with surrounding environs. The drilling, logging and sample handling operations were conducted in a professional manner to industry standards and the on-site facilities were clean, well organised and of professional norms.

Kirkham reviewed the geological information from various programs and other relevant data available in the Giga Metals offices and is of the opinion that the programs were conducted and the data gathered in a professional and ethical manner.

Data validation and verification programs have been undertaken by numerous independent consultants as well as Giga Metals personnel, as discussed in previous NI 43-101 technical reports (AMC 2011, AMEC 2007, AGORATEK 2011) and performed subsequently including a database review by Kirkham Geosystems. The independent qualified person responsible for Section 12 of this report, Garth Kirkham, P. Geo., believes that the datasets are validated and verified sufficiently to support their use in mineral resource and mineral reserve estimation for each of the respective deposits.

Kirkham is confident that the data and results are valid based on the site visits and inspection of all aspects of the project, including the methods and procedures used. It is the opinion of Kirkham that all work, procedures, and results have adhered to best practices and industry standards as required by NI 43-101. No duplicate samples were taken to verify assay results, but Kirkham is of the opinion that the work is being performed by a well-respected company that employs

competent professionals that adhere to best practices and standards. Kirkham also notes that authors of prior technical reports (AMC 2011) collected duplicate samples and had no issues.

The datasets employed for use in the mineral resource estimates are a mix of historic data and recent data. There is always a concern regarding the validity of historic data. Extensive validation and verification must be performed to ensure that the data may be relied upon.

Kirkham reviewed extensive validation and verification studies along with procedures performed by external consultants and Giga Metals to ensure the validity of the mineral resource estimates.

It is the opinion of Kirkham that the data used for estimating the current mineral resources for the Northwest and Horsetrail deposits is adequate for this PEA and may be relied upon to report the mineral resources and mineral reserves contained in this report.

13.0 MINERAL PROCESSING & METALLURGICAL TESTING

13.1 Introduction

The Turnagain deposit is a large, low-grade ultramafic deposit containing nickel and cobalt bearing pentlandite and pyrrhotite, as well as minor amounts of chalcopyrite and pyrite. It hosts anomalous levels of platinum and palladium, as well as trace amounts of silver, gold and native copper. The main economic value is in the nickel with some modest cobalt byproduct credits.

The main lithological domains are pyroxenite-dominated, green dunite and wehrlite/ dunite with various degrees of serpentinisation. The pyroxenite lithotype component accounts for less than 10% of the overall deposit tonnage.

A history of the metallurgical testwork conducted until 2010 was summarised in AMEC's 2007 NI 43-101 report, the Wardrop's 2010 Preliminary Economic Assessment NI 43-101 and AMC's 2011 Preliminary Economic Assessment. Work pertinent to the current study is referred to in this report.

Prior to 2010, the focus of mineral processing work was to create a concentrate suitable for on-site hydrometallurgical processing. In this early work, little test data showed the potential to make a high-grade saleable concentrate, while the sheer tonnage of the deposit and the attendant potentially high nickel production rate made inclusion of on-site high-capital hydrometallurgical processing more attractive. In 2010, testing at SGS working in parallel with G&T Metallurgical Services (G&T) started to expose the potential for the production of high-grade nickel concentrates, assaying 15-25% nickel. This led to the preparation of the 2011 technical report.

After a seven-year hiatus in metallurgical testing, work was re-started at Blue Coast Research Ltd. (BCR) in 2018. Initial work was conducted on samples drilled prior to and during 2010 (and stored as drill core under ambient conditions), while work in 2019 has been conducted on samples freshly drilled in 2018. The most recent work is probably the most valuable work supporting the 2020 PEA; however, early work is still of significant value and has been referred to where appropriate.

13.2 Sources of Information for this Study

The key sources of metallurgical information referred to in this study are listed below.

- G&T Metallurgical Services Ltd (2008) Metallurgical Development for the Hard Creek Project, Dease Lake, British Columbia, Canada, Project No. KM2181, October 31, 2008
- Xstrata Process Support (2008) Turnagain Ore Characterisation Project, Phase 1A, Hard Creek Nickel Corporation, Turnagain Project No. 09001823-09010824, Falconbridge, ON, June 17, 2008. This variability study of 17 samples included rougher flotation only.
- SGS Canada Inc. (2019) An Investigation into Flotation Flowsheet Development Testing on the Turnagain Deposit, Report 17124-01, March 6, 2019. This program

was executed in 2010 and 2011 but was only recently reported. It included two separate variability studies: Rougher flotation on 16 variability samples using a soda ash-based flowsheet, and cleaner flotation on 38 variability samples and 2 composites.

- Blue Coast Research (2019) PJ5252 Giga Metals – Turnagain Project Pre-feasibility Study Testwork Report, January 18, 2019. A Study of a master composite including seven locked cycle tests, plus a variability program using 11 samples.
- Blue Coast Research (2019) PJ5280 Giga Metals – Review of Turnagain Metallurgical Flowsheet Development Summary Report, October 2, 2019. As of the end of 2019, work included a preliminary variability program on 24 samples sourced from throughout the deposit, an ongoing optimisation program, two major (16-cycle) locked cycle programs and one regular (6 cycle) locked cycle test.

13.3 Grindability

Turnagain material is hard, with an average SAG grindability (Axb) of 27.1 and a Bond ball mill work index of 19.8 kWh/t, when ground to a closing screen size of 75 µm (see Table 13.1).

Table 13.1: Grindability Data from the Turnagain Project

	# Samples	Mean	85 th Percentile	15 th Percentile
JK SMC				
- A	10	92.5	100.0	79.6
- b	10	0.31	0.41	0.24
- Axb	10	27.1	32.9	23.0
- ta	10	0.27	0.37	0.20
Bond Rod Mill Work Index				
- kWh/t	5	18.6	22.3	14.1
- P80	5	901	925	873
Bond Ball Mill Work Index				
- kWh/t	77	19.8	22.5	14.1
- P ₈₀	47*	83.8	111.1	71.0
Abrasion test	9	0.23	0.38	0.10
Crusher Work Index				
- kWh/t	5	14.2	18.2	10.0

Note: *Not all BWI product sizes have been reported.

For the design criteria, Hatch will typically use values at the 85th percentile for testwork that might not have sufficient samples or show a large standard deviation in value since the mineralized material type may not be well defined.

For testwork that has a high count of samples and +85% confidence interval, Hatch will determine that the testwork for the representative mineralized material type is well defined and the average value can be used for design basis.

The abrasion index used in the design criteria was different from Table 13.1, since previous testwork showed a slightly more conservative value of 0.26.

HPGR testwork was conducted at UBC on five samples at four different forces. The results were then modelled to predict the reduction ratio, specific energy consumption, and product size distribution. The mean and variance data are shown in Table 13.2. The results suggest significant variability in hardness between the five tested samples.

Table 13.2: HPGR Data

	1 N/mm ²	2 N/mm ²	3 N/mm ²	4 N/mm ²
Reduction ratio (F₅₀/P₅₀)				
Mean	4.13	5.59	7.05	8.53
Std. dev.	1.46	2.13	2.81	3.50
Maximum	6.50	9.16	11.83	14.49
Minimum	2.70	3.77	4.83	5.90
Specific energy consumption (open circuit), kWh/t				
Mean	1.41	1.87	2.33	2.80
Std. dev.	0.20	0.26	0.33	0.39
Maximum	1.61	2.15	2.65	3.22
Minimum	1.11	1.47	1.84	2.21
Specific energy consumption (closed-circuit with 6 mm screen), kWh/t				
Mean	2.76	3.22	3.62	4.01
Std. dev.	0.65	0.74	0.79	0.85
Maximum	3.56	4.11	4.51	4.91
Minimum	1.82	2.14	2.45	2.75

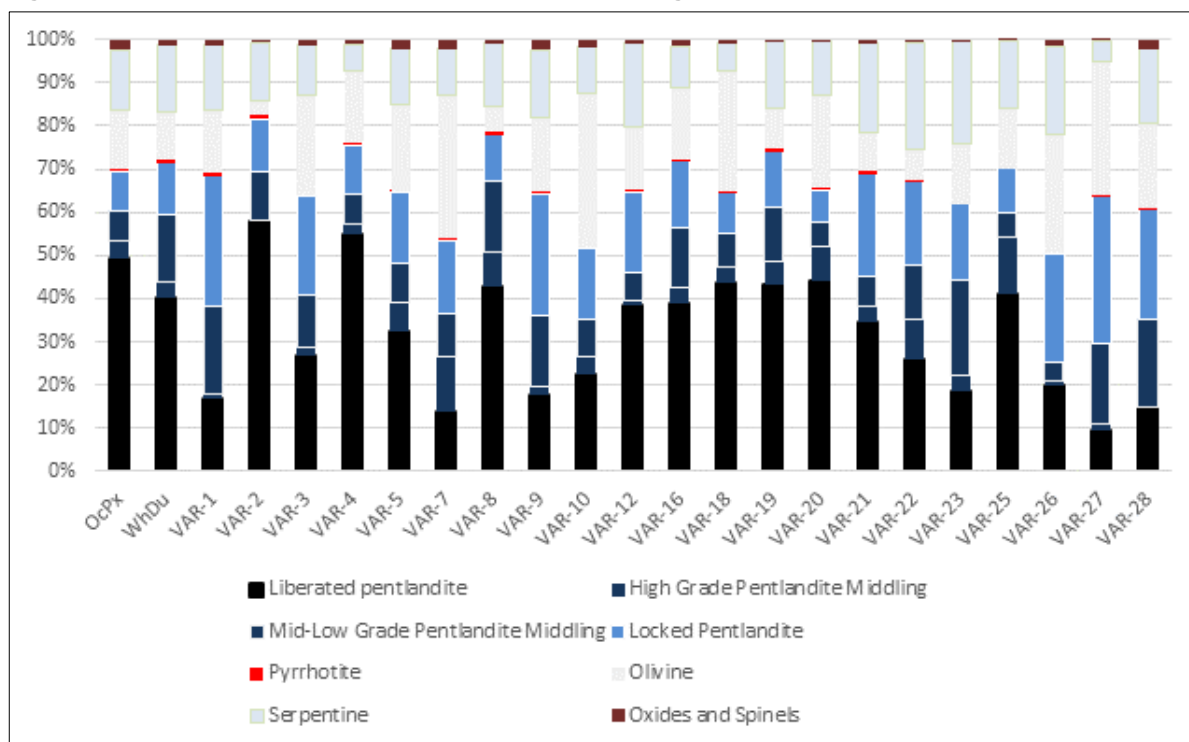
13.4 Mineralogy

Nickel deportment is distributed between pentlandite, pyrrhotite, olivine, serpentine and various oxides and spinels.

Based on QEMSCAN and probe analyses from 23 samples, assaying on average 0.25% nickel and 1.11% sulphur, and located throughout the resource, the average nickel deportment as pentlandite is 66%, with just 0.42% present in pyrrhotite (Figure 13-1). The remainder is present in non-sulphide minerals, on average 17% as olivine and 14% as serpentine. A small amount is contained with oxides and spinels. The presence of nickel as pentlandite is closely linked to the

sulphur assay in the feed, with the samples assaying more and less than 1% sulphur containing 71% and 61% nickel as pentlandite, respectively. Further, pentlandite liberation is linked to sulphur assay, with 78% of the pentlandite being present in liberated or mid/high-grade middling form in samples assaying over 1% sulphur. That number dropped to 66% for samples assaying below 1% sulphur.

Figure 13-1: Nickel Speciation in 23 Samples Tested during 2019



Source: Blue Coast Metallurgy, 2020.

For the current technical report, the only economically recoverable nickel is hosted in pentlandite. At a grind of 80% passing 80 µm, roughly half is liberated (32% of all nickel) and another 4% is hosted in high-grade middlings. If not slimed in grinding, this nickel will float quickly and has the potential to create very high-grade concentrates. Another 12% of the nickel is present as mid- or lower-grade middlings. These should also respond well to flotation. The remaining pentlandite, comprising about 18% of the nickel, is locked in silicates and will be poorly recovered. Typically, these will be mostly recoverable using longer flotation residence times and more collector. The degree of nickel locking suggests that at a grind of 80% passing 80 µm, 80% to 90% of the pentlandite is floatable. As 66% of the nickel is present as pentlandite, this suggests a theoretical nickel recovery ceiling of 55% to 60% based on these 23 samples.

The proportion of nickel present in poorly liberated or locked form, averaging 30% but ranging from 13% to 52%, points to a material that will benefit from fine grinding to achieve good liberation.

However, the comminution-resistant material, and the propensity for the softer pentlandite¹ to slime in such an extreme grinding environment, all conflict with this assumption. Optimising the trade-off in grinding power will be a key step in the Turnagain Project.

Olivine and serpentine are important hosts of nickel that is not economically recoverable by flotation. Pyrrhotite is a very minor host of nickel and its recovery is not economic, so the flotation process has been developed to maximise its rejection to tails.

The median, 95th, 80th, 20th and 5th percentile host rock mineralogy, as determined by QEMSCAN, is shown in Table 13.3. Talc is commonly problematic with mafic nickel ores, as it can be free-floating and contains high levels of MgO, which is challenging for smelters to process. However, the Turnagain deposit is largely free from talc (a small proportion of the samples contained talc at levels that would require significant depressant doses).

Table 13.3: Modal Abundance from QEMSCAN Analysis of 34 Samples Studied by XPS in 2018 & 2019

	Median	95 th Percentile	80 th Percentile	20 th Percentile	5 th Percentile
Pentlandite	0.59	0.97	0.74	0.44	0.28
Chalcopyrite/Valleriite	0.09	0.45	0.19	0.03	0.02
Pyrrhotite	2.8	5.92	3.8	1.0	0.39
Total Sulphides	3.5	7.01	4.6	1.6	0.93
Olivine	29.4	52.85	42.5	19.0	13.30
Serpentine	41.5	69.48	62.5	29.3	25.42
Quartz	0.00	0.01	0.01	0.00	0.00
Feldspar	0.02	0.56	0.17	0.00	0.00
Orthopyroxene	0.05	17.07	0.62	0.02	0.01
Clinopyroxene	11.9	22.53	18.6	2.2	1.14
Amphibole	0.07	1.34	0.32	0.03	0.01
Chlorite	0.36	1.31	0.85	0.09	0.01
Epidote	0.14	0.73	0.44	0.03	0.01
Mica	0.23	1.19	0.66	0.01	0.00
Talc	0.01	3.51	0.04	0.00	0.00
Oxides and Spinel	5.1	7.30	6.4	3.6	3.08
Carbonates	0.14	0.59	0.37	0.09	0.04
Other	0.09	0.16	0.11	0.07	0.05
Total NSG	96.5	99.07	98.4	95.4	92.99

¹ Slimed pentlandite floats particularly poorly.

Pyrrhotite is another potentially problematic mineral, owing to challenges that can occur in separating pentlandite from pyrrhotite. The mass ratio of pyrrhotite to pentlandite, which averages about 5:1, means that pyrrhotite rejection is a requirement for the production of a saleable nickel concentrate. Fortunately, the Turnagain deposit hosts, by nickel industry norms, relatively little pyrrhotite and the pyrrhotite is reasonably easy to reject in flotation. This is a key feature of the mineralisation that allows for production of a superior grade nickel concentrate.

13.5 Flotation

The Turnagain resource is an example of a low-sulphur, nickel-bearing mafic or ultramafic deposit, the treatment of which tends to follow well-established schemes. Recoverable nickel is contained within pentlandite with very minor pyrrhotite, the latter hosting nickel at a grade that is too low to warrant its shipment to smelters. The pentlandite grain size range is moderately fine, but varies widely meaning recovery is quite dependent on primary grind size. Host rock mineralisation is predominantly benign silicates (from a flotation sense) such as olivine and serpentine. Some tested samples have contained a more problematic abundance of talc suggesting that this exists, rarely, within the resource, while one sample out of the 118 variability samples tested since 2007 contained some active carbon. The flowsheet as developed does not handle higher levels of talc or active carbon, rather the much more process-friendly mineral mix, which constitutes the overwhelming majority of samples tested to date.

Typical pentlandite flotation schemes, when present in a low-sulphur host mineralisation, tend to include moderate doses of xanthate collectors and reagents designed to both disperse and in some cases depress the silicates. Raising the pH is only necessary if the pyrrhotite proves to be highly floatable.

In the case of Turnagain flotation, the following principals have been used in flotation flowsheet development:

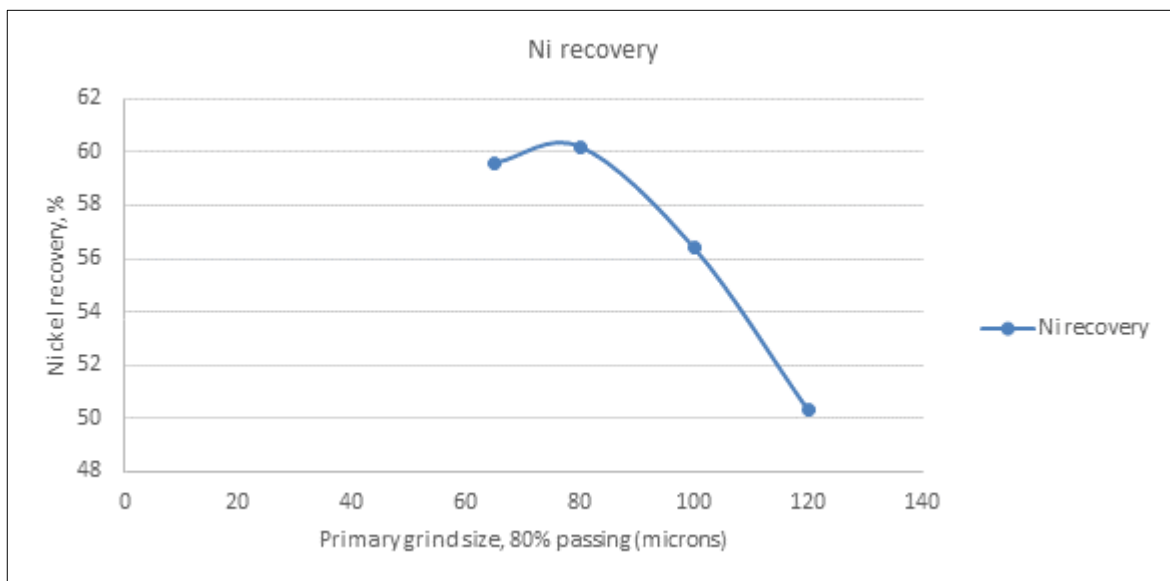
- Pyrrhotite has proven to be poorly floatable with recoveries to final concentrates usually in the range of 3-7%, so pH manipulation is not needed to assist in pyrrhotite rejection. Consequently, flotation is effected at natural pH (pH 8.5-10).
- The silicate mix usually contains little or no talc, so gangue floatability is weak. This eliminates the need for large doses of gangue depressants, although some of the tested treatment schemes have used modest doses of polymeric guar gum and/or carboxymethyl cellulose (CMC) based depressants in testing of Turnagain samples from time to time.
- However, the silicates can interfere with pentlandite flotation, presumably by interacting with the pentlandite surfaces. Hexametaphosphate dispersants, such as Calgon, are widely used to address this and have been adopted for this flowsheet. Calgon enhances pentlandite floatability, but too much also increases the challenge of gangue rejection in cleaning, so they are used sparingly, especially in cleaner flotation.

- Pulp density: The use of dilute pulps has proven advantageous in flotation of Turnagain samples.
- Xanthate is highly effective as a baseline reagent for Turnagain flotation. Isopropyl or isobutyl xanthate both work well. However, adding a secondary collector can be useful in nickel flotation and Turnagain is a candidate for this. Adding the alkyl thionocarbamate collector AERO 3894 at a fraction of the xanthate dose may enhance pentlandite floatability.
- MIBC is used as a frother. The silicate-dominant froths have some degree of inherent stability so strong frothers are not needed, while MIBC volatilises in the process, thereby reducing the risk of frother buildup in latter stages of cleaning.

Primary grind size has a strong influence on nickel recovery. A series of four locked cycle tests were run at different grind sizes in 2018 (Figure 13-2). They pointed to an optimal recovery at about 80 µm. Turnagain material is very hard and grinding costs will be high; however, the steepness of the recovery curve meant that the finer grind was still justified, though grinding finer than 80 µm had a tendency of over-sliming the soft pentlandite, adversely affecting recovery. Therefore, for the design criteria, it is recommended that the target grind size should be between a P₈₀ of 80 to 85 µm.

So far, testwork employing concentrate regrinding has failed to yield improved metallurgy, so the flowsheet includes only grinding prior to rougher flotation.

Figure 13-2: Link between Primary Grind size & Nickel Recovery to Final Concentrate by Locked Cycle Test



Source: Blue Coast Metallurgy, 2020.

Table 13.4, from the latter cycles of the second super cycle test, shows a typical treatment scheme used since 2018 for six-cycle locked cycle and 16-cycle super cycle tests. The latter were 10 kg production runs, run in closed circuit and aimed at producing concentrate for marketing purposes. The composites were created to reflect geologist visual estimates of talc grade, though in reality very little talc has been seen in processing any of them.

Table 13.4: Typical Conditions used in Closed Circuit Flotation Testing at BCR

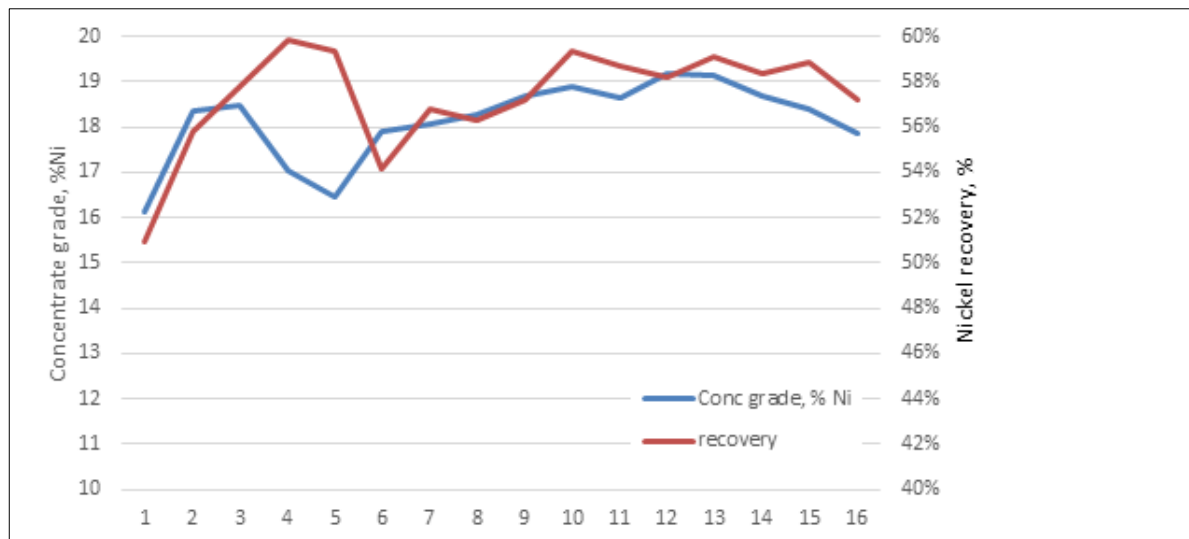
Stage	Reagents (g/t)			Grind (µm)	Time, Minutes	
	Calgon	SIPX	MIBC		Cond.	Froth
Primary Grind	33			80		
Ni Rougher 1		10	16		1	3
Ni Rougher 2	7	10	8		1	3
Ni Rougher 3	7	10	16		1	8
Ni Rougher 4	13	20	32		1	21
Rougher Total	60	50	73	80	4	35
Ni Cleaner 1		18	5		2	15
Ni Cleaner 1 Scavenger						5
Ni Cleaner 2		6	3		1	10
Ni Cleaner 3		3.5			1	9
Ni Cleaner 4		1			1	4
Cleaner Total		29	8		5	43

Metallurgy in this super cycle test stabilised in the second half of the test; the first half being partly used to test different process parameters. During the last eight cycles, nickel recoveries were close to 59%, to a concentrate assaying 18% to 19% nickel (Figure 13-3).

Metallurgical projections from ten locked and super cycle tests run using optimal flowsheets are shown in Table 13.5. All the locked-cycle testwork shown in Table 13.5 has been conducted on samples assaying over 1.1% sulphur and 0.26% nickel; samples lower in nickel and sulphur have been tested in batch flotation.

No recent locked cycle work has been done on low nickel or sulphur samples; the only previous work done at SGS consists of two locked cycle tests yielding recoveries of less than 40% to lower grade nickel concentrates. These tests did not implement many of the process improvements made in more recent testwork, so the data should be interpreted with caution.

Figure 13-3: Nickel Concentrate Grades & Recoveries per Cycle in the Talc 2-3 Super Cycle Test at BCR



Source: Blue Coast Metallurgy, 2020.

Table 13.5: Summary of Locked Cycle Test Data using Optimised Treatment Schemes

Lab	Locked Cycle Test	Feed Grade		Conc. Grade			Ni Recovery
		Ni, %	S, %	Ni, %	Fe, %	MgO, %	
SGS	08-264 LCT 4	0.31	1.15	21.8	34.4	6.6	50.8
SGS	08-264 LCT 5	0.31	1.15	19.4	28.9	9.6	51.0
SGS	10-265 LCT2	0.32	1.15	20.9	32.3	7.1	61.7
SGS	10-265 LCT6	0.32	1.15	20.3	32.9	8.3	63.6
SGS	10-265 Bulk LCT	0.32	1.15	19.7	n/a	n/a	57.9
BCR	10-266 LCT2	0.30	1.26	15.3	38.5	7.4	59.8
BCR	10-266 LCT3	0.30	1.26	18.3	37.6	6.1	60.2
BCR	Litho comp LCT1	0.26	1.14	19.2	30.3	8.4	57.0
BCR	Talc 1, SCT	0.30	1.48	16.4	n/a	n/a	60.5
BCR	Talc 2-3, SCT	0.30	1.44	19.0	n/a	n/a	58.6
Average				19.3			57.8

13.6 Other Treatment Schemes

13.6.1 Two Concentrates

Work has been conducted at different laboratories to explore the potential to produce two concentrates. It has been repeatedly demonstrated that high-grade concentrates in excess of 20% nickel can be produced. Previous tests at BCR have produced premium grade concentrates,

while locked cycle tests at SGS have produced concentrates assaying up to 28% nickel, albeit at 49% nickel recovery. While this concentrate may have a virtually unique quality and may attract premium terms, the key is to produce a second, lower grade concentrate that is still reliably saleable. To date this has not been demonstrated consistently enough to adopt the flowsheet with two concentrates as the baseline process.

13.6.2 Hydrometallurgical Processing

Historically, hydrometallurgical testwork has been completed on lower-grade Turnagain concentrates in four separate testing periods. Work with Cominco Engineering Services Ltd. (CESL) in 1999, as reported in the 2006 AMEC PEA, achieved extractions of nickel and cobalt of approximately 97% and 93%, respectively. Work with Outokumpu in the late 2000s, reported in the 2010 Wardrop PEA, noted chloride leach extractions from a 4% nickel concentrate of 98% nickel and 97% cobalt. Subsequent work on sulphate leach flowsheets was completed at SGS in 2007 and 2008 on concentrate samples grading 4-5% nickel and 10% nickel. This work reported leach extractions of over 97.5% for nickel and cobalt from finely ground concentrates at leach conditions of 110°C to 220°C.

Additionally, one of these test programs by SGS in 2008 demonstrated the complete flowsheet, treating leach solution by iron removal, copper solvent extraction, mixed hydroxide precipitation, and magnesium removal, producing a mixed hydroxide primary product grading over 45% nickel.

Although no hydrometallurgical testwork has been completed on the higher-grade nickel concentrates produced since the mineral processing breakthroughs of 2010-2011 achieved commercial grade concentrates, it is expected that the current Turnagain concentrates would have equal or better performance due to lower levels of impurities.

13.7 Metallurgical Forecast

13.7.1 Introduction & Background

Nickel recovery represents the greatest source of variability for metallurgical forecasting. Concentrate grades of 18-25% nickel have been repeatedly achieved in each study since 2010, and while there is a trade-off between concentrate grade and recovery, a concentrate grade of 18% nickel is consistently achievable, typically at high cleaner circuit recoveries (90% or higher).

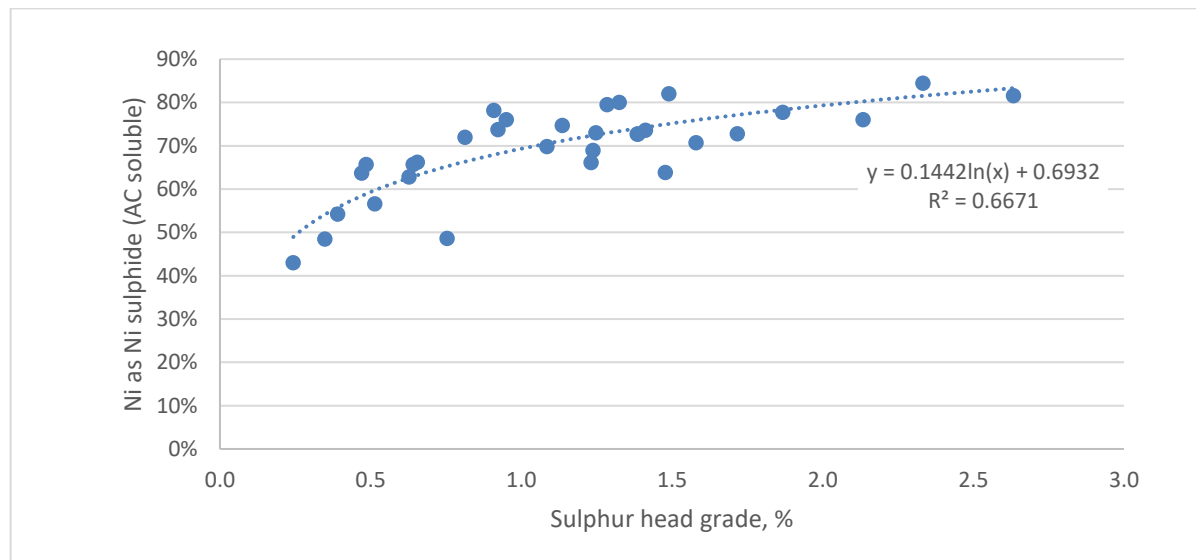
Past studies have recognised nickel recovery as the primary source of metallurgical variability. Work by G&T in 2009 led to the creation of a multi-variate regression driven by the proportion of nickel in sulphide form and the sulphur grade, while the 2010 PEA study employed a metallurgical forecast that was largely based on a nickel head grade/recovery relationship. That study chose to filter out much of the low recovery data on the assumption that they were not optimally tested; however, the weight of additional data points to the presence of samples of lower nickel recovery, making the elimination of these data more difficult to justify.

The present approach recognises that the bulk of the variability in recovery occurs in rougher flotation, while the recovery of nickel from rougher concentrate to final concentrate tends to be quite high and quite consistent. Accordingly, a parameter is first developed to predict rougher flotation recovery.

13.7.2 Rougher Flotation Recovery

As described earlier in this section, nickel is deported within two broad host types, namely (1) pentlandite (recoverable), and (2) non-sulphides (non-recoverable). The distribution of nickel between these hosts is the primary cause of metallurgical variability for the project². Various diagnostic leaches exist that provide some insight into the sulphide and non-sulphide hosted nickel. Ammonium citrate digestion is one of these and has been used in this study as a guide for pentlandite abundance both in metallurgical testing and, to a limited extent, in resource modelling (Figure 13-4). However, the method has a propensity to partially leach some silicate minerals, releasing nickel that is unrecoverable by flotation. This makes it somewhat unreliable and prone to error associated with minor variations in procedure between laboratories.

Figure 13-4: Link between Sample S Assay & Ni as Ni(s) Assay as determined by Ammonium Citrate Method



Source: Blue Coast Metallurgy, 2020.

Sulphur grades perhaps offer a better parameter to predict nickel rougher recovery. It follows from a geological perspective that more sulphidic samples have a higher proportion of sulphide nickel, and hence more recoverable nickel. In fact, data from recent studies at Blue Coast bear this out,

² Pentlandite grain size is probably an additional factor. At this time, its effect on nickel recovery and how it can be modelled in the resource is yet to be established.

where a logarithmic fit can be used to link sulphur assays with the proportion of nickel as a sulphide with reasonable accuracy³:

A data resource comprising the six different variability studies listed earlier and 128 samples has been used to evaluate possible parameters affecting nickel flotation recovery.

Each of these studies employed different rougher and cleaner flotation procedures, leading to different mass pull rates to the rougher concentrate. Driven by flowsheet selection at each laboratory, these varied from 5% to 25% and with them, nickel recoveries varied. Accordingly, the data cannot be combined into a single dataset. However, they provide an opportunity to repeatedly, and independently, explore different candidate parameters driving nickel recovery when each dataset is examined in isolation.

Table 13.6 lists correlation coefficients as determined from each of the study datasets between nickel rougher and cleaner recoveries, and some typical candidate geometallurgical parameters. Total and sulphide nickel head grades are not well connected with nickel recovery. Nickel recovery is somewhat more reliably linked with the proportion of nickel in sulphide form, and better still with sulphur assay in the feed. Study 3a is an outlier to these trends for reasons that are presently not well understood. This has been excluded in calculating the average numbers.

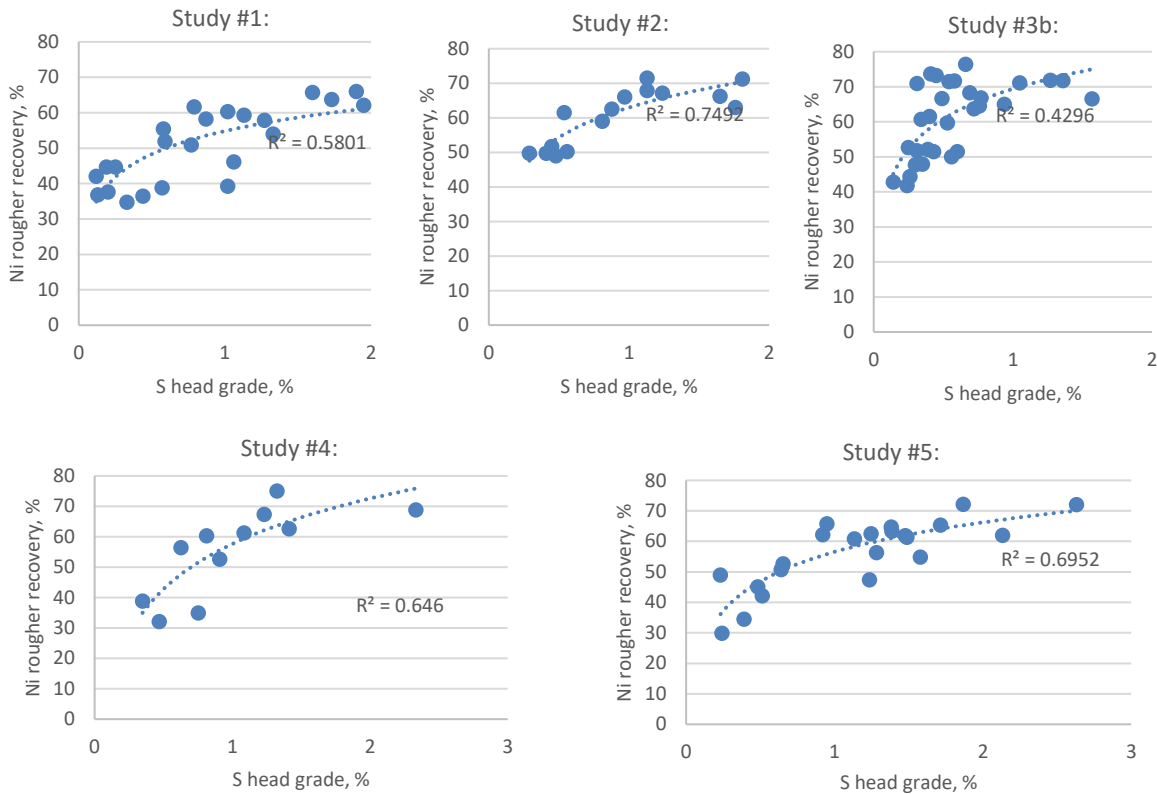
Table 13.6: Correlation Coefficients between Four Candidate Geometallurgical Parameters & Nickel Recovery (R-squared)

Parameter	Study 1		Study 2		Study 3a		Study 3b		Study 4		Study 5		Average	
	Rghr	Clnr	Rghr	Clnr	Rghr	Clnr	Rghr	Clnr	Rghr	Clnr	Rghr	Clnr	Rghr	Clnr
Ni Head Grade	0.01	0.05	0.04	n/a	0.20	0.21	0.01	0.04	0.18	0.05	0.03	0.02	0.05	0.04
Ni(s) Head Grade	0.10	0.27	0.26	n/a	0.23	0.20	0.41	0.17	0.37	0.12	0.43	0.35	0.31	0.23
S Head Grade	0.58	0.80	0.75	n/a	0.17	0.07	0.45	0.56	0.65	0.50	0.70	0.64	0.63	0.63
% Ni as Sulphide	0.63	0.38	0.36	n/a	n/a	n/a	0.58	0.50	0.58	0.25	0.67	0.68	0.56	0.45

Relationships between the sulphur head grade and the recovery of nickel to the rougher concentrate from Studies 1, 2, 3b, 4 and 5 are shown in Figure 13-5. While none of the relationships is tight, they are all quite similar, making sulphur grade a consistent if somewhat crude indicator of nickel recovery. The degree of scatter in the relationships points to the presence of as-yet undetermined additional factors affecting nickel recovery, pointing to the need for more in depth geometallurgical work in the future as the project progresses.

³ The nickel sulphide assays were all completed by the Blue Coast assay laboratory.

Figure 13-5: Regression Analysis of Feed Sulphur Grade & Nickel Rougher Recovery⁴ from Five Variability Studies

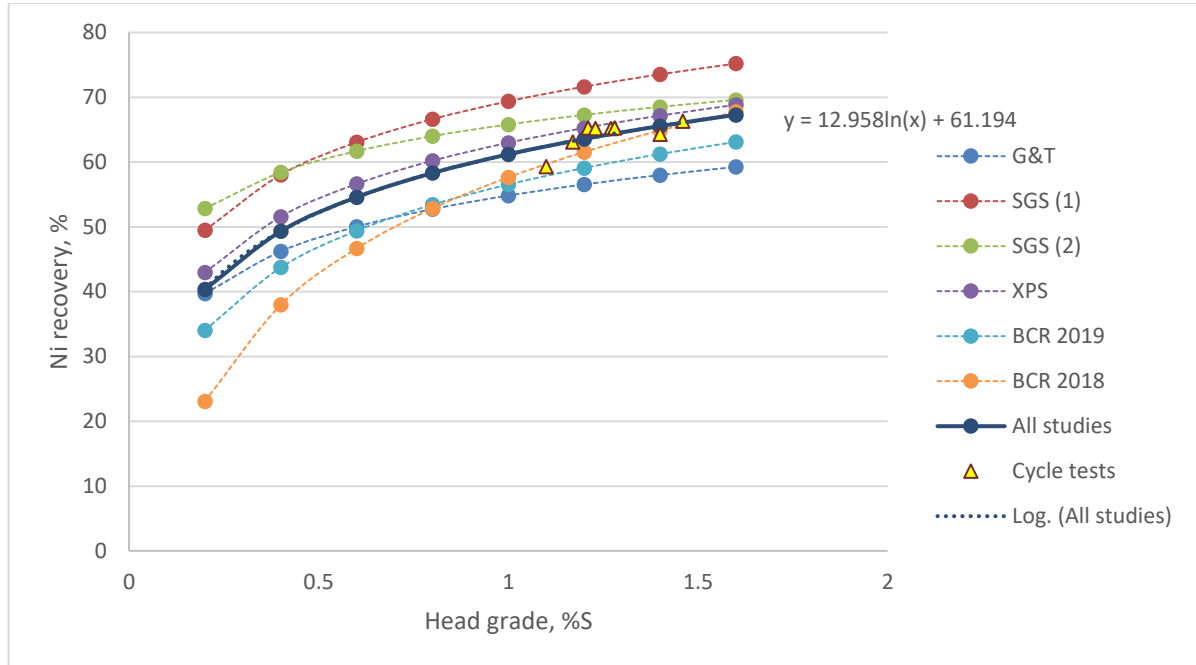


Source: Blue Coast Metallurgy, 2020.

Each of the regression fits are described by logarithmic equations. Plotting the logarithm curves from each of these variability studies on the same graph reveals a series of S grade vs. Ni rougher recovery curves that, for the most part, run parallel with each other (Figure 13-6). As described earlier in this section, the offset between them is due to the different flowsheets used for each of the programs, and the resulting rougher mass pull rates, which varied from an average of 5% to 25%.

⁴ Nickel cleaner recoveries are based on mill feed.

Figure 13-6: Algorithms Fitting S Head Grade vs. Ni Rougher Recovery from the Five Variability Studies



Source: Blue Coast Metallurgy, 2020.

For this study, the sulphur head grade/Ni rougher recovery relationship used for metallurgical forecasting was nominated to be the mean from all the different datasets. This was established at:

$$Ni\ rougher\ recovery\ (\%) = 12.958 \times \ln [sulphur\ head\ grade\ (\%)] + 61.194$$

To check the validity of this curve, average rougher recoveries were plotted against sulphur grades from a host of locked cycle tests and super-cycle tests. As each of these tests consists of between 6 and 16 rougher flotation tests making them statistically robust, and as they were all on composites of material sourced from around the resource, they represent a good quality check of the proposed curve. They are shown in Figure 13-7 as triangles and coincide well with the chosen curve, so validating the rougher recovery relationship.

The reader should be aware that the reliability of the data declines at lower feed sulphur grades, as (1) there is no locked cycle data to validate cleaner performance for samples below 1% sulphur, (2) the best quality data, which is from the most recent studies, contained a paucity of data points below 0.5% sulphur, and (3) the flowsheets have been developed for sulphur grades in excess of 1% and are believed to be less than optimal for lower feed sulphur grades. As such application of the regressions on feed sulphur grades below 0.5% sulphur for the sake of financial forecasting is not recommended.

13.7.3 Recovery to Final Concentrate

Data from the same locked cycle tests and super cycle tests can also be used to establish the cleaner stage recovery of nickel from rougher concentrate to final concentrate. Four of the five tests exhibited quite similar cleaner stage recoveries varying from 88% to 92%, with just one test being higher, at 96%.

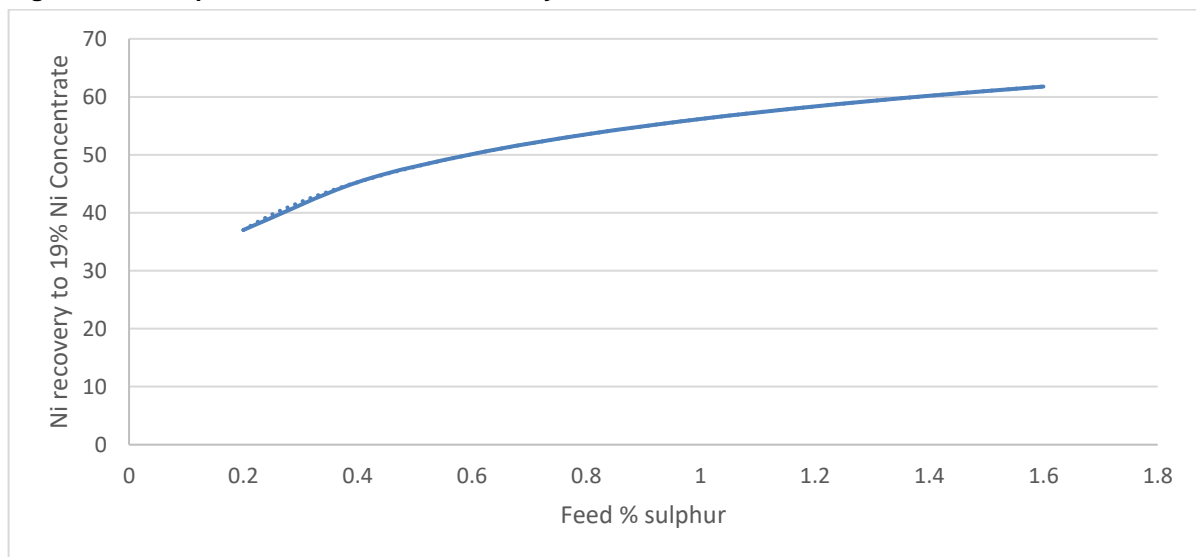
There is inadequate evidence to indicate any relationship between Ni or S grade, or any other tested parameter, and cleaner stage recovery, so a fixed recovery has been assumed, to be the average from the five tests (91.8%). The recoveries are shown in Table 13.7.

Table 13.7: Cleaner Stage Recoveries from Five Recent Locked & Super Cycle Tests

	% Ni	Final Conc.	Rougher	Cleaner Stage Recovery
LCT1: 2018	19.2	57.4	65.3	87.9%
LCT3- 2018	18.3	59.8	65.2	91.7%
SCT Talc 1 – 2019	17.4	60.9	66.2	92.0%
SCT Talc 2-3 – 2019	19.0	58.6	64.1	91.4%
LCT1 – 2019	19.2	57.0	59.3	96.1%
Average	18.6	58.7	64.0	91.8%

Applying this cleaner recovery factor to the regression curve for rougher flotation yields the following S head grade vs nickel recovery curve, to a concentrate grade of 18.6% nickel, as shown in Figure 13-7.

Figure 13-7: Sulphur Grade vs. Nickel Recovery to Final Concentrate



Source: Blue Coast Metallurgy, 2020.

The respective curve, and therefore the equation used for recovery forecasting for this study, is:

$$Ni \text{ recovery to } 18\% \text{ Ni concentrate} = (12.958 \times \ln [\text{feed sulphur}(\%)] + 61.194) \times 0.918$$

13.8 Final Concentrate Specifications

Multi-element scans have been conducted on saleable nickel concentrates with grades close to the expected life-of-mine product, from five different locked cycle tests on different samples and composites. The average for each element from the dataset is shown in Table 13.8.

Table 13.8: Average Assay of 39 Elements in Five LCT Concentrates

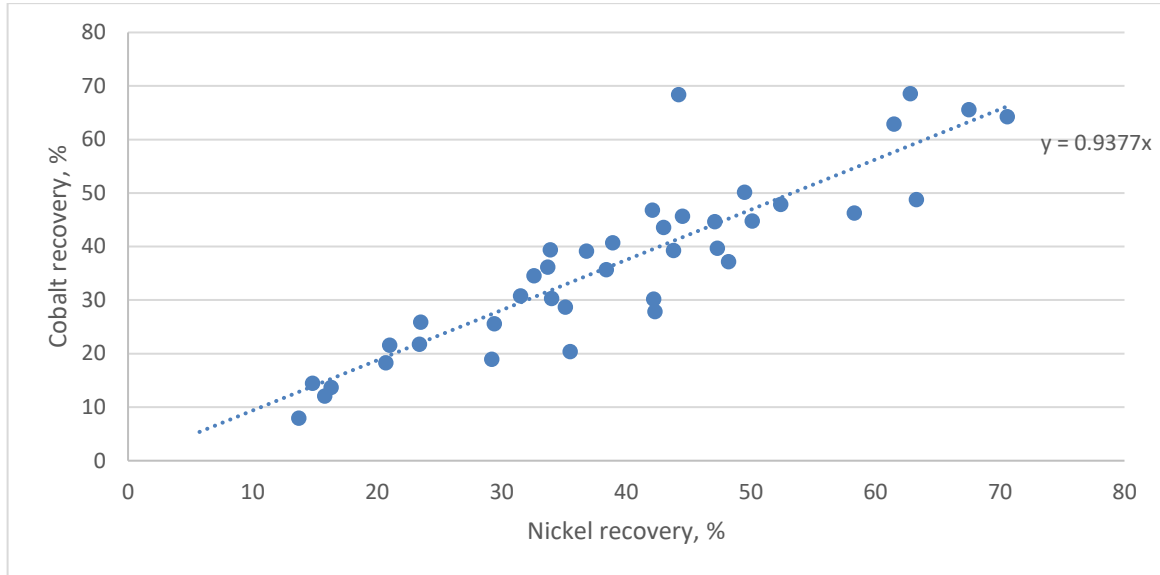
Element	Assay	Element	Assay	Element	Assay	Element	Assay
Ni %	19.7	As %	<0.001	F %	<0.01	Se g/t	78.4
Co %	1.2	Ag g/t	9.4	Hg g/t	0.7	Sn g/t	<20
Cu %	0.46	Al %	0.56	K %	0.09	Sr g/t	24
Fe %	32.3	Ba g/t	81	Li g/t	< 5	Te g/t	<60
S %	25.9	Be g/t	1	Mn g/t	280	Ti g/t	210
SiO ₂ %	6.4	Bi g/t	<20	Mo g/t	53	Tl g/t	<60
Mg %	4.4	Ca %	0.48	Na g/t	540	U %	<0.005
Pt g/t	1.1	Cd g/t	<3	P g/t	<100	V g/t	48
Pd g/t	2	Cl g/t	67	Pb g/t	380	Y g/t	2.1
		Cr %	0.1	Sb %	<0.002	Zn g/t	210

Pentlandite hosts both cobalt and palladium, such that for any given sample cobalt recovery equates to roughly 93.8% of nickel recovery (Figure 13-8).

The assay ratio of cobalt to nickel is quite consistent at 0.6% Co per 10% Ni, and that of palladium is 1 g/t Pd for every 10% Ni. Platinum roughly follows palladium at 0.5 g/t Pt for every 1 g/t Pd.

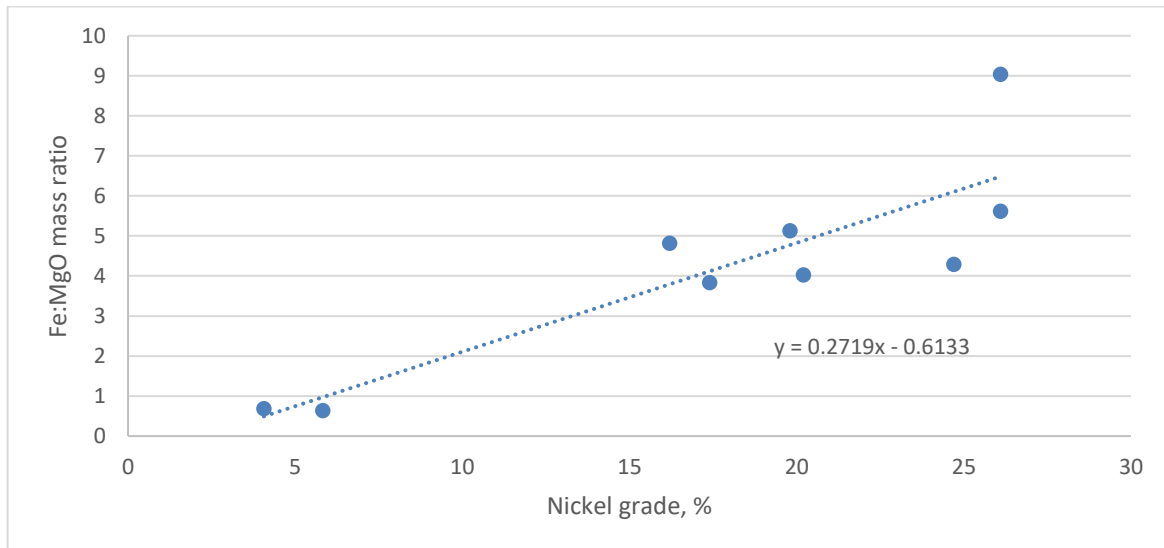
The relationship between nickel grade and Fe:MgO ratio is shown in Figure 13-9. The assay ratio of Fe:MgO is a key criterion in the marketability of many nickel flotation concentrates, as it impacts metallurgy in nickel smelting. This is described further in Section 19, Market Studies and Contracts.

Figure 13-8: Cobalt Recovery vs. Nickel Recovery



Source: Blue Coast Metallurgy, 2020.

Figure 13-9: Relationship between Ni Grade & Fe/MgO Ratio



Source: Blue Coast Metallurgy, 2020.

13.9 Recovery Methods & Equipment Selection

The process recommended to Hatch for plant design includes primary comminution to 80% passing 85 μm . Subject to successful resolution of any dust handling issues when crushing dry, potentially fibrous Turnagain materials, the suggested comminution process would involve crushing using high-pressure grinding rolls, followed by tumbling and/or stirred milling technologies to achieve the final primary grind size.

For this study, rougher flotation would employ conventional tank cell flotation technology, although future consideration should be given to newer flotation technologies (e.g., Woodgrove SFR technology) as a substitute for early-stage rougher flotation. This may lower capital costs, will likely lower operating costs, and may enhance final concentrate grades. In our experience, with slower floating sulphides tank cells are still needed after SFR flotation to ensure optimal recoveries. This requires testing prior to being included in the design, so the more conservative all tank cell option has been adopted for this study.

Relatively low pulp densities have been included, reflecting test results that have indicated that a more dilute pulp yields better rougher metallurgy. At the designed tonnages, this is an expensive option, so more testing and analysis are warranted. The residence time reflects laboratory residence times in an 8 L cell scaled up by a factor of 2.2, which is industry practice for such applications.

No regrinding is recommended at this stage. Regrinding is being tested, but no recent data have indicated any advantage can be gained from its use.

It is recommended that concentrate cleaning is conducted in three stages in the plant using conventional mechanical flotation cells throughout. Column or Jameson Cell flotation could offer advantages, but would need to be tested in a pilot plant, as for the most part they have not been successful commercially in nickel flotation (due to poor recoveries). Mechanical cells represent a safe selection, but using them may forego some upside in concentrate grades (although they will still match what is achieved in the laboratory). The residence time scale up factors for the first cleaner and cleaner scavenger circuit are average (1.8 x) and high (3 x) respectively. Past experience from benchmarking operating plants against lab or pilot plant cells has shown that slower floating material, as found in the cleaner scavenger flotation stage, requires a bigger scale-up factor to the plant due to the lower energy intensity employed commercially.

The second and third cleaner stage scale-up times are 3:1. This is quite high, but the higher residence time mitigates against the use of just three cells at each stage and resulting potential for short-circuiting to tails.

14.0 MINERAL RESOURCE ESTIMATES

14.1 Introduction

The purpose of this report is to document the resource estimations for the Turnagain deposit. This section describes the work undertaken by Garth Kirkham, P.Ge., of Kirkham Geosystems Ltd., and includes key assumptions and parameters used to prepare the mineral resource models for Northwest and Horsetail zones in addition to extensions of the Duffy and Hatzl zones, together with appropriate commentary regarding the merits and possible limitations of such assumptions.

The Mineral Resource Statement presented herein represents an updated mineral resource evaluation prepared for Giga Metals in accordance with the Canadian Securities Administrators' NI 43-101.

This section describes the mineral resource estimation methodology and summarises the key assumptions. In the opinion of qualified person Garth Kirkham, P.Ge., the mineral resource estimates reported herein are a reasonable representation of the mineral resources found within the project at the current level of sampling. The mineral resources were estimated in conformity with generally accepted CIM guidelines ("Estimation of Mineral Resources and Mineral Reserves Best Practices Guidelines", December 2019) and are reported in accordance with NI 43-101 guidelines. It is important to note that mineral resources that are not mineral reserves do not have demonstrated economic viability. Mineral resource estimates do not account for mineability, selectivity, mining loss and dilution. These mineral resource estimates include inferred mineral resources that are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. It is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated.

The Turnagain resource model includes the southern portions of the Horseshoe zone which abut and underlie the Turnagain River, and the Hatzl zone south of the river. These zones are potentially exploitable with a diversion of a relatively short section of the Turnagain River, which Giga Metals is advised is technically viable. These zones are not included in the current mine plan, as the diversion of the river is not currently contemplated.

The mineral resource evaluation reported herein for Turnagain is current and supersedes earlier mineral resource estimates completed for Hard Creek Nickel Corp. including:

- Preliminary Economic Assessment Technical Report for the Turnagain Project, December 2011 (AMC, 2011).

The mineral resource estimates were prepared, reviewed and verified by Garth Kirkham, P.Ge., the independent qualified person for the mineral resource estimates included in this report. Giga Metals' field work on the Project from 2018, including drilling, was carried out under the supervision of Greg Ross, P.Ge., who is Giga Metals' senior geologist.

The general mineral resource estimation methodology for the deposit involved the following procedures:

- database verification and validation
- data exploration, compositing and evaluation of outliers
- construction of estimation domains
- spatial statistics
- block modelling and grade interpolation
- mineral resource classification and validation
- assessment of “reasonable prospects for eventual economic extraction”
- preparation of the mineral resource statement

14.2 Data

The 362 drill holes in the database were supplied in electronic format by Giga Metals, 307 of which had assay values. However, for the purpose of the resource estimation, 240 drill holes are used which lie within the study area and are supported by supportable quality assurance/quality control data, validation and verification. This drill hole subset forms the basis for the resource estimation, herein. This included collars, downhole surveys, lithology data and assay data of varying vintages and analysis types.

Prior to 2004, samples were analysed for nickel, copper, cobalt, and approximately 20 major and minor elements by aqua regia digestion followed by an inductively coupled plasma emission spectroscopy (ICP-ES) finish. Samples collected from the 2004 to 2018 programs were subjected to a four-acid ($\text{HNO}_3\text{-HClO}_4\text{-HF}$ and HCl) digestion followed by ICP-ES analyses to determine values for total nickel, copper, cobalt, and 22 other elements, including sulphur. Drill holes drilled prior to 2018 were also analysed by a ‘sulphide-specific, partial leach’ ammonium citrate-hydrogen peroxide method, followed by ICP-ES finish for Ni, Cu, Cu, Mg and S (the AC method).

In 2004 and 2005, sulphur content was analysed by the Leco furnace method. In 2006, sulphur content was analysed by ICP-ES after a four-acid digestion. Since 2007, sulphur content has been analysed by both ICP-ES after a four-acid digestion, and Leco furnace.

Some exploration drill holes prior to 2004, and all drill holes since 2004, were analysed for platinum, palladium, and gold by lead-collection fire-assay (FA) fusion followed by ICP-ES.

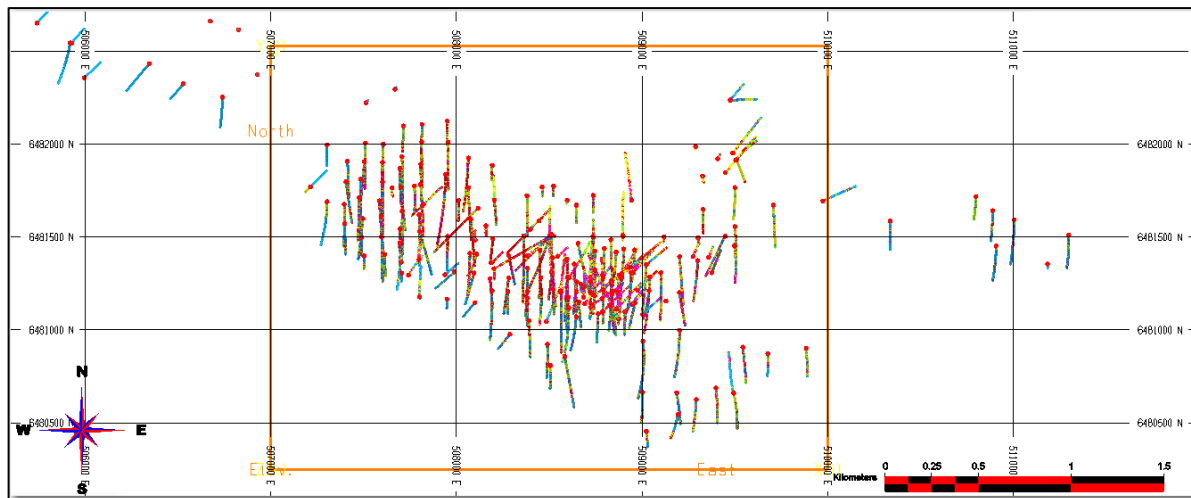
Table 14.1 lists the elements and analyses namely FA (Au, Pt, Pd), AC (Ni, Co, Cu, Mg), ICP (26 element) and LECO (S) along with a listing of ‘best’ values which refers to the final to be used when multiple vintages and methods are in the database. Table 14.1 shows the list of valid elements and analyses methods.

Table 14.1: List of Analysis Elements & Method

ELEMENT	VALUE		
Ag_ICP_ppm	x		
Al_ICP_pct	x		
As_ICP_ppm	x		
Be_ICP_ppm	x		
Bi_ICP_ppm	x		
Ca_ICP_pct	x		
Cd_ICP_ppm	x		
Co_ICP_ppm	x		
Cr_ICP_ppm	x		
Cu_ICP_ppm	x		
Fe_ICP_pct	x		
K_ICP_pct	x		
Mg_ICP_pct	x		
Mn_ICP_ppm	x		
Mo_ICP_ppm	x		
Na_ICP_pct	x		
Ni_ICP_pct	x		
P_ICP_pct	x		
Pb_ICP_ppm	x		
S_ICP_pct	x		
Sb_ICP_ppm	x		
Sr_ICP_ppm	x		
Ti_ICP_pct	x		
V_ICP_ppm	x		
W_ICP_ppm	x		
Zn_ICP_ppm	x		
ELEMENT	VALUE	ELEMENT	VALUE
		Au_FA_ppm	x
		Pd_FA_ppb	x
		Pt_FA_ppb	x
		S_LECO_pct	x
		Ni_AC_pct	x
		Co_AC_pct	x
		Cu_AC_pct	x
		Mg_AC_pct	x
		S_Best_pct	x

Validation and verification checks were performed during importation of data to ensure there were no overlapping intervals, typographic errors or anomalous entries. None were found. Figure 14-1 shows a plan view of the supplied drill holes.

Figure 14-1: Plan View of Turnagain Drill Holes & Model Limits



Source: Kirkham Geosystems, 2020.

14.3 Data Analysis

Statistics were run to evaluate the elements of primary potential economic and geometallurgical interest namely Ni%, NiAC%, Co%, CoAC%, Cu%, CuAC%, Mg, MgAC%, Fe%, Pt ppm, Pd ppm, S%, S% (Leco), Au and Ag. The primary economic contributor is shown to be nickel content whilst the secondary is cobalt. The relative concentrations of platinum, palladium, gold and silver are very low and considered not to be economic at this time and although not the subject of this resource estimate and not reported, they have been estimated. However, they may be payable depending upon mineral processing and concentrate treatment methods and terms. The NiAC%, Mg, MgAC%, Cu, CuAC%, CoAC%, Fe%, S% and S%(Leco) have similarly been analysed and estimated on a block by block basis which are useful from a geometallurgical standpoint. However, they are not reported within the resource statement.

The statistical analysis was grouped by lithology as logged by the site geologists and supplied in the database. The lithology codes and descriptions are listed in Table 14.2. There was only one occurrence of Bx (breccia) and SMS (semi-massive sulphide) so they are not listed.

Table 14.3 details the statistical analyses for Ni% and Co% for each of the individual lithologic units. Note that a large percentage of the data is associated with the Wehrlite, Dunite, Serpentinite, and Green Dunite lithologies which range in mean grades between 0.2% and 0.25% nickel followed by the Pyroxenites which are lower grade at approximately 0.11% - 0.2% nickel. However, the mean cobalt grades are consistently in the 0.011% - 0.014% range for all.

In addition, the coefficients of variability for nickel, cobalt and sulphur are all very low for all lithology units which indicates very low variability and risk. The coefficient of variation is defined as $CV = \sigma/m$ (standard deviation/mean) and represents a measure of variability that is unit independent. This variability index can be used to compare different and unrelated distributions.

Table 14.2: Lithology Codes & Descriptions for Statistical Grouping

Lithology	Description
cPx	Clinopyroxenite
CS	Calc-Silicate
Di	Diorite
Dk	Dyke
Du	Dunite
flt	Fault
gDi	Granodiorite
gDu	Green Dunite
GS	Graphite-Sulphide
Hb	Hornblendite
hbcPx	Hornblende Clinopyroxenite
Hfs	Hornfels
Inc	Inclusion
MS	Massive Sulphide
MSD	Metasediment
mtcPx	Magnetite Clinopyroxenite
MV	Metavolcanics
ocPx	Olivine Clinopyroxenite
Ovb	Overburden
Phy	Phyllite
Sp	Serpentinite
Um	Undifferentiated Ultramafic
Wh	Wehrlite

Source: Kirkham Geosystems, 2020.

Table 14.3: Statistics for Nickel, Cobalt & Sulphur

Lith	Lith Code	Value	Valid	Length (m)	Min	Max	Mean	SD	CV	Ni:S	Lith	Lith Code	Value	Valid	Length (m)	Min	Max	Mean	SD	CV	Ni:S	Lith	Lith Code	Value	Valid	Length (m)	Min	Max	Mean	SD	CV	Ni:S
cPx	100	NI	1,987	3,648.4	0.001	1.051	0.074	0.087	1.2		Hb	109	NI	914	1,761.8	0.001	0.210	0.019	0.026	1.4		ocPx	101	NI	2,920	5,836.9	0.003	5.148	0.157	0.145	0.9	
		CO	1,987	3,648.4	0.001	0.077	0.010	0.005	0.5				CO	2,920	5,836.9	0.003	0.146	0.012	0.006	0.5												
		S	1,040	2,161.0	0.010	6.530	1.084	0.975	0.9	0.1			S	2,184	4,726.8	0.010	11.550	0.962	0.908	0.9	0.2											
CS	50	NI	125	220.5	0.003	0.355	0.082	0.068	0.8		hbcPx	108	NI	772	1,604.2	0.002	0.188	0.020	0.020	1.0		Ovb	10	NI	15	21.2	0.080	0.303	0.204	0.073	0.4	
		CO	125	220.5	0.001	0.027	0.008	0.004	0.6				CO	772	1,604.2	0.003	0.033	0.007	0.003	0.4				CO	15	21.2	0.010	0.021	0.015	0.004	0.2	
		S	46	116.6	0.020	1.360	0.441	0.401	0.9	0.2			S	421	967.8	0.010	2.980	0.610	0.511	0.8	0.0				S	2	1.6	0.160	0.480	0.440	0.106	0.2
Di	90	NI	398	995.7	0.000	0.313	0.034	0.048	1.4		Hfs	51	NI	291	596.9	0.001	0.276	0.024	0.044	1.9		oxPx	102	NI	11	20.1	0.038	0.367	0.202	0.096	0.5	
		CO	398	995.7	0.000	0.016	0.005	0.002	0.5				CO	291	596.9	0.001	0.030	0.004	0.003	0.8				CO	11	20.1	0.009	0.024	0.014	0.005	0.3	
		S	350	904.9	0.010	3.090	0.562	0.472	0.8	0.1			S	217	453.3	0.050	4.580	1.156	0.903	0.8	0.0				S	8	16.0	0.310	1.130	0.660	0.296	0.4
Dk	20	NI	452	849.7	0.001	0.604	0.071	0.078	1.1		Inc	8	NI	28	46.3	0.010	0.122	0.052	0.038	0.7		Phy	53	NI	82	232.1	0.002	0.184	0.018	0.032	1.8	
		CO	452	849.7	0.001	0.032	0.006	0.004	0.7				CO	28	46.3	0.006	0.020	0.011	0.004	0.4				CO	82	232.1	0.001	0.011	0.002	0.002	0.9	
		S	363	735.6	0.010	3.370	0.394	0.381	1.0	0.2			S	27	45.7	0.010	6.690	2.464	2.068	0.8	0.0				S	82	232.1	0.110	2.870	1.071	0.757	0.7
Du	110	NI	14,819	30,439.0	0.001	2.861	0.231	0.088	0.4		MGS	31	NI	4	7.4	0.275	0.599	0.497	0.135	0.3		Sp	115	NI	1,124	2,043.5	0.004	1.646	0.227	0.096	0.4	
		CO	14,819	30,439.0	0.001	0.166	0.014	0.005	0.3				CO	4	7.4	0.025	0.052	0.044	0.012	0.3				CO	1,124	2,043.5	0.001	0.097	0.013	0.005	0.4	
		S	12,046	26,201.7	0.010	12.040	0.469	0.561	1.2	0.5			S	4	7.4	1.730	6.570	4.943	2.106	0.4	0.1				S	799	1,564.1	0.010	3.670	0.395	0.465	1.2
flt	7	NI	515	1,057.9	0.005	0.581	0.163	0.079	0.5		MSD	52	NI	195	402.1	0.002	0.287	0.054	0.051	0.9		SMS	33	NI	1	2.0	0.534	0.534	0.534	0.000	0.0	
		CO	515	1,057.9	0.001	0.026	0.011	0.004	0.4				CO	195	402.1	0.001	0.014	0.005	0.003	0.6				CO	1	2.0	0.057	0.057	0.057	0.000	0.0	
		S	451	963.2	0.010	5.030	0.593	0.564	1.0	0.3			S	191	399.9	0.010	8.390	1.410	1.714	1.2	0.0				S	1	2.0	7.670	7.670	7.670	0.000	0.0
qDi	91	NI	18	35.2	0.001	0.024	0.005	0.006	1.1		MS	32	NI	6	11.0	0.038	1.987	0.286	0.425	1.5		Um	130	NI	53	129.3	0.036	0.192	0.097	0.035	0.4	
		CO	18	35.2	0.001	0.005	0.002	0.001	0.5				CO	6	11.0	0.003	0.149	0.026	0.032	1.3				CO	53	129.3	0.005	0.013	0.009	0.002	0.3	
		S	13	28.6	0.150	0.600	0.375	0.144	0.4	0.0			S	5	10.0	0.690	14.060	3.056	3.173	1.0	0.1				S	53	129.3	0.010	1.910	0.751	0.449	0.6
gDu	120	NI	2,053	4,021.9	0.001	0.750	0.250	0.053	0.2		mtcPx	103	NI	1,560	2,683.2	0.001	0.140	0.024	0.014	0.6		Wh	111	NI	10,644	21,957.0	0.001	2.587	0.224	0.099	0.4	
		CO	2,053	4,021.9	0.001	0.030	0.013	0.002	0.2				CO	1,560	2,683.2	0.001	0.024	0.007	0.003	0.4				CO	10,644	21,957.0	0.001	0.141	0.014	0.005	0.4	
		S	1,917	3,794.3	0.010	3.370	0.110	0.232	2.1	2.3			S	846	1,521.2	0.010	5.060	0.594	0.759	1.3	0.0				S	8,706	19,030.4	0.010	11.810	0.614	0.665	1.1
GS	30	NI	40	67.8	0.038	0.546	0.228	0.124	0.5		MV	17	NI	8	21.4	0.002	0.074	0.024	0.025	1.1		Total	Total	NI	39,078	78,806.4	0.000	5.148	0.192	0.116	0.6	
		CO	40	67.8	0.008	0.041	0.019	0.008	0.4				CO	8	21.4	0.001	0.005	0.003	0.001	0.5				CO	39,078	78,806.4	0.000	0.166	0.013	0.005	0.4	
		S	30	56.7	1.340	8.100	3.764	1.970	0.5	0.1			S	8	21.4	0.330	0.790	0.547	0.156	0.3	0.0				S	30,406	65,333.0	0.010	14.060	0.578	0.703	1.2

Source: Kirkham Geosystems, 2020.

The box plots illustrate the various lithologic units and their statistical relationship to each other. The box plots also show that there are grade similarities that justify the grouping of particular lithologic units. Therefore, it is acceptable to treat them in a similar manner both geologically and statistically. Box plots for all lithologic units are shown in Figure 14-2 through Figure 14-4 for nickel, cobalt and sulphur, respectively. The lithology units displayed represent greater than 92% of the samples and do not list all units as shown in Table 14.3 for the sake of brevity and significance. These include the dunite, wehrlite, green dunite, serpentinite and pyroxenites.

In order to evaluate lithologies in further granularity for the purpose of determining if there are logical, justifiable groupings, dunite, green dunite, wehrlite and serpentinite are shown in Figure 14-5 through Figure 14-7 for nickel, cobalt and sulphur, respectively. Nickel and cobalt box plots show a very good correlation and support for grouping however the sulphur makes it is clear that the green dunite should be estimated separately.

In addition, the clinopyroxenite, olivine clinopyroxenite, magnetite clinopyroxenite and hornblende clinopyroxenite were also statistically evaluated to determine if there are logical, justifiable groupings. The box plots are shown in Figure 14-8 through Figure 14-10 for nickel, cobalt and sulphur, respectively. It appears that there is no justification to separate the sub-groups during estimation.

To further support the statistical groupings during estimation of nickel and sulphur, a useful analysis is the comparison of the nickel-to-sulphur ratio against the nickel grades by lithologic unit as shown in the plot in Figure 14-11. It is clear that the dunite, wehrlite and serpentinite are very similar with the clinopyroxenites having lesser but similar characteristics. It is very clear that the green dunite is statistically different from all other zones and as such understandable that it is estimated separately.

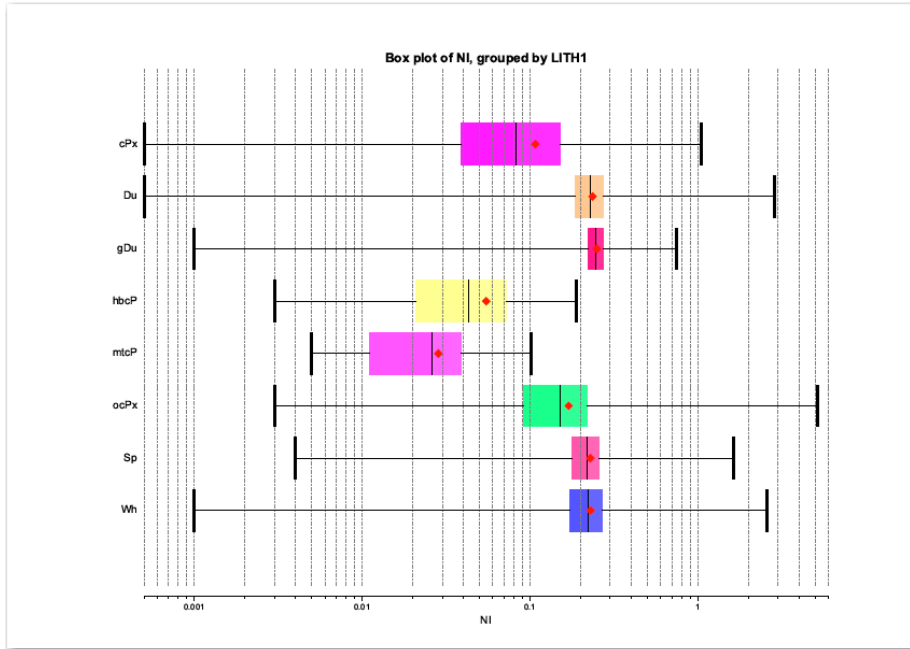
14.4 Geology Model

The mineral resource estimate is based on the validated drill hole database, interpreted three-dimensional geological model, digitised as-built data of historical workings, and topographic data. The geologic modelling was completed using the commercially available software Seequent Leapfrog Geo 4.3. The estimation of mineral resources was completed using commercial three-dimensional block modelling and mine planning software Hexagon Minesight™ MS3D Version 15.50.

Solid models (Figure 14-12) were created from coded drill hole intersections based primarily on lithology and site knowledge. It is important to note that the understanding and interpretation has evolved relatively flat lying units intruded by late dykes and sub-volcanics.

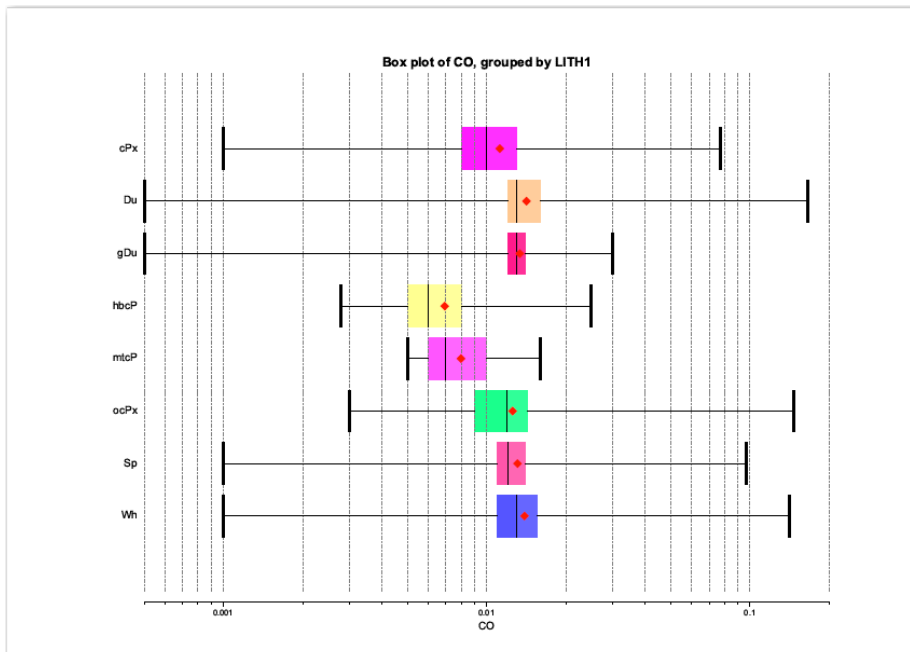
The domain models were modelled based on current drilling and assay data using Seequent Leapfrog Geo 4.3 and then imported into Minesight™ MS3D Version 15.50 for interpretation and refinement.

Figure 14-2: Box Plot of Nickel Composites by Lithology



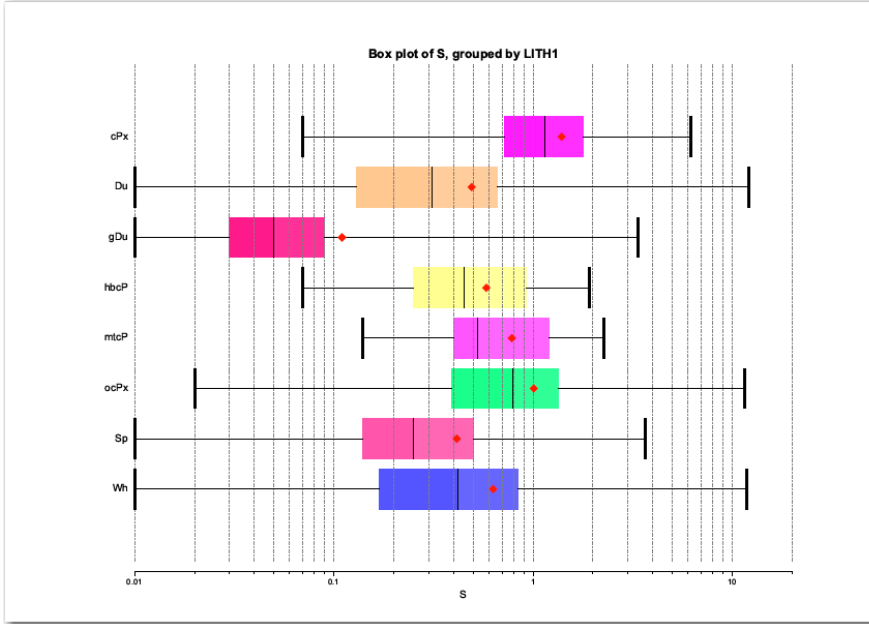
Source: Kirkham Geosystems, 2020.

Figure 14-3: Box Plot of Cobalt Composites by Lithology



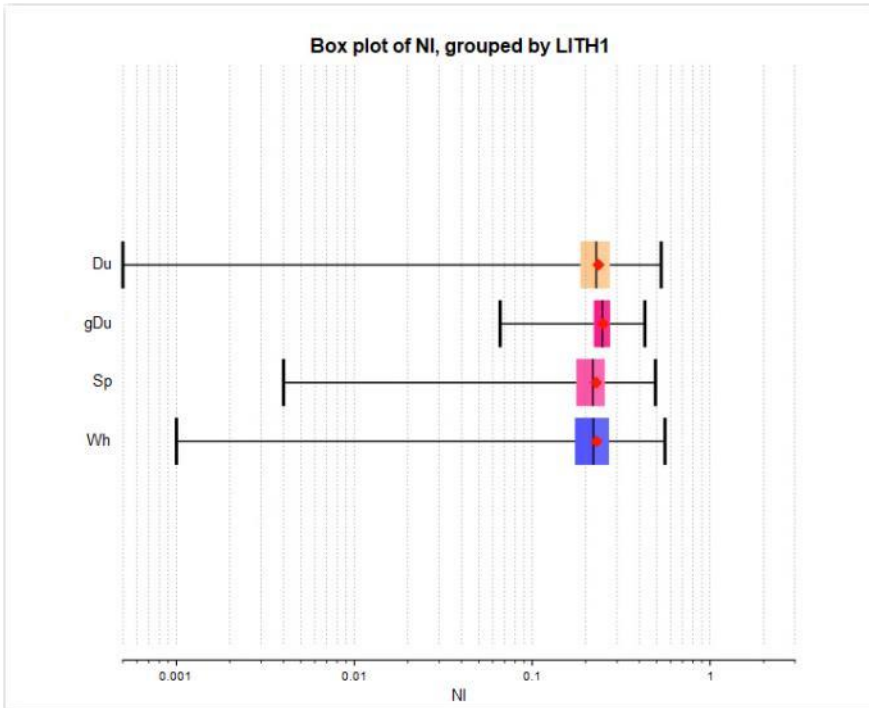
Source: Kirkham Geosystems, 2020.

Figure 14-4: Box Plot of Sulphur Composites by Lithology



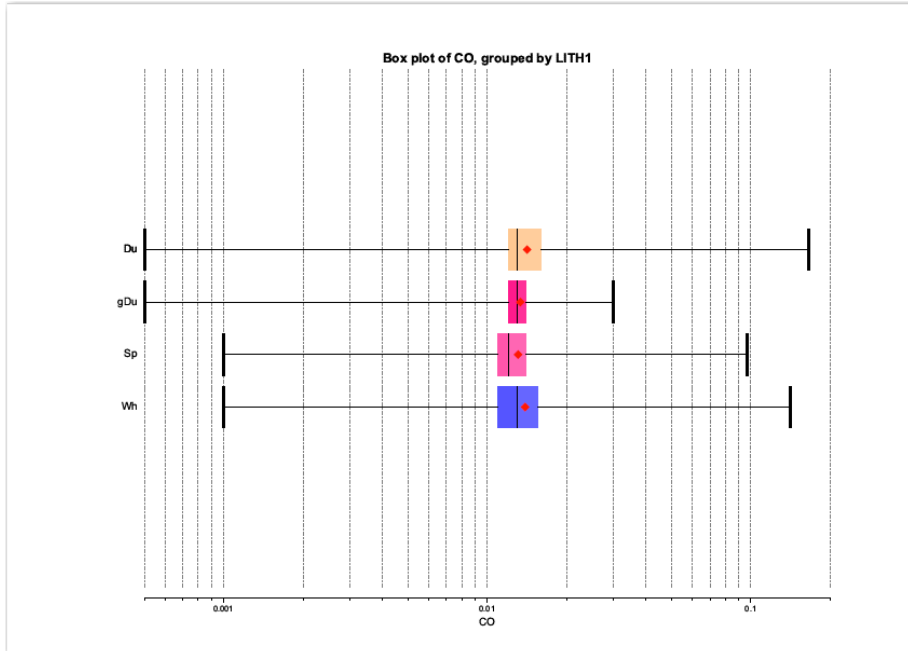
Source: Kirkham Geosystems, 2020.

Figure 14-5: Box Plot of Nickel Composites for Dunite, Green Dunite, Wehrlite, Serpentinite



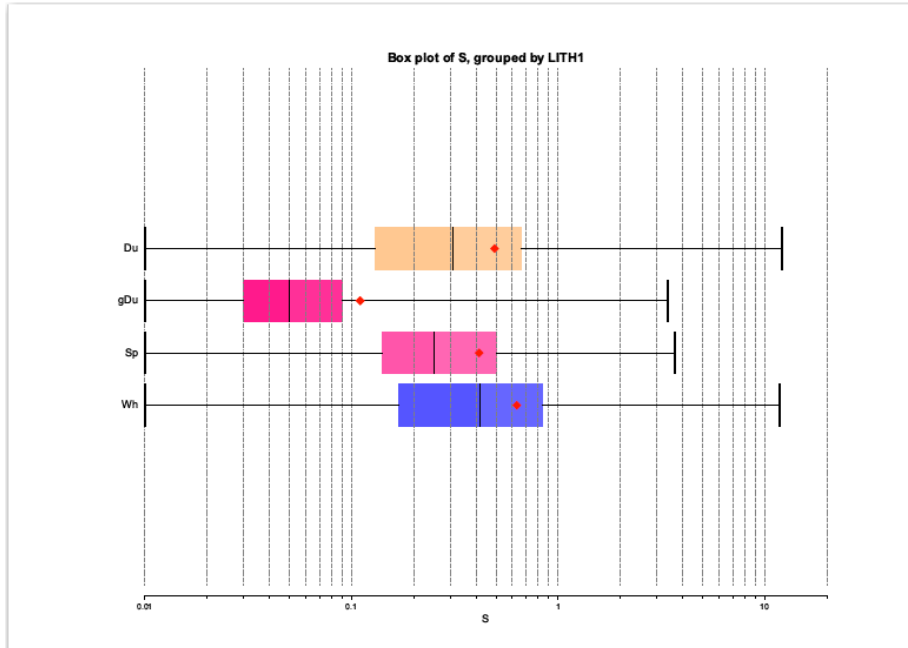
Source: Kirkham Geosystems, 2020.

Figure 14-6: Box Plot of Cobalt Composites for Dunite, Green Dunite, Wehrlite, Serpentinite



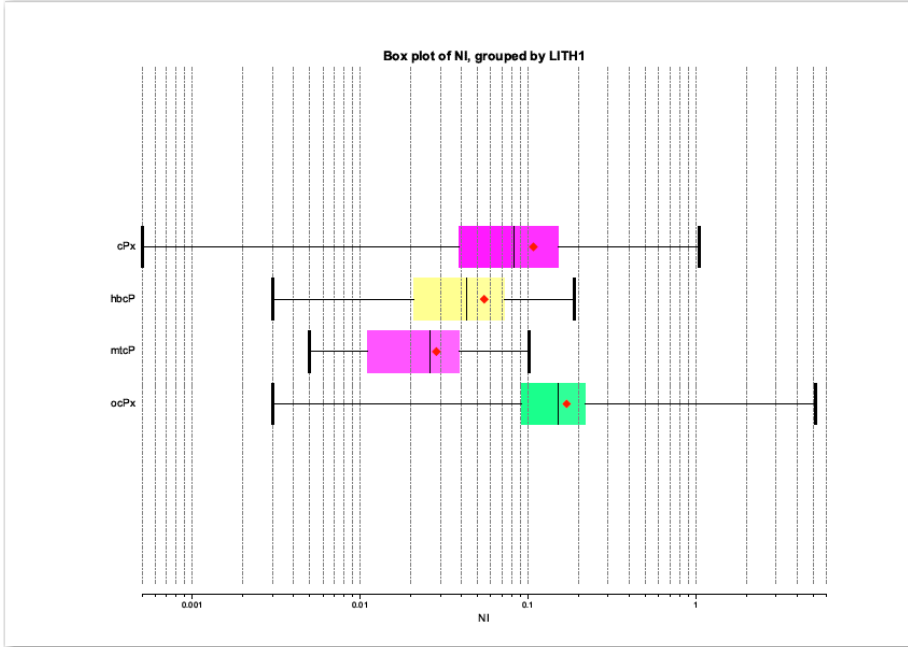
Source: Kirkham Geosystems, 2020.

Figure 14-7: Box Plot of Sulphur Composites for Dunite, Green Dunite, Wehrlite, Serpentinite



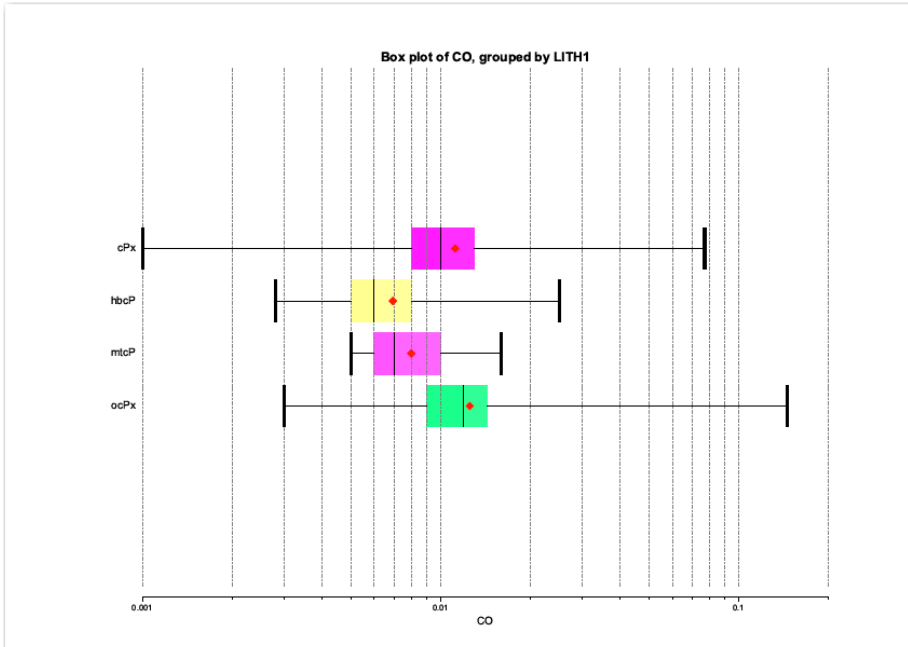
Source: Kirkham Geosystems, 2020.

Figure 14-8: Box Plot of Nickel Composites by Lithology Unit



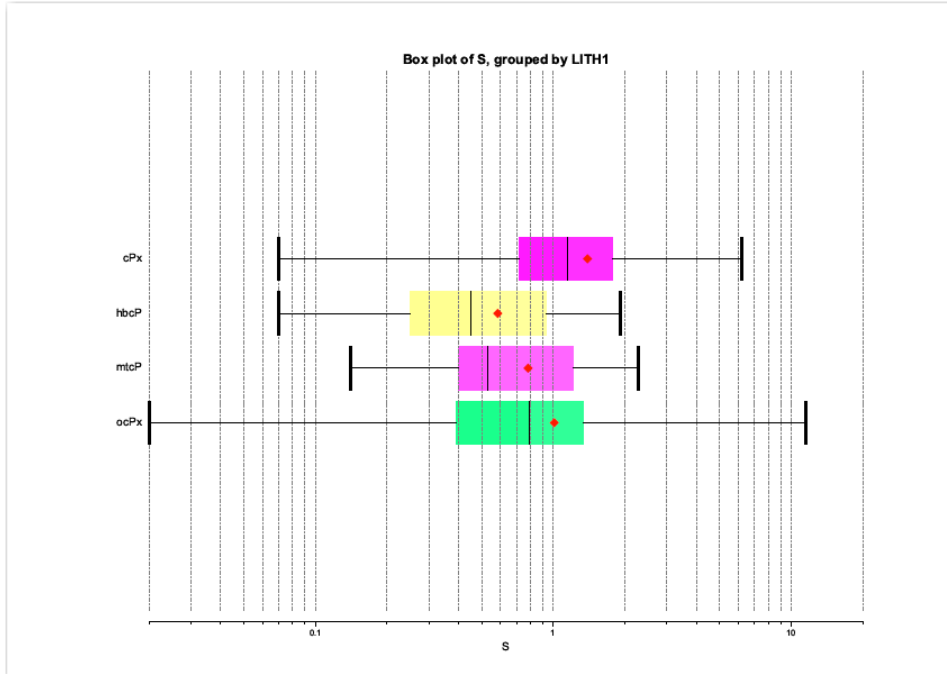
Source: Kirkham Geosystems, 2020.

Figure 14-9: Box Plot of Cobalt Composites by Lithology Unit



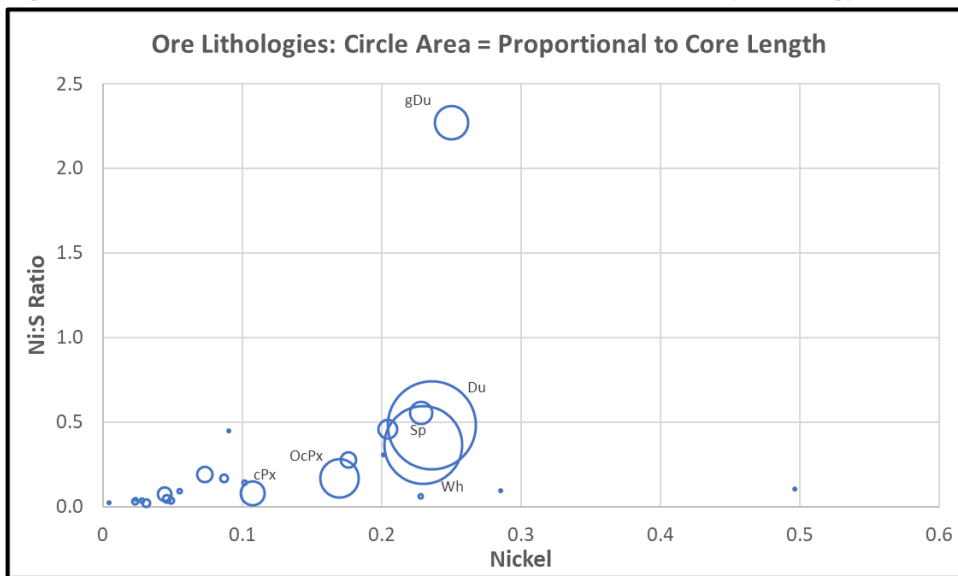
Source: Kirkham Geosystems, 2020.

Figure 14-10: Box Plot of Sulphur Composites by Lithology



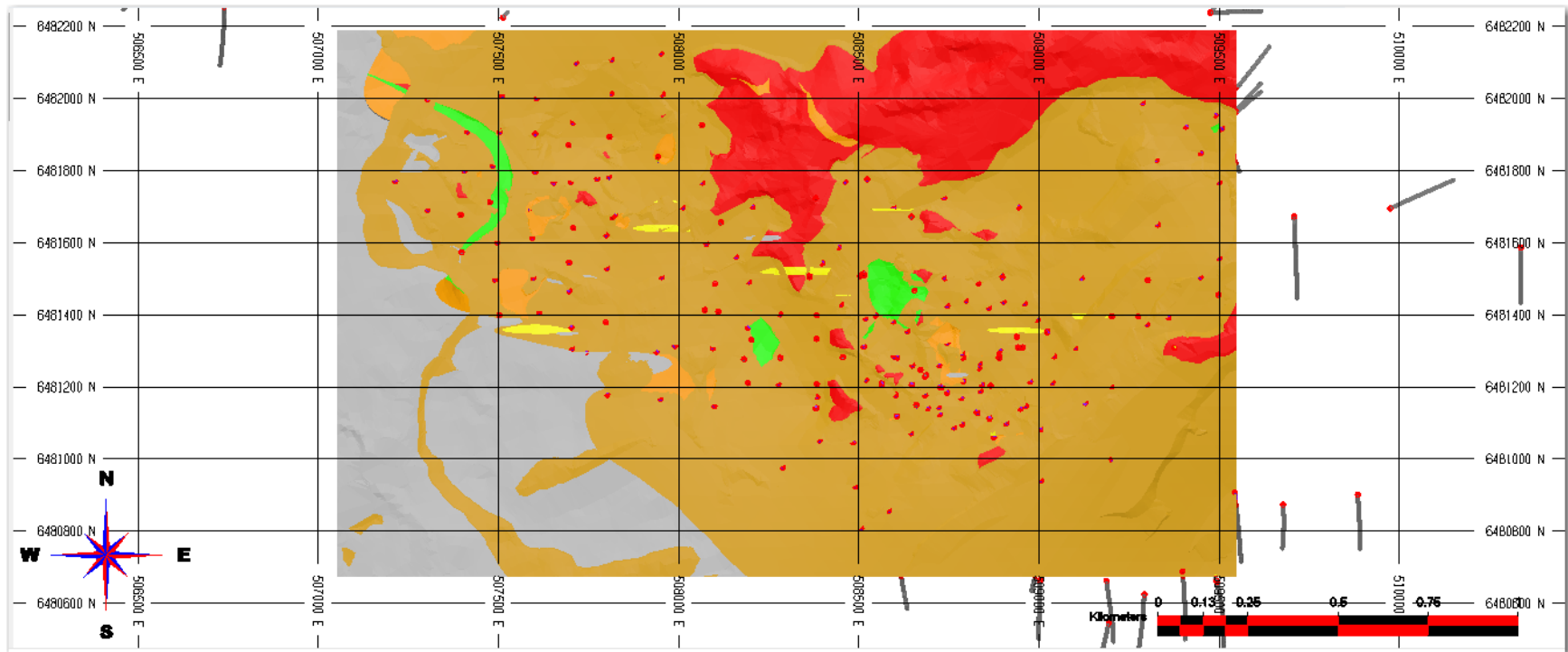
Source: Kirkham Geosystems, 2020.

Figure 14-11: Plot of Nickel-to-Sulphur Ratio vs. Nickel Grade by Lithology Unit



Source: Kirkham Geosystems, 2020.

Figure 14-12: Plan View of Turnagain Deposit Geology Domains & Drill Holes



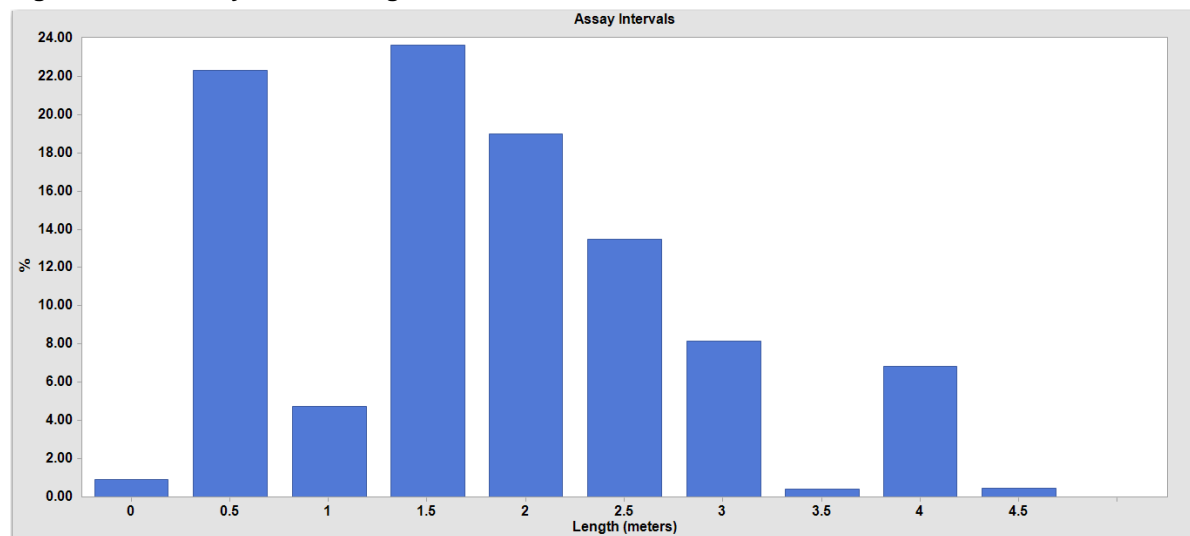
Notes: Grey = volcanics; brown = overburden; red = Wh-Du-Sp; green = green dunite; yellow = dykes; orange = pyroxenes. Source: Kirkham Geosystems, 2020.

The database was numerically coded by solids for the various zones. Intersections were inspected to ensure approximate agreement with the solids and then manually adjusted to match the drill intercepts where required. Once the solid model was created, it was used to code the drill hole assays and composites for subsequent statistical and geostatistical analyses. The solid zones were used to constrain the block model by matching assays to those within the zones. The orientation and ranges (distances) used for search ellipsoids in the estimation process were derived from strike and dip of the mineralised zone, site knowledge and on-site observations by Giga Metals geological staff. It is important to note that the block model is coded with the solids on a whole block majority basis which results in smoothing of the coded blocks and exclusion of thin stringers.

14.5 Composites

It was determined that a 4.0 m composite length offered the best balance between supplying common support for samples and minimising the smoothing of the grades. The 4.0 m sample length also was consistent with the distribution of sample lengths within the mineralised domains as shown in the histogram of assay lengths in Figure 14-13.

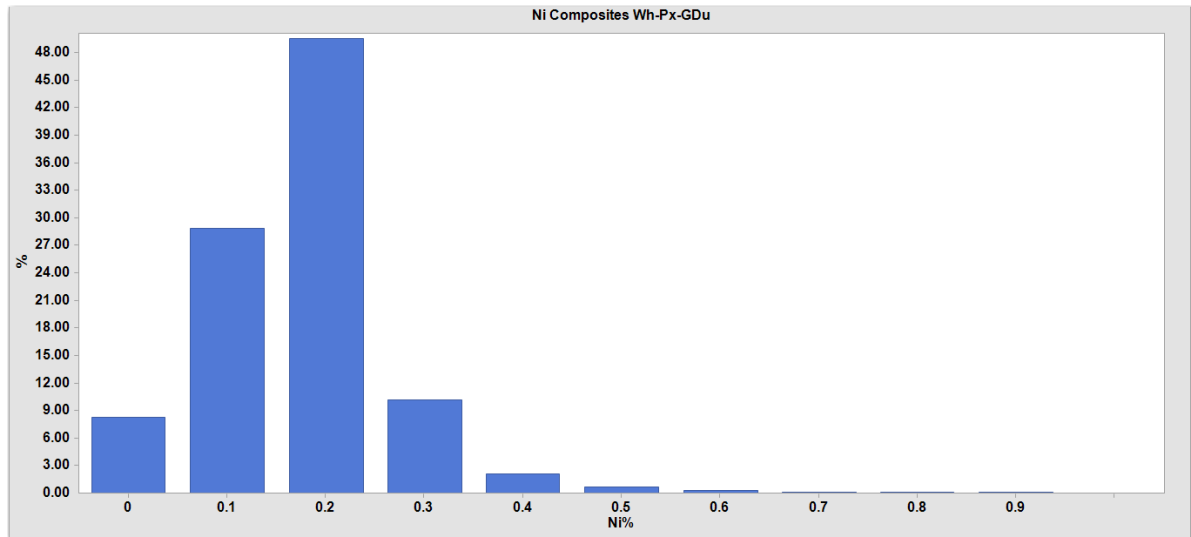
Figure 14-13: Assay Interval Lengths



Source: Kirkham Geosystems, 2020.

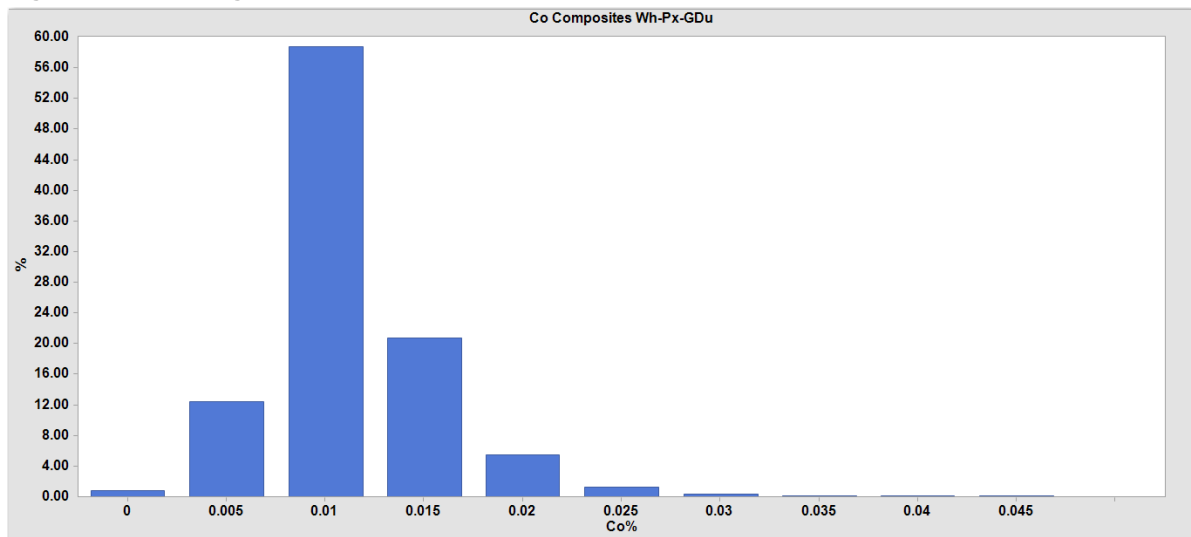
Figures 14-14 through 14-16 show the histograms for nickel, cobalt and sulphur, respectively, within the mineralised solids for all zones which demonstrate well-formed normal distribution for nickel and cobalt and log-normal distribution for sulphur.

Figure 14-14: Histogram of Nickel Composite Grades in Zones



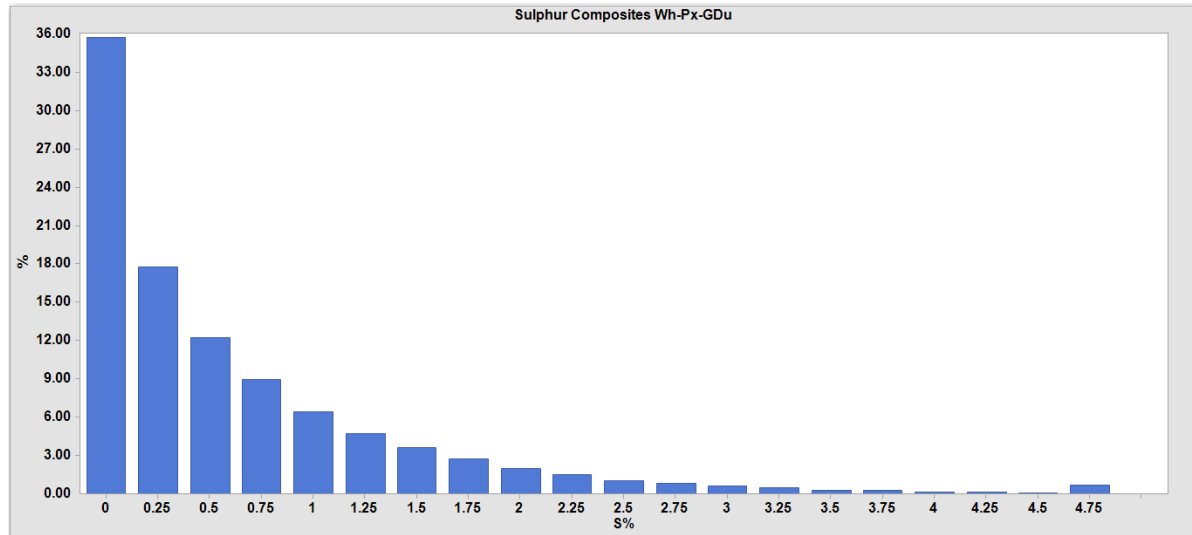
Source: Kirkham Geosystems, 2020.

Figure 14-15: Histogram of Cobalt Composite Grades in Zones



Source: Kirkham Geosystems, 2020.

Figure 14-16: Histogram of Sulphur Composite Grades in Zones



Source: Kirkham Geosystems, 2020.

Table 14.4 shows the basic statistics for the 4.0 m composite grades within the mineralised domains: (1) Du-Wh-Sp (dunite, wehrlite, serpentinite); (2) cPx-oPx (clinopyroxenite, olivine, magnetite and hornblende clinopyroxenite); (3) Volcanics; (4) Dykes; (5) Overburden. It should be noted that although 4.0 m is the composite length, any residual composites of lengths greater than 2.0 m and less than 4.0 m were retained to represent a composite, while any composite residuals less than 2.0 m were combined with the previous composite.

There is a total of 2,017 composites, with the averages (i.e., Ni%, NiAC%, Co%, CoAC%, Cu%, CuAC%, Mg, MgAC%, Fe%, Pt ppm, Pd ppm, S%, S% (Leco), Au, Ag), respectively, shown in Table 14.4.

Table 14.4: Composite Statistics Weighted by Length

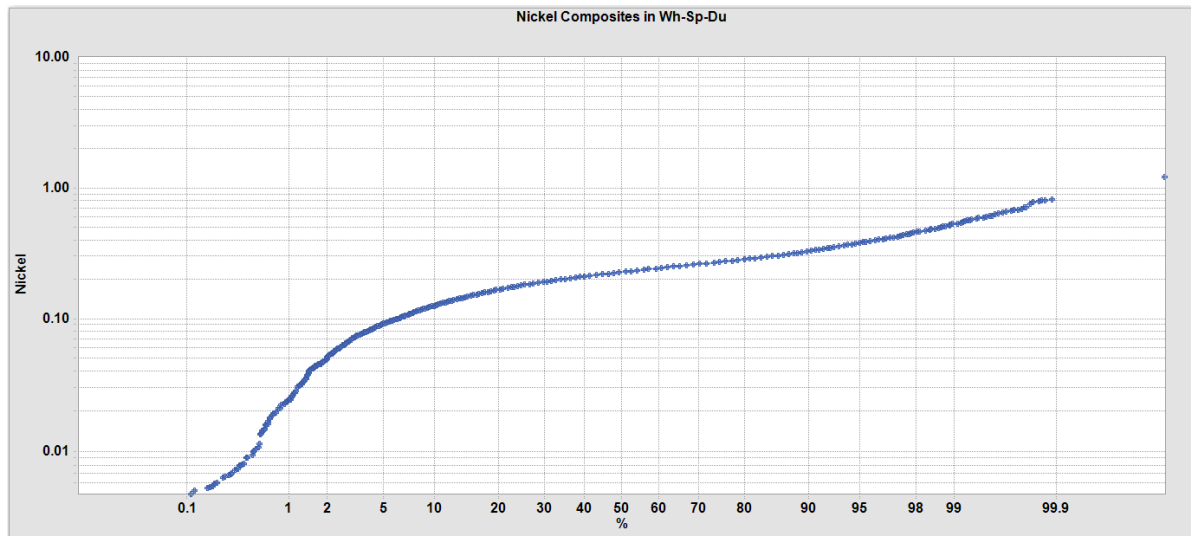
	Litho Zone	Valid	Count	Min	Max	Mean	SD	CV
NI	Wh-Du-Sp	9,114	36,345.3	0.00	1.21	0.23	0.09	0.4
	gDu	3,132	12,483.2	0.01	2.73	0.24	0.10	0.4
	cPx-oPx	2,679	10,643.2	0.00	0.97	0.18	0.10	0.6
	Dyke	76	293.1	0.00	0.65	0.10	0.13	1.3
	Volcanics	184	725.4	0.00	0.32	0.07	0.08	1.1
	Overburden	43	113.7	0.09	0.40	0.24	0.08	0.3
	Total	15,228	60,603.9	0.00	2.73	0.22	0.10	0.4
All	20,141	79,923.4	0.00	2.73	0.19	0.11	0.6	
NIAC	Wh-Du-Sp	7,645	30,481.1	0.00	1.26	0.17	0.09	0.6
	gDu	2,773	11,053.8	0.00	2.79	0.13	0.10	0.8
	cPx-oPx	2,352	9,340.2	0.00	0.96	0.14	0.08	0.6
	Dyke	68	261.2	0.00	0.68	0.08	0.12	1.5
	Volcanics	114	447.6	0.00	0.27	0.07	0.07	1.0
	Overburden	33	79.9	0.04	0.29	0.17	0.07	0.4
	Total	12,985	51,663.8	0.00	2.79	0.15	0.10	0.6
All	16,997	67,435.5	0.00	2.79	0.14	0.10	0.7	
CO	Wh-Du-Sp	9,114	36,345.3	0.00	0.09	0.01	0.00	0.3
	gDu	3,132	12,483.2	0.001	0.071	0.013	0.004	0.3
	cPx-oPx	2,679	10,643.2	0.001	0.049	0.013	0.005	0.4
	Dyke	76	293.1	0.001	0.021	0.006	0.005	0.8
	Volcanics	184	725.4	0.000	0.023	0.006	0.004	0.6
	Overburden	43	113.7	0.006	0.024	0.015	0.003	0.2
	Total	15,228	60,603.9	0.000	0.086	0.014	0.005	0.3
All	20,141	79,923.4	0.000	0.086	0.013	0.005	0.4	
COAC	Wh-Du-Sp	7,645	30,481.1	0.001	0.088	0.009	0.005	0.6
	gDu	2,773	11,053.8	0.001	0.076	0.007	0.004	0.6
	cPx-oPx	2,352	9,340.2	0.001	0.042	0.009	0.005	0.5
	Dyke	68	261.2	0.001	0.015	0.004	0.004	1.0
	Volcanics	114	447.6	0.001	0.020	0.005	0.004	0.8
	Overburden	33	79.9	0.003	0.017	0.010	0.003	0.3
	Total	12,985	51,663.8	0.001	0.088	0.009	0.005	0.6
All	16,997	67,435.5	0.001	0.088	0.008	0.005	0.6	
CU	Wh-Du-Sp	9,114	36,345.3	0.000	0.394	0.024	0.028	1.2
	gDu	3,132	12,483.2	0.000	0.271	0.017	0.025	1.5
	cPx-oPx	2,679	10,643.2	0.000	0.374	0.025	0.029	1.1
	Dyke	76	293.1	0.001	0.054	0.013	0.013	1.0
	Volcanics	184	725.4	0.002	0.090	0.016	0.010	0.7
	Overburden	43	113.7	0.000	0.076	0.023	0.019	0.9
	Total	15,228	60,603.9	0.000	0.394	0.022	0.027	1.2
All	20,141	79,923.4	0.000	0.414	0.023	0.030	1.3	
CUAC	Wh-Du-Sp	7,645	30,481.1	0.001	0.362	0.023	0.027	1.2
	gDu	2,773	11,053.8	0.001	0.251	0.016	0.024	1.5
	cPx-oPx	2,352	9,340.2	0.001	0.331	0.023	0.024	1.0
	Dyke	68	261.2	0.001	0.051	0.013	0.012	1.0
	Volcanics	114	447.6	0.003	0.044	0.016	0.008	0.5
	Overburden	33	79.9	0.002	0.065	0.025	0.018	0.7
	Total	12,985	51,663.8	0.001	0.362	0.022	0.026	1.2
All	16,997	67,435.5	0.001	0.419	0.022	0.028	1.3	
MG	Wh-Du-Sp	9,112	36,337.3	1.38	35.16	23.36	4.68	0.2
	gDu	3,132	12,483.2	0.73	33.71	24.54	4.52	0.2
	cPx-oPx	2,679	10,643.2	2.53	33.48	20.38	5.58	0.3
	Dyke	76	293.1	0.45	28.89	10.34	8.96	0.9
	Volcanics	184	725.4	0.47	26.58	9.69	6.58	0.7
	Overburden	43	113.7	3.55	31.34	24.33	3.47	0.1
	Total	15,226	60,595.9	0.45	35.16	22.85	5.33	0.2
All	20,139	79,915.4	0.01	35.16	20.99	6.66	0.3	
MGAC	Wh-Du-Sp	6,612	26,395.7	0.04	9.5	2.1	1.1	0.5
	gDu	2,442	9,732.4	0.01	7.4	2.4	1.1	0.5
	cPx-oPx	1,970	7,826.8	0.04	5.6	1.5	1.1	0.8
	Dyke	46	181.1	0.02	5.2	0.8	1.2	1.4
	Volcanics	113	444.1	0.05	4.9	0.7	0.8	1.3
	Overburden	25	58.9	0.48	3.6	1.6	0.7	0.5
	Total	11,208	44,638.9	0.01	9.5	2.0	1.1	0.6
All	14,985	59,516.9	0.01	9.5	1.8	1.2	0.7	
S	Wh-Du-Sp	9,114	36,345.3	0.01	11.53	0.72	0.87	1.2
	gDu	3,132	12,483.2	0.01	13.14	0.47	0.72	1.5
	cPx-oPx	2,679	10,643.2	0.01	9.33	1.11	1.03	0.9
	Dyke	76	293.1	0.01	1.45	0.37	0.30	0.8
	Volcanics	184	725.4	0.09	3.64	0.91	0.79	0.9
	Overburden	43	113.7	0.01	2.27	0.63	0.51	0.8
	Total	15,228	60,603.9	0.01	13.14	0.74	0.89	1.2
All	20,141	79,923.4	0.01	13.14	0.71	0.88	1.2	
SICP	Wh-Du-Sp	9,044	36,064.9	0.01	11.53	0.64	0.74	1.2
	gDu	3,126	12,458.2	0.01	6.97	0.42	0.60	1.4
	cPx-oPx	2,671	10,613.2	0.01	9.33	1.00	0.92	0.9
	Dyke	76	293.1	0.01	1.20	0.34	0.26	0.8
	Volcanics	184	725.4	0.09	3.32	0.84	0.70	0.8
	Overburden	42	109.6	0.01	2.27	0.62	0.47	0.8
	Total	15,143	60,264.4	0.01	11.53	0.66	0.77	1.2
All	20,056	79,583.9	0.01	11.53	0.64	0.76	1.2	
SLECO	Wh-Du-Sp	6,838	27,264.8	0.01	11.53	0.78	0.94	1.2
	gDu	2,339	9,323.5	0.01	13.14	0.52	0.79	1.5
	cPx-oPx	2,131	8,471.3	0.01	9.33	1.20	1.07	0.9
	Dyke	58	219.9	0.01	1.45	0.40	0.33	0.8
	Volcanics	138	542.5	0.11	3.64	1.05	0.85	0.8
	Overburden	33	85.2	0.01	2.13	0.60	0.56	0.9
	Total	11,537	45,907.1	0.01	13.14	0.81	0.96	1.2
All	14,438	57,337.4	0.01	13.14	0.78	0.95	1.2	
FE	Wh-Du-Sp	9,114	36,345.3	0.77	26.50	7.95	1.74	0.2
	gDu	3,132	12,483.2	0.46	22.82	7.48	1.77	0.2
	cPx-oPx	2,679	10,643.2	4.18	19.31	8.52	1.80	0.2
	Dyke	76	293.1	1.95	11.00	5.91	2.38	0.4
	Volcanics	184	725.4	1.93	13.45	7.67	2.19	0.3
	Overburden	43	113.7	0.79	12.23	7.81	1.38	0.2
	Total	15,228	60,603.9	0.46	26.50	7.94	1.80	0.2
All	20,141	79,923.4	0.01	26.50	8.02	2.00	0.2	
PT	Wh-Du-Sp	8,203	32,720.2	1	1,054	22	32	1.4
	gDu	2,808	11,188.4	1	647	21	34	1.6
	cPx-oPx	2,406	9,566.3	1	213	18	23	1.2
	Dyke	66	253.0	1	198	16	32	2.0
	Volcanics	168	659.8	1	171	11	16	1.4
	Overburden	37	95.1	2	65	23	13	0.6
	Total	13,688	54,482.8	1	1,054	21	31	1.5
All	18,592	73,769.7	1	1,974	24	45	1.9	
PD	Wh-Du-Sp	8,441	33,669.7	1	1,192	23	33	1.4
	gDu	2,883	11,489.4	1	707	21	35	1.7
	cPx-oPx	2,460	9,780.6	1	284	20	23	1.2
	Dyke	66	253.0	1	201	16	34	2.1
	Volcanics	183	721.4	1	125	10	13	1.2
	Overburden	37	95.1	1	98	24	16	0.6
	Total	14,070	56,009.2	1	1,192	22	32	1.4
All	18,980	75,320.0	1	1,602	25	43	1.7	
AU	Wh-Du-Sp	7,668	30,590.2	0.001	1.525	0.005	0.023	4.4
	gDu	2,677	10,663.9	0.001	0.164	0.004	0.008	1.9
	cPx-oPx	2,283	9,071.8	0.001	0.219	0.005	0.008	1.7
	Dyke	59	225.1	0.001	0.044	0.004	0.006	1.8
	Volcanics	149	586.3	0.001	0.018	0.002	0.002	1.0
	Overburden	33	81.7	0.001	0.027	0.005	0.007	1.5
	Total	12,869	51,219.1	0.001	1.525	0.005	0.018	3.8
All	17,541	69,582.9	0.001	1.525	0.005	0.017	3.8	
AG	Wh-Du-Sp	7,828	31,210.8	0.27	26.4	1.1	0.6	0.6
	gDu	2,786	11,105.8	0.15	29.0	1.1	0.7	0.6
	cPx-oPx	2,400	9,530.6	0.5	17.9	1.1	0.5	0.5
	Dyke	68	261.2	1	2.0	1.0	0.2	0.2
	Volcanics	143	560.5	0.5	3.0	1.1	0.3	0.3
	Overburden	33	79.9	0.15	2.0	1.0	0.2	0.2
	Total	13,258	52,748.8	0.15	29.0	1.1	0.6	0.6
All	17,901	70,993.3	0.15	152.0	1.1	1.4	1.2	

Source: Kirkham Geosystems, 2020.

14.6 Evaluation of Outlier Assay Values

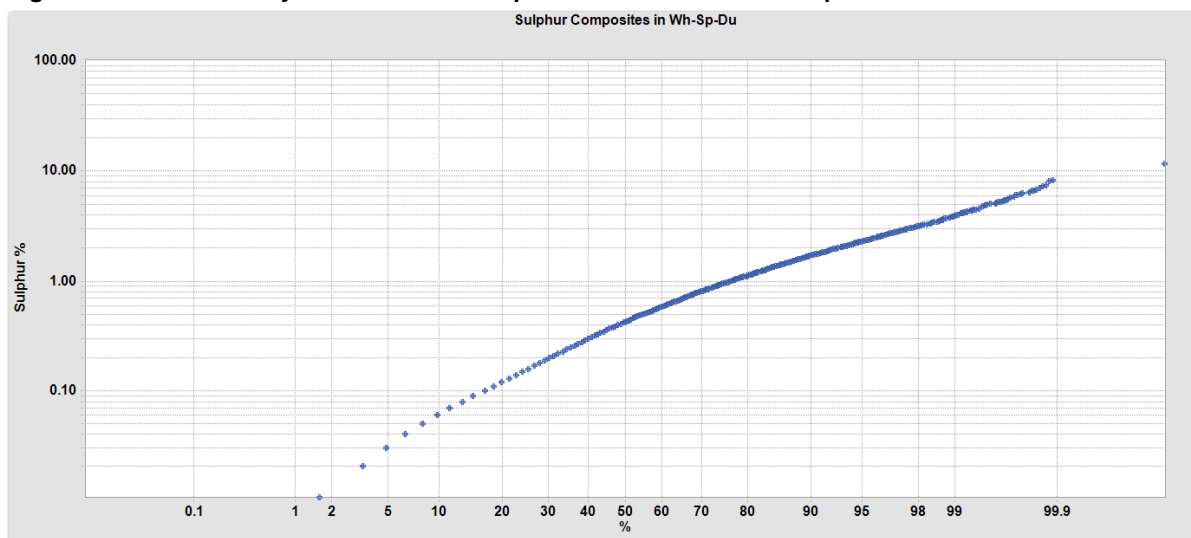
An evaluation of the probability plot of nickel and sulphur composites suggests there are no outlier values that could result in an overestimation of resources. Figure 14-17 and 14-18 illustrate that there are no distinct “breaks” in the cumulative frequency plots with which to determine the potential of an outlier population.

Figure 14-17: Probability Plot of Nickel Composites within the Wh-Du-Sp Zone



Source: Kirkham Geosystems, 2020.

Figure 14-18: Probability Plot of Nickel Composites within the Wh-Du-Sp Zone



Source: Kirkham Geosystems, 2020.

14.7 Bulk Density Estimation

Bulk density measurements were carried out on 1,318 core samples collected between 2004 and 2018. Bulk density of core samples was measured in the field by the immersion method. A piece of whole core up to 50 cm in length was weighed in air and in water and the density calculated using the following formula:

$$\text{Bulk density} = [\text{weight in air}/(\text{weight in air} - \text{weight in water})] * 1 \text{ t/m}^3$$

As part of the metallurgical test program, Process Research Associates Ltd. (PRA), measured bulk density using the pycnometric method with -10 Tyler mesh assay rejects. Their results were within 5% of density determinations measured by ACME Laboratory in 2007 using the same method. A total of 1,318 measurements were done by the immersion method on whole core and 312 measurements carried out on crushed samples using the pycnometric procedure.

Bulk densities were based on 1,630 measurements taken by personnel throughout the zones. These density values ranged from 2.24 t/m³ to 5.36 t/m³. Density was assigned to the model blocks based on the mean value for the corresponding lithology, as listed in Table 14.5.

Table 14.5: Bulk Density Statistics by Zone

			Valid	Min	Max	Mean	SD	CV	
SG	1	DuWhSp	997	1.81	4.32	3.05	0.20	0.1	
	2	gDu	276	2.64	4.49	3.08	0.22	0.1	
	3	cPx/ocPx	313	2.24	5.36	3.07	0.28	0.1	
	8	Dyke	11	2.71	3.21	2.99	0.14	0.0	
	9	Volcanic	18	2.74	3.2	3.00	0.15	0.1	
	10	OB	3	2.87	2.91	2.89	0.02	0.0	
		Total		1,618	1.81	5.36	3.06	0.22	0.1
		All		2,035	1.81	5.36	3.07	0.22	0.1

Source: Kirkham Geosystems, 2020.

14.8 Variography

The degree of spatial variability and continuity in a mineral deposit depend on both the distance and direction between points of comparison. Typically, the variability between samples is proportionate to the distance between samples. If the variability is related to the direction of comparison, then the deposit is said to exhibit *anisotropic* tendencies which can be summarised by an ellipse fitted to the ranges in the different directions. The semi-variogram is a common function used to measure the spatial variability within a deposit.

The components of the variogram include the nugget, the sill, and the range. Often samples compared over very short distances (including samples from the same location) show some

degree of variability. As a result, the curve of the variogram often begins at a point on the y-axis above the origin; this point is called the *nugget*. The nugget is a measure of not only the natural variability of the data over very short distances, but also a measure of the variability which can be introduced due to errors during sample collection, preparation, and assaying.

Typically, the amount of variability between samples increases as the distance between the samples increase. Eventually, the degree of variability between samples reaches a constant or maximum value; this is called the *sill*, and the distance between samples at which this occurs is called the *range*.

The spatial evaluation of the data was conducted using a correlogram instead of the traditional variogram. The correlogram is normalised to the variance of the data and is less sensitive to outlier values; this generally gives cleaner results.

Experimental variograms and variogram models in the form of correlograms were generated for nickel and cobalt along with sulphur.

Correlograms were generated for the distribution of nickel and cobalt along with sulphur in the various areas using the commercial software package Sage 2001© developed by Isaacs & Co. Correlogram model data is shown in Table 14.6 for nickel, cobalt and sulphur along with platinum and palladium in Table 14.7.

Table 14.6: Variography for Nickel, Cobalt & Sulphur by Zone

Ni		Px	gDu	Wh/Du
	C0	0.294	0.103	0.267
	C1	0.225	0.567	0.498
	C2	0.481	0.33	0.235
1st Structure	DY	16.6	15.5	20.3
	DX	136.8	32.2	32.8
	DZ	124.5	11.3	44
	R1	30	85	-49
	R2	16	6	-6
	R3	-61	-32	3
2nd Structure	DY	85.3	81.7	102.3
	DX	62.3	34.3	175
	DZ	326.5	273.2	282.2
	R1	33	-22	43
	R2	28	13	-4
	R3	-25	0	-46

Co		Px	gDu	Wh/Du
	C0	0.332	0.329	0.381
	C1	0.45	0.477	0.454
	C2	0.218	0.194	0.165
1st Structure	DY	38.4	28.5	96.5
	DX	25.4	17.6	31.6
	DZ	128.34	79	27.4
	R1	41	-16	0
	R2	10	10	65
	R3	-9	-12	-71
2nd Structure	DY	85.4	410.1	354.4
	DX	220.4	119.5	109.7
	DZ	889.8	246.4	449.1
	R1	81	14	-73
	R2	4	-15	20
	R3	-60	-65	14

S		Px	gDu	Wh/Du
	C0	0.294	0.076	0.277
	C1	0.299	0.802	0.543
	C2	0.407	0.122	0.18
1st Structure	DY	14.6	320.6	37.5
	DX	10	33.4	46.3
	DZ	35.5	211	131.9
	R1	-22	10	3
	R2	-39	33	0
	R3	-6	7	-1
2nd Structure	DY	81.9	62.1	246.6
	DX	71.1	187.4	965.5
	DZ	1596.9	248	719.6
	R1	42	-7	20
	R2	36	31	-4
	R3	-30	-73	-80

Source: Kirkham Geosystems, 2020.

Table 14.7: Variography for Platinum & Palladium by Zone

Pt		Px	gDu	Wh/Du
	C0	0.311	0.411	0.44
	C1	0.435	0.451	0.43
	C2	0.254	0.138	0.13
1st Structure	DY	17.2	17.7	15.5
	DX	11.6	48.5	25.5
	DZ	21.6	13.3	52.1
	R1	93	-27	79
	R2	-70	27	-1
	R3	-23	63	-4
2nd Structure	DY	46.8	227	179.8
	DX	115.9	113	139.9
	DZ	813.1	482.7	392.8
	R1	71	-10	-39
	R2	4	133	33
	R3	-18	-21	-21

Source: Kirkham Geosystems, 2020.

Pd		Px	gDu	Wh/Du
	C0	0.404	0.349	0.384
	C1	0.391	0.48	0.433
	C2	0.205	0.171	0.183
1st Structure	DY	11.1	16.2	14.9
	DX	12.6	51	49.7
	DZ	74.3	17.8	20.8
	R1	-16	-65	66
	R2	-1	31	-2
	R3	1	76	77
2nd Structure	DY	76.3	727.6	133.3
	DX	149.2	193.1	176.7
	DZ	675.7	138.9	562.8
	R1	56	-28	36
	R2	3	42	-10
	R3	-20	-57	-40

14.9 Block Model Definition

The block model used to estimate the resources was defined according to the limits specified in Figures 14-19 and 14-20. The block model is orthogonal and non-rotated, reflecting the orientation of the deposit. The chosen block size was 15 m x 15 m x 15 m, roughly reflecting the drill hole spacing (i.e., 4 to 6 blocks between drill holes) which is spaced at approximately 50 m centres. Note: MineSight™ uses the centroid of the blocks as the origin.

Figure 14-19: Dimensions for the Turnagain Block Model

Rotate PCF J:\Turnagain\Turnagain MineSigh... — □ ×

Rotation Extents

Model Limits (in model coordinates)

Coordinate	Min	Max	Block size	Number of blocks
X (columns / i)	507000	510000	15	200
Y (rows / j)	6480250	6482530	15	152
Z (levels / k)	600	1350	15	50

Move Model Move to a point specified in Project coordinates
Default: point specified in Model coordinates

Project Bounds

	Min	Max
Easting	(507000)	(510000)
Northing	(6480250)	(6482530)
Elevation	(600)	(1350)

Minimal bounds to contain the model are shown in parenthesis

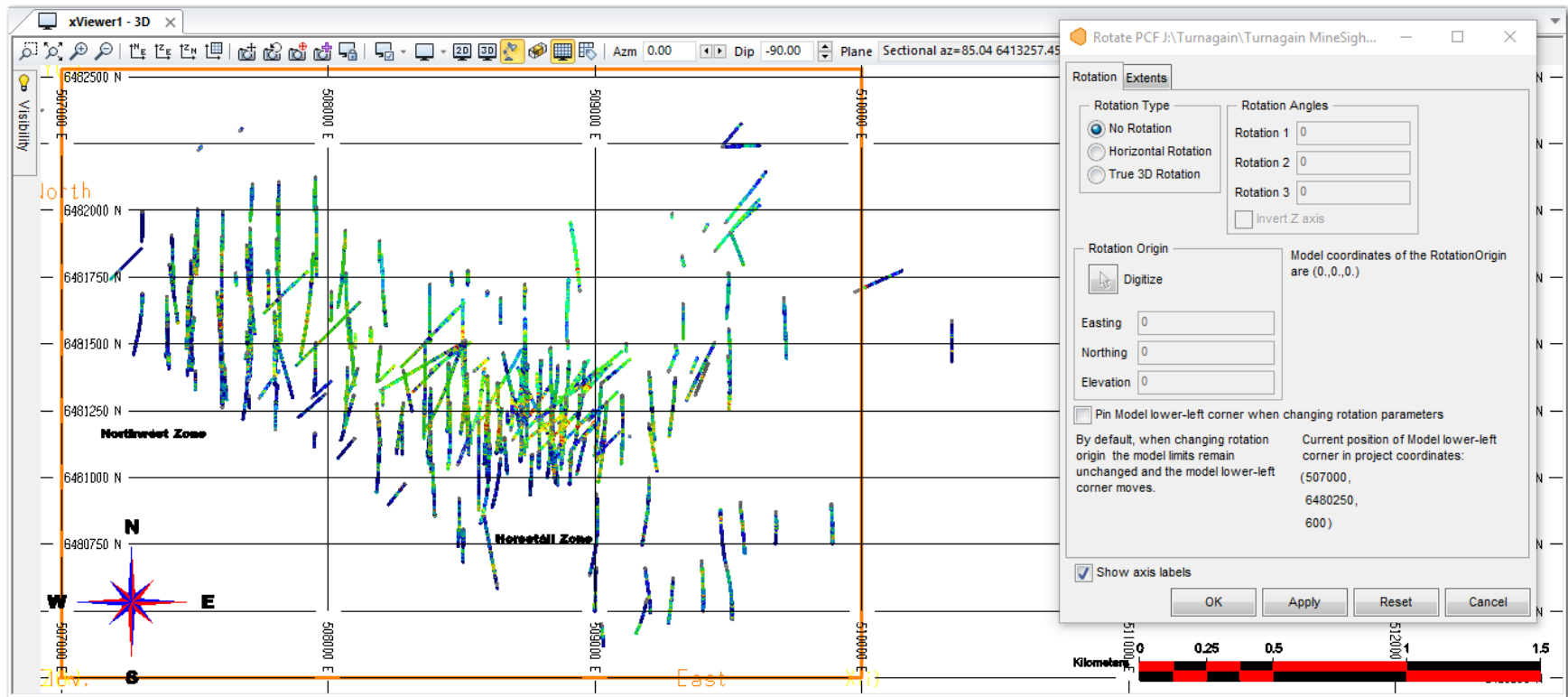
Set Bounds to Min Auto update Round to No Round ▼

Show axis labels

OK Apply Reset Cancel

Source: Kirkham Geosystems, 2020.

Figure 14-20: Origin & Orientation for the Turnagain Block Model



Source: Kirkham Geosystems, 2020.

14.10 Resource Estimation Methodology

The resource estimation plan includes the following items:

- lithological zone code in each block
- estimated block nickel, cobalt, sulphur grades using ordinary kriging
- estimated block platinum, palladium grades using ordinary kriging

Table 14.8 summarises the search ellipse dimensions for the one estimation pass for each zone by majority code.

Table 14.8: Search Ellipse Parameters for the Turnagain Deposit

Major Axis	Semi-Major Axis	Minor Axis	1 st Rotation Angle Azimuth	2 nd Rotation Angle Dip	3 rd Rotation Angle	Min. No. Of Comps	Max. No. Of Comps	Max. Samples per Drill Hole
150	150	150	0	90	0	2	16	4

Source: Kirkham Geosystems, 2020.

14.11 Resource Validation

A graphical validation was completed on the block model. This type of validation serves the following purposes:

- checks the reasonableness of the estimated grades based on the estimation plan and the nearby composites
- checks that the general drift and the local grade trends compare to the drift and local grade trends of the composites
- ensures that all blocks in the core of the deposit have been estimated
- checks that topography has been properly accounted for
- checks against manual approximate estimates of tonnages to determine reasonableness
- inspects for and explains potentially high-grade block estimates in the neighbourhood of the extremely high assays

A full set of cross sections, long sections and plans were used to digitally check the block model; these showed the block grades and composites. There was no indication that a block was wrongly estimated, and it appears that every block grade could be explained as a function of the surrounding composites and the applied estimation plan.

The validation techniques included the following:

- visual inspections on a section-by-section and plan-by-plan basis

- use of grade-tonnage curves
- swath plots comparing kriged estimated block grades with inverse distance and nearest neighbour estimates
- inspection of histograms showing distance from first composite to nearest block, and average distance to blocks for all composites (this gives a quantitative measure of confidence that blocks are adequately informed in addition to assisting in the classification of resources)

14.12 Mineral Resource Classification

Mineral resources were estimated in conformity with generally accepted CIM's "Estimation of Mineral Resources and Mineral Reserves Best Practice Guidelines" (2019). Mineral resources are not mineral reserves and do not have demonstrated economic viability.

The mineral resources may be impacted by further infill and exploration drilling that may result in an increase or decrease in future resource evaluations. The mineral resources may also be affected by subsequent assessment of mining, environmental, processing, permitting, taxation, socio-economic and other factors.

Mineral resources for the Turnagain deposit were classified according to the CIM's "Definition Standards for Mineral Resources and Mineral Reserves" (2014) by Garth Kirkham, P.Geol., an independent qualified person as defined by NI 43-101 guidelines.

Drill hole spacing in the Turnagain deposit is sufficient for preliminary geostatistical analysis and evaluating spatial grade variability. Kirkham Geosystems, therefore, is of the opinion that the amount of sample data is adequate to demonstrate very good confidence in the grade estimates for the deposit.

The estimated blocks were classified according to the following:

- confidence in interpretation of the mineralised zones
- number of data used to estimate a block
- number of composites allowed per drill hole
- distance to nearest composite used to estimate a block

The classification of resources was based primarily on distance to the nearest composite; however, all of the quantitative measures, as listed here, were inspected and taken into consideration. In addition, the classification of resources for each zone was considered individually by virtue of their relative depth from surface and the ability to derive meaningful geostatistical results.

The mineral resource estimates for Turnagain were prepared to industry standards and best practices using commercial mine-modelling and geostatistical software. Garth Kirkham, P.Geol.,

is the qualified person responsible for the Turnagain mineral resource estimates for the purposes of NI 43-101.

Mineral resources are classified under the categories of *measured*, *indicated* and *inferred* according to CIM guidelines. Mineral resource classification was based primarily on drill hole spacing and on continuity of mineralisation. Measured resources were defined at Turnagain as blocks with a distance to three drill holes of less than ~40 m to nearest composite and an average of 80 m and occurring within the estimation domains. Indicated resources were defined as those with a distance to three drill holes of less than ~60 m and an average distance of 100 m. Inferred resources were defined as those with an average drill hole spacing of less than ~150 m and meeting additional requirements. Final resource classification shells were manually constructed on sections.

Furthermore, an interpreted boundary was created for the measured, indicated and inferred thresholds in order to exclude orphans and reduce “spotted dog” effect. The remaining blocks were unclassified and may be considered as geologic potential for further exploration.

14.13 Sensitivity of the Block Model to Selection Cut-off Grade

The mineral resources are sensitive to the selection of cut-off grade. Table 14.9 shows the total resources for all metals at varying Ni% cut-off grades. The reader is cautioned that these values should not be misconstrued as a mineral reserve. The reported quantities and grades are only presented as a sensitivity of the resource model to the selection of cut-off grades. Note: The base case cut-off grades presented in Table 14.9 are based on potentially open pit resources at the base case of 0.1% Ni.

14.14 Mineral Resource Statement

Table 14.10 shows the mineral resource statement for the Turnagain deposit. This estimate is based upon the reasonable prospect of eventual economic extraction based on continuity an optimized pit, using estimates of operating costs and price assumptions. The “reasonable prospects for eventual economic extraction” were tested using floating cone pit shells. The Horsetrail, Northwest, Hatzl and Duffy zones of the deposit are all included within the Horsetrail reasonable prospects pit shells. The pit optimization results are used solely for testing the “reasonable prospects for eventual economic extraction” and do not represent an attempt to estimate Mineral Reserves.

The Turnagain resource model includes the southern portions of the Horseshoe zone that abut and underlie the Turnagain River, and the Hatzl zone south of the river as shown in Figure 14-21. These zones are potentially exploitable with a diversion of a relatively short section of the Turnagain River, which remains a potentially viable option. These zones are not included in the current mine plan, as the diversion of the river is not currently contemplated from a mining perspective within this PEA, however, it is still considered as a potential option eventually.

Differences from the previous resource estimate described in AMC's 2011 PEA are the inclusion of an additional 36 infill drill holes totalling 8,940 m drilled in 2018 in the areas of the conceptual open pit, updated geological modelling (Figures 14-22 to 14-24) and current updated price and cost parameters.

Table 14.9: Sensitivity Analyses of Global Tonnage & Grades at Various Ni% Cut-off Grades

Classification	Cut-off	Tonnage (000s)	Ni Grade (%)	Co Grade (%)
Measured	0.05	364,997	0.228	0.0137
	0.10	360,913	0.230	0.0138
	0.15	341,518	0.236	0.0140
	0.20	271,773	0.251	0.0143
	0.25	111,963	0.285	0.0151
	0.30	24,868	0.340	0.0173
Indicated	0.05	744,776	0.209	0.0127
	0.10	712,406	0.215	0.0129
	0.15	632,964	0.226	0.0133
	0.20	468,776	0.242	0.0136
	0.25	158,978	0.274	0.0140
	0.30	17,020	0.326	0.0153
Inferred	0.05	1,219,566	0.211	0.0128
	0.10	1,142,101	0.217	0.0130
	0.15	1,041,600	0.226	0.0133
	0.20	791,347	0.241	0.0137
	0.25	243,580	0.277	0.0144
	0.30	27,211	0.347	0.0159

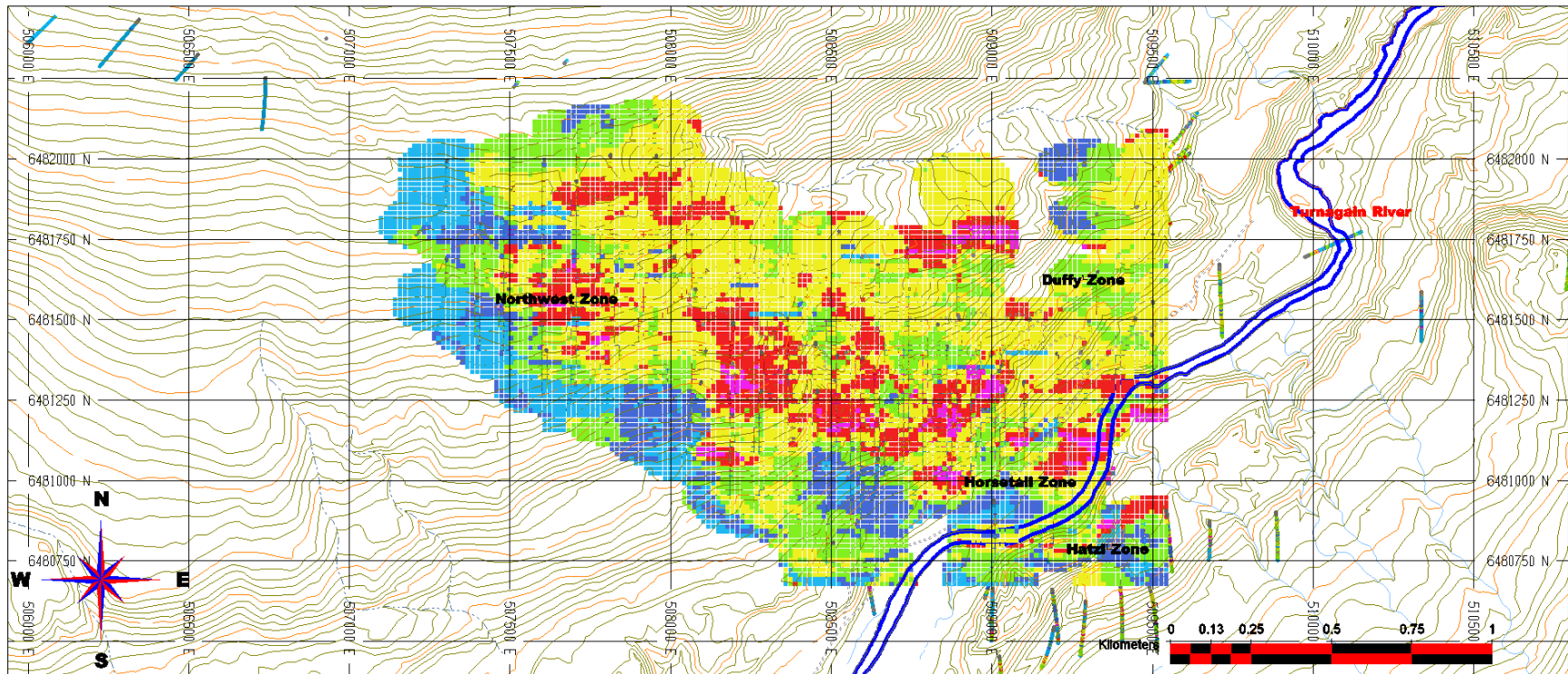
Notes: **(1)** The current resource estimate was prepared by Garth Kirkham, P.Geo., of Kirkham Geosystems Ltd. **(2)** All mineral resources have been estimated in accordance with Canadian Institute of Mining and Metallurgy and Petroleum definitions, as required under National Instrument 43-101. **(3)** Mineral resources are reported in relation to a conceptual pit shell in order to demonstrate reasonable expectation of eventual economic extraction, as required under NI 43-101; mineralisation lying outside of these pit shells is not reported as a mineral resource. **Mineral resources are not mineral reserves and do not have demonstrated economic viability.** All figures are rounded to reflect the relative accuracy of the estimate and therefore numbers may not appear to add precisely. **(4)** Open pit mineral resources are reported at a cut-off grade of 0.1% Ni. Cut-off grades are based on a price of US \$7.50 per pound, nickel recoveries of 60%, mineralized material and waste mining costs of \$2.80, along with milling, processing and G&A costs of \$7.20. **(5)** Inferred mineral resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. However, it is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated. **(6)** Due to rounding, numbers presented may not add up precisely to the totals provided and percentages may not precisely reflect absolute figures. Source: Kirkham Geosystems, 2020.

Table 14.10: Open Pit Mineral Resource Statement^(1,2,3,4,5) for the Turnagain Project. Base Case Estimate at 0.1% Nickel Cut-off Grade

Classification	Tonnage (000s)	Ni Grade (%)	Contained Ni (klbs)	Co Grade (%)	Contained Co (klbs)
Measured	360,913	0.230	1,832,424	0.0138	109,802
Indicated	712,406	0.215	3,373,585	0.0129	202,604
Measured & Indicated	1,073,319	0.220	5,206,009	0.0132	312,406
Inferred	1,142,101	0.217	5,473,862	0.0130	327,324

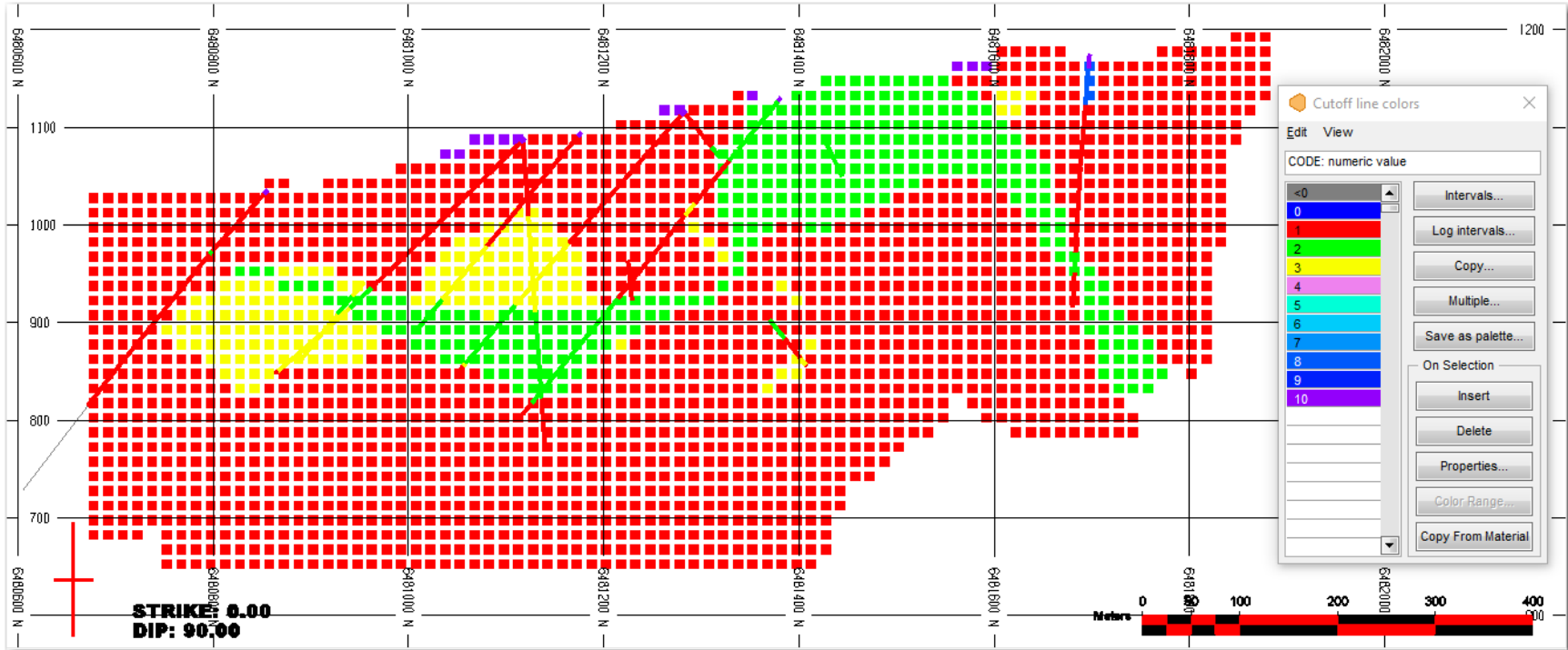
Notes: **(1)** All mineral resources have been estimated in accordance with Canadian Institute of Mining and Metallurgy and Petroleum definitions, as required under National Instrument 43-101. **(2)** Mineral resources are reported in relation to a conceptual pit shell in order to demonstrate reasonable expectation of eventual economic extraction, as required under NI 43-101; mineralisation lying outside of these pit shells is not reported as a mineral resource. **Mineral resources are not mineral reserves & do not have demonstrated economic viability.** **(3)** Open pit mineral resources are reported at a cut-off grade of 0.1% Ni. Cut-off grades are based on a price of US \$7.50 per pound, nickel recoveries of 60%, mineralized material and waste mining costs of \$2.80, along with milling, processing and G&A costs of \$7.20. **(4)** Inferred mineral resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. However, it is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated. **(5)** Due to rounding, numbers presented may not add up precisely to the totals provided and percentages may not precisely reflect absolute figures. Source: Kirkham Geosystems, 2020.

Figure 14-21: Plan View of Ni% Blocks & Drill Holes along with Surface Features and Turnagain River Location



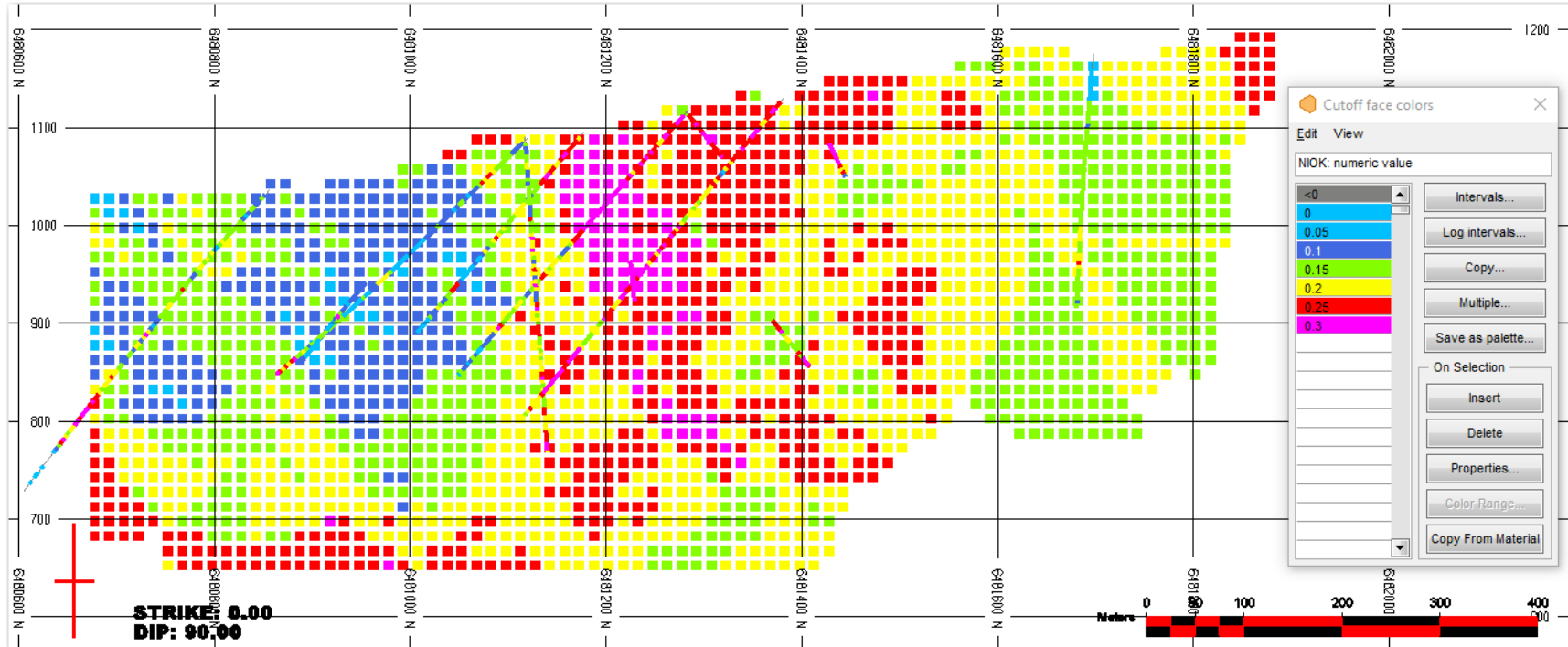
Source: Kirkham Geosystems, 2020

Figure 14-22: Section View of Lithology Coded Blocks & Drill Holes for the Block Model



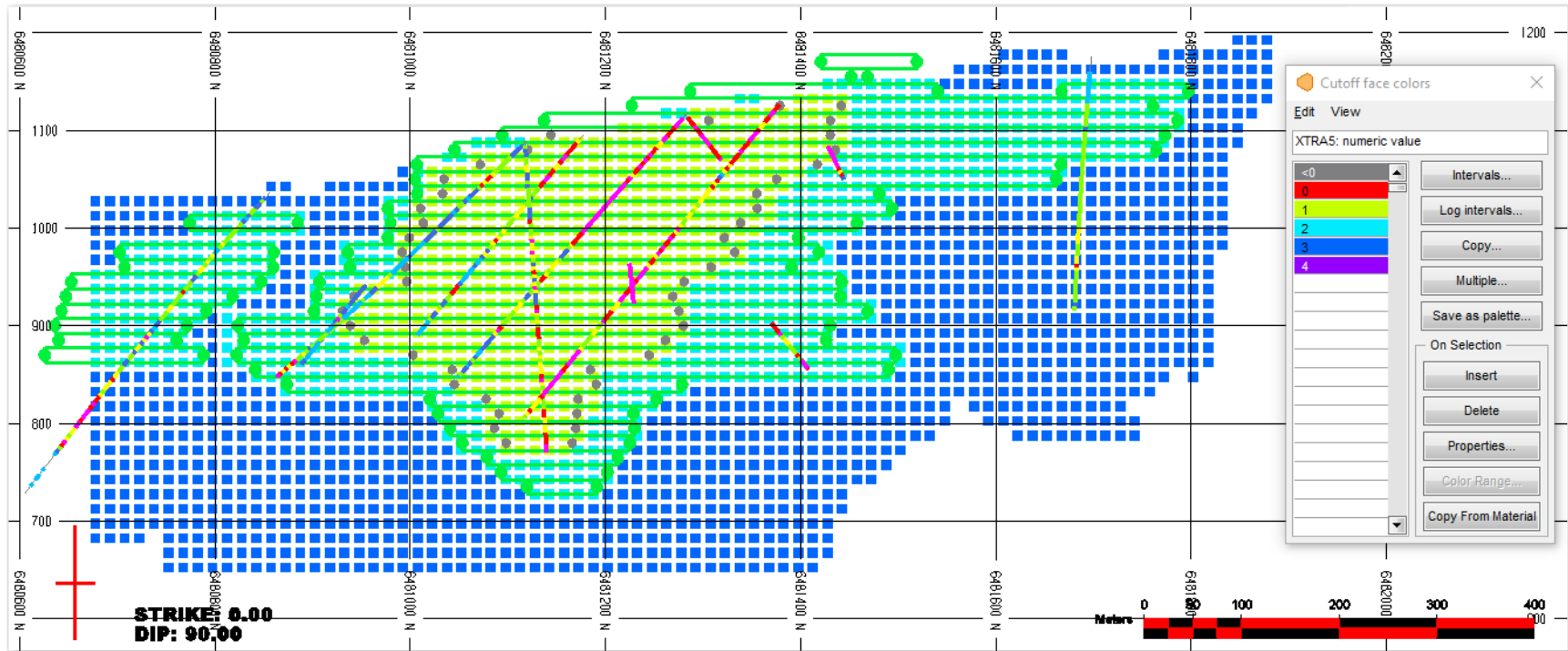
Note: 1 = Wehrlite-Dunite-Serpentinite (red), 2 = Green Dunite (green), 3 = Pyroxenite-Clinopyroxenite-Olivine Clinopyroxenite (yellow), 8 = Dyke (light blue), 9 – Volcanics (dark blue), 10 = Overburden (purple). Source: Kirkham Geosystems, 2020.

Figure 14-23: Section View of Ni% & Drill Holes for the Block Model



Source: Kirkham Geosystems, 2020.

Figure 14-24: Section View of Classification of Blocks & Drill Holes



Note: 1 = Measured (green), 2 = Indicated (light blue), 3 = Inferred (blue). Source: Kirkham Geosystems, 2020.

Differences from the previous resource estimate described in AMC's 2011 PEA are the inclusion of an additional 36 infill drill holes totalling 8,940 m drilled in 2018 in the areas of the conceptual open pit, updated geological modelling and current updated price and cost parameters.

14.15 Discussion on Material Affects to the Mineral Resource Estimate

The resource could be affected should future development options exclude the potential to divert a small section of the Turnagain River. In such a case, either the Hatzl Zone would be mined via its own independent, non-continuous pit or excluded altogether.

In addition, the project as a whole relies upon attaining social license to operate and as such may be affected by First nations and socioeconomic factors; however, these factors are not specific to the resource estimate and affect the project as a whole.

To the extent known, the author is not aware of any legal, title, permitting, taxation, marketing or political factors that would affect the resource estimate.

14.16 Comparison to Previous 2011 Mineral Resource Estimate

Since the 2011 mineral resource update, Giga Metals has performed infill drilling and updated its geological modelling. Differences from the previous resource estimate described in AMC's 2011 PEA are the inclusion of an additional 36 infill drill holes totalling 8,940 m drilled in 2018 in the areas of the conceptual open pit, updated geological modelling, and current updated price and cost parameters. As a result, the measured plus indicated resources have grown due to infill drilling, but the inferred resources have also grown because the volumes of the ultimate conceptual pit have grown (see Table 14.11). This comparison is provided for information purposes only. This comparison should not be interpreted as a statement of mineral reserves; mineral reserves can only be defined in a pre-feasibility or feasibility study.

Table 14.11: Comparison of 2019 & 2011 Consolidated Mineral Resource Statement^(1,2,3,4,5) for the Turnagain Project

Classification	Tonnage (000s)	Ni Grade (%)	Contained Ni (000s lbs)	Co Grade (%)	Contained Co (000s lbs)
2019 Update					
Measured and Indicated	1,073,885	0.22	5,206,051	0.013	312,550
Inferred⁽⁴⁾	1,163,515	0.2176	5,581,627	0.013	333,461
2011 Estimate					
Measured and Indicated	865,482	0.213	4,057,052	0.013	253,061
Inferred⁽⁴⁾	976,295	0.2	4,304,719	0.013	279,807
2011-2019 Change					
Measured and Indicated	208,403	0.007	1,148,999	unchanged	59,489
Inferred⁽⁴⁾	187,220	0.018	1,276,908	unchanged	53,654
Percentage Change					
Measured and Indicated	24.08%	3.50%	28.32%	unchanged	23.51%
Inferred	19.18%	8.70%	29.66%	unchanged	19.18%

Notes: (1) All mineral resources have been estimated in accordance with Canadian Institute of Mining and Metallurgy and Petroleum definitions, as required under National Instrument 43-101. (2) Mineral resources are reported in relation to a conceptual pit shell in order to demonstrate reasonable expectation of eventual economic extraction, as required under NI 43-101; mineralisation lying outside of these pit shells is not reported as a mineral resource. **Mineral resources are not mineral reserves & do not have demonstrated economic viability.** All figures are rounded to reflect the relative accuracy of the estimate and therefore numbers may not appear to add precisely. (3) Open pit mineral resources are reported at a cut-off grade of 0.1% Ni. Cut-off grades are based on a price of US \$7.50 per pound, nickel recoveries of 60%, mineralized material and waste mining costs of \$2.80, along with milling, processing and G&A costs of \$7.20. (4) Inferred mineral resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. However, it is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated. (5) Due to rounding, numbers presented may not add up precisely to the totals provided and percentages may not precisely reflect absolute figures. Source: Kirkham Geosystems, 2020.

15.0 MINERAL RESERVE ESTIMATES

There are no reserves to report at this stage.

16.0 MINING METHODS

16.1 Summary

This section includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that the PEA results based on these resources will be realised.

The Turnagain deposit will be mined using an open pit mining method, employing high volume trucks and shovels. The use of large mining equipment will achieve high mining rates and ensure the lowest possible operational unit costs. The waste and mineralisation will require blasting and typical grade control methods using blast-hole sampling.

For the purpose of this study, extraction from the Horsetrail, Northwest, and Duffy mineralised zones are incorporated in the LOM mine plan with two separate excavations. Previous evaluations have indicated a potential open pit resource in the Hatzl Zone on the east side of the Turnagain River, but that opportunity is not included in the scope of this study. The Turnagain River is a fish habitat and wildlife corridor, so the underlying mineralisation is excluded.

The potential resource contained in the Horsetrail pit is summarised in Table 16.1. These pit shells form the basis of the mine production schedule in this study. It is defined by the 95% sensitivity revenue base case optimisation shell.

Table 16.1: Schedule In-pit Material

Description	Mineralisation (kt)	Ni (%)	Co (%)	S (%)	MHV (\$/t milled)
Measured	249,200	0.23	0.01	0.80	11.4
Indicated	550,551	0.22	0.01	0.62	8.8
Measured & Indicated	799,751	0.220	0.013	0.68	9.60
Inferred	322,225	0.223	0.013	0.41	7.03
Total Stripping (kt)	207,880				
Total Strip Ratio (t:t)	0.19				

Notes: (1) * MHV = mill head value at base case metal pricing. (2) Note: includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

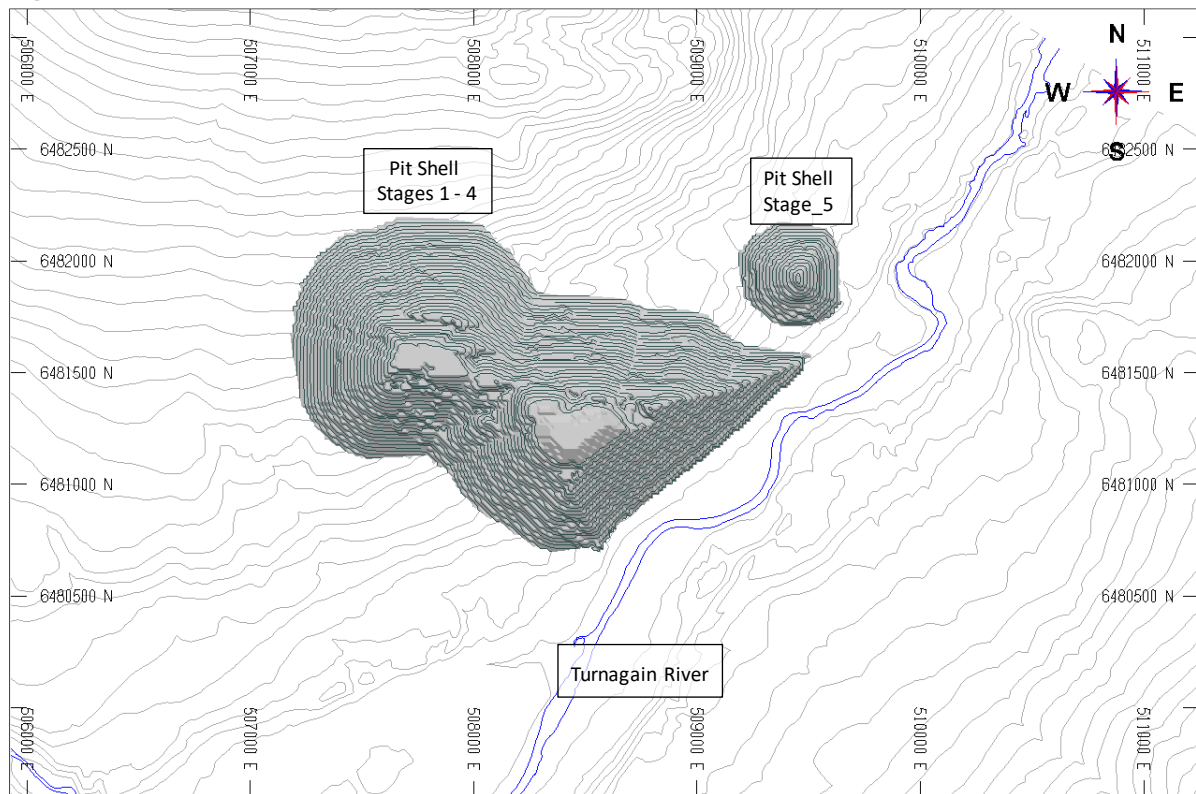
MHV calculations and values described in this section were calculated and utilised for the development of the mine plan with the input parameters listed in this section, and are not necessarily consistent with final values utilised in the site assessment evaluation described in Section 22.

Figure 16-1 shows a plan view of the selected ultimate Horsetrail pit shells used for PEA mine scheduling.

The mine will feed the crusher at an average rate of 45,000 t/d during the first five years and increase to an average of 90,000 t/d thereafter. The resource will be mined for 37 years at these rates based on a 365-day production year.

To access the most economic mineralisation in the early years and provide a smooth strip ratio throughout the life of mine, mineralisation production from the Horsetrail pit is scheduled from five mining phases. Stage 1 will commence at the centre of the pit, where the highest grade and lowest strip ratio will be encountered.

Figure 16-1: Horsetrail Scheduled Pit Shells – Plan View



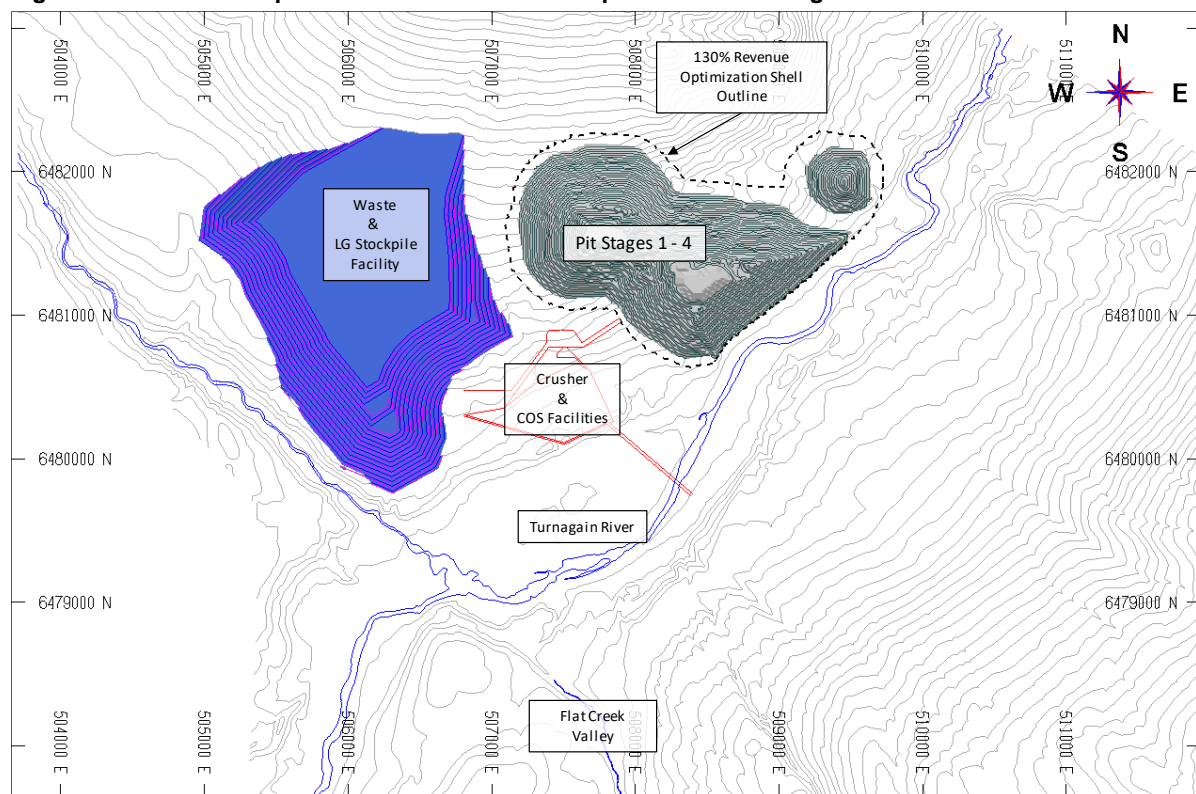
Source: Hatch, 2020.

An elevated cut-off grade will be employed in the initial production years to enhance the economics of the project. Mineralisation that is below the mine high-grade (HG) direct feed cut-off, but of sufficient grade to cover the cost of milling and rehandling once it is hauled out of the pit, will be classified and stockpiled by categorised value for subsequent rehandling. Stockpile reclaim will occur at the end of the mine life or it will be blended with the ROM feed as the

appropriate opportunity arises. Low-grade (LG) stockpiles will be placed in the same facility as the waste dump to avoid additional costs.

Pit waste and LG material will be hauled to a waste dump and stockpile complex southwest of the pit, past the crusher and coarse ore stockpile facilities. The design shown in Figure 16-2 is capable of containing all scheduled waste and LG material in the LOM plan. Current geochemistry data suggest there is insignificant acid generating potential in the waste rock. There is also the potential that if deemed cost effective and geochemically acceptable, waste rock can be utilised as buttress material for the TMF in Flat Creek valley, thus it is conceivable that the waste and LG storage facilities will have minimal impact at the end of mine life. Further studies will be undertaken to confirm this possibility. Figure 16-2 shows the conceptual waste and LG maximum extents dumping plan.

Figure 16-2: Waste Disposal & Mineralisation Stockpile General Arrangement



Source: Hatch, 2020.

16.2 Open Pit Optimisation Study

The optimisation study methodology that was used is widely accepted in the mining industry for preliminary assessments of open pit mining potential. The potential resource for the open pit was evaluated by undertaking pit optimisation studies on the geological model using Hexagon

MineSight® Pseudoflow software, which produces equivalent results as the industry-standard Lerchs-Grossman computer algorithm. The Pseudoflow programming produces results significantly faster than Lerchs-Grossman runs. Various preliminary pit shells were generated from the simulations and analysed. Selected shells were assessed for whether they are appropriate to use for framing the ultimate pit and mining phases.

16.2.1 Optimisation Parameters

Economic values are assigned on measured, indicated, and inferred resource classes as categorised in the resource block model. The preliminary input parameters applied on the optimised pit (Table 16.2) are estimated based on previous studies and discussions with Giga Metals. Costs, exchange rate, recoveries, and pit slope angles are preliminary and are specific for this optimisation study only. Values utilised in the pit optimisation process were determined and applied early in this PEA study, and are not necessarily consistent with final values utilised in the cashflow and site assessment evaluation.

Table 16.2: Preliminary Design Parameters for Optimised Pit

Parameter	Units	Value
Exchange Rate	(CAD/US)	0.75
Nickel Price	US\$/lb	8.00
Cobalt Price	US\$/lb	20.00
Concentrate Grade	(%)	18.0
Concentrate Transport Cost	(US\$/dmt)	169.20
Payable* (of recovered metal value)	(%)	70.56
Total Milling & Site (incl. G&A) Unit Operating Cost	(US\$/t milled)	6.29
Total Base Unit Mining Cost	(US\$/t mined)	2.29
Incremental Bench Unit Costs	(US\$/t/bench)	0.04
Stockpile Rehandling	(US\$/t moved)	0.92
Overall Wall Angles	(degrees or °)	45°
River Boundary Offset	(m)	65

Note: *Payable is inclusive of metals payable, treatment and refining costs.

Process recoveries for nickel and cobalt were provided by Giga Metals (see Section 13 for a description of the process used to determine recoveries). The nickel recovery formula used for an 18% concentrate for the optimisation sensitivity runs was:

$$\%Ni_Recovery = 2.293*(\%S)^3 - 17.079*(\%S)^2 + 42.382*(\%S) + 28.916$$

$$Total\ recovery\ cap\ (maximum) = 63.96\%$$

$$\%Co_Recovery = \%Ni_Recovery$$

No other byproduct metals were included in the valuations, although copper, palladium and platinum were included in previous project cashflow evaluations.

16.2.2 Turnagain River Restriction

A mining restriction will limit mining activity to either side of the Turnagain River. Until further studies are carried out to assess other mining scenarios, the river will not be disturbed. The limit is determined by approximating the high water level, which in previous evaluations was deemed to be 1,015 masl along the river banks. The pit crest lines are offset from this contour by 65 m, which includes 50 m for a no-disturbance zone and 15 m for an access corridor. These preliminary estimates will be updated as necessary.

16.2.3 Pit Optimisation Variable – Net Metal Value

The pits were optimised on the net metal value that is calculated from the Ni% and Co% grades in the 3D block model. This variable represents the combined net metal values for nickel and cobalt in the mineralisation. It was calculated in US dollars, and is the sum of the net nickel value and net cobalt value. They are derived as follows:

- Net metal value (\$/t) nickel = 2,204.6 lb/t x Ni grade (%) x payable nickel (%) x net nickel price (\$/lb) at mine gate x process recovery (%)
- Net metal value (\$/t) cobalt = 2,204.6 lb/t x Co grade (%) x payable cobalt (%) x net cobalt price (\$/lb) at mine gate x process recovery (%)

The parameters that were used to calculate the net metal value for the base case are provided in Table 16.2. The net metal value calculated for the base case is carried in the model as the NSR value. A mill head value (MHV) method was used in the evaluations, wherein the MHV represents the total value per tonne milled if it were to be processed (i.e., the value at the crusher pocket) and is the net value of NSR less mill processing, TMF and G&A.

16.2.3.1 Pit Optimisation Results

Table 16.3 shows the mineralisation and waste quantities contained in the optimised pit shells generated against the net metal value variable. The base case is Shell 39, where the input metal price is US\$8.00/lb for nickel and US\$20.00/lb for cobalt, and the shell contains 1.26 billion tonnes of mineralisation at a 0.15 to 1 strip ratio. The cut-off grade applied is on a MHV value of \$0.01/t (i.e., breakeven grade cut-off).

The other shells were generated by varying net metal value to test the sensitivity of the resource, assess possible pit phases and the opportunities for expansion. Figure 16-3 illustrates the contained mineralisation in the LG shells.

The results from this set of optimised pits indicate that the Turnagain deposit total feed is insensitive to metal prices until nickel and cobalt prices exceed around 60% of the base case. The 95% revenue case was selected as the ultimate shell. Larger pits mine significant material at

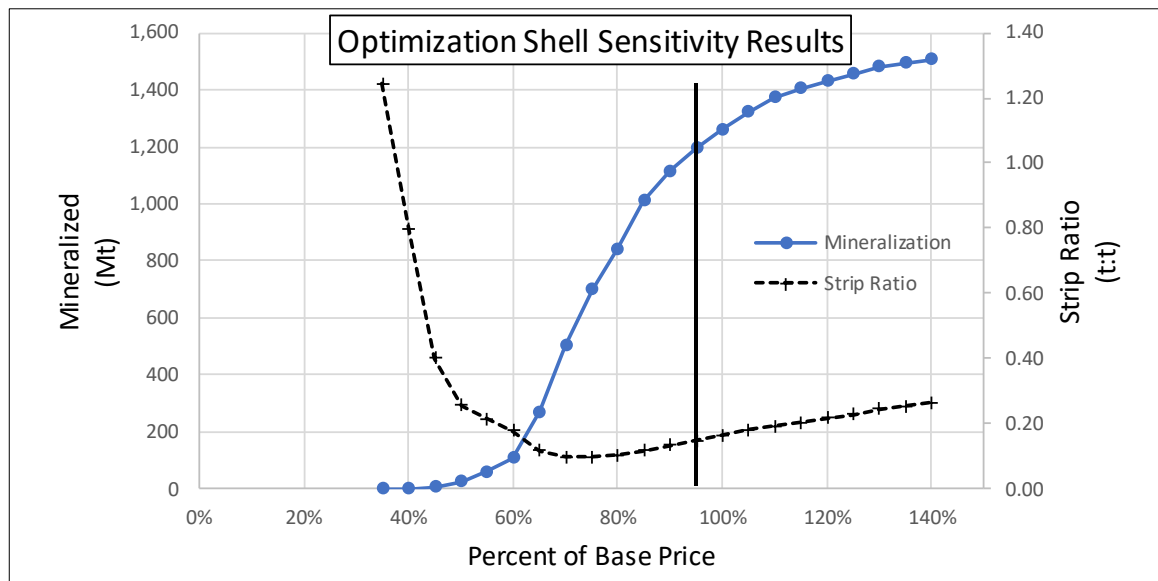
no value, while smaller ones would leave a lot of value behind. Of note, the ultimate shell selected in this evaluation did bottom out at the lower limit of modelled nickel grades.

Table 16.3: Optimised Pit Shells (Cut-off on \$0.01/t Milled MHV Value)

% of Metal Price (Base Case)	Optimised Shell	Mineralisation (Mt)	Ni (%)	Co (%)	S (%)	MHV (US\$/t Milled)	Strip (Mt)	Strip Ratio (t:t)
35%	Pit_52	0	0.37	0.02	1.65	23.64	0.1	1.24
40%	Pit_51	0	0.33	0.02	1.71	21.13	0.3	0.79
45%	Pit_50	7	0.29	0.02	1.19	15.95	2.7	0.40
50%	Pit_49	25	0.28	0.02	1.13	14.32	6.5	0.26
55%	Pit_48	59	0.26	0.02	1.06	12.73	12.6	0.21
60%	Pit_47	106	0.25	0.01	1.00	11.49	18.9	0.18
65%	Pit_46	270	0.23	0.01	0.82	9.54	31.7	0.12
70%	Pit_45	500	0.23	0.01	0.75	8.59	49.1	0.10
75%	Pit_44	698	0.23	0.01	0.68	8.00	67.7	0.10
80%	Pit_43	842	0.23	0.01	0.65	7.62	86.9	0.10
85%	Pit_42	1,010	0.22	0.01	0.61	7.21	118.3	0.12
90%	Pit_41	1,115	0.22	0.01	0.58	6.99	147.0	0.13
95%	Pit_40	1,196	0.22	0.01	0.57	6.82	175.7	0.15
Base Case	Pit_39	1,262	0.22	0.01	0.55	6.68	205.9	0.16
105%	Pit_38	1,322	0.22	0.01	0.54	6.55	239.1	0.18
110%	Pit_37	1,373	0.22	0.01	0.53	6.43	264.7	0.19
115%	Pit_36	1,405	0.22	0.01	0.52	6.36	285.5	0.20
120%	Pit_35	1,432	0.22	0.01	0.52	6.31	311.3	0.22
125%	Pit_34	1,457	0.22	0.01	0.52	6.25	333.0	0.23
130%	Pit_33	1,481	0.22	0.01	0.51	6.20	360.2	0.24
135%	Pit_32	1,493	0.22	0.01	0.51	6.18	376.2	0.25
140%	Pit_31	1,506	0.22	0.01	0.51	6.15	396.5	0.26

Note: Includes Inferred Resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

Figure 16-3: Sensitivity of Contained In-Pit Resource & Respective Strip Ratios



Source: Hatch, 2020.

16.2.3.2 Updated Planning Parameters Used for Mine Scheduling

During the course of this PEA, the metal recovery formula was revised, base metal pricing was updated, and mining costs were refined based on the mine production schedule. As a confirmation check, the base case optimised pit was re-generated with the updated parameters and costs for comparison against results of the preliminary input criteria. The revised mining and processing costs are shown in Table 16.4.

Table 16.4: Updated Design Parameters for Optimised Pit – Base Case

Parameter	Units	Amount
Exchange Rate	(CAD/US)	0.77
Nickel Price	US\$/lb	9.00
Cobalt Price	US\$/lb	20.00
Concentrate Grade	(%)	18
Concentrate Transport Cost	(US\$/dmt)	170
Payable* (of recovered metal value)	(%)	70.56
Total Milling & Site (incl. G&A) Unit Operating Cost	(US\$/t milled)	5.80
Total Base Unit Mining Cost	(US\$/t mined)	\$2.31
Incremental Bench Unit Costs	(US\$/t/bench)	\$0.03
Stockpile Rehandling	(US\$/t moved)	\$0.92
Overall Wall Angles	(degrees or °)	45°
River Boundary Offset	(m)	65
% Ni Recovery	(%)	=11.895*LN(%S)+56.176

Note: *Payable is inclusive of metals payable, treatment and refining costs.

The contained mineralisation and grades for the revised base case optimised pit is summarised in Table 16.5. It is reported on the respective MHV cut-off values of \$0.01/t for each scenario.

Table 16.5: Base Case Optimised Pit – Updated Cost Parameters

Scenario	Mineralisation (Mt)	Ni (%)	Co (%)	S (%)	MHV (US\$/t Milled)	Strip (Mt)	Strip Ratio (t:t)
Preliminary Base Case	1,262	0.223	0.013	0.552	6.68	205.9	0.16
Updated Base Case	1,251	0.217	0.013	0.588	8.43	281.7	0.23
Difference (Update - Preliminary)	-12	-0.005	0.000	0.037	1.75	75.8	0.06
% Variance	-1%	-2%	0%	7%	26%	37%	38%

Note: Includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

The results indicate that the optimised pit with the updated input criteria is a slightly larger excavation but with marginally fewer feed tonnes (-1%) and an incremental strip ratio increase of 0.06 (0.23 versus 0.16). The results confirm the applicability of the preliminary shell selection process for scheduling and PEA evaluation purposes.

The updated parameters were implemented in model valuations for mine production scheduling as discussed in Section 16.5. The process for selecting the ultimate pit should be further refined at the pre-feasibility study stage relative to measured, indicated and inferred mineralisation categories and should include sensitivity analysis and discounting. It is important to note that the contained mineralisation in this simulated pit shell is only an indication of the potential open pit mineable resource and should not be relied on as a recoverable resource.

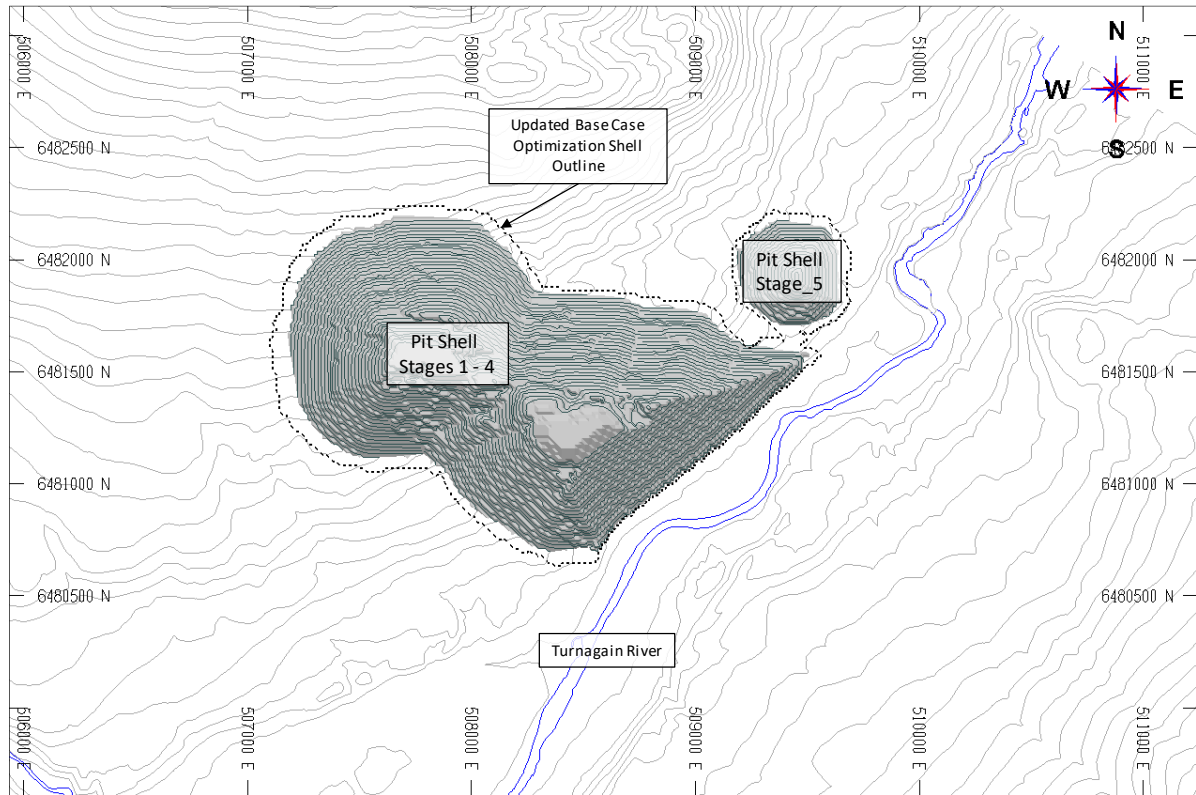
Figure 16-4 on the following page is a plan view of the revised base case optimised pit shell outline, compared to the ultimate selected shell (Pit 40) for mine planning in this PEA.

16.3 Pit Designs

Smoothed pit designs were not developed for this study, as optimised pit shells are sufficient for this PEA analysis and detailed pit designs at this stage will not necessarily improve mine planning accuracy, given the relatively large size of excavations anticipated along with the preliminary level of current pit slope geotechnical analysis.

Pit stages were identified from the pit optimisation sensitivity runs based on step changes in pit values. Additionally, a minimum 100 m pushback width was incorporated to facilitate productive efficient mining operations. The ultimate selected shell provides sufficient material for a mine life of 37 years (1.12 Bt), and for this study, five stages are planned. As the project develops and further knowledge is gained regarding the basic economics, pit geotechnical and geometallurgy, smoothed designs and more refined stage selection can be implemented.

Figure 16-4: Plan View of Updated Base Case Shell Outline compared to PEA Selected Planning Shells

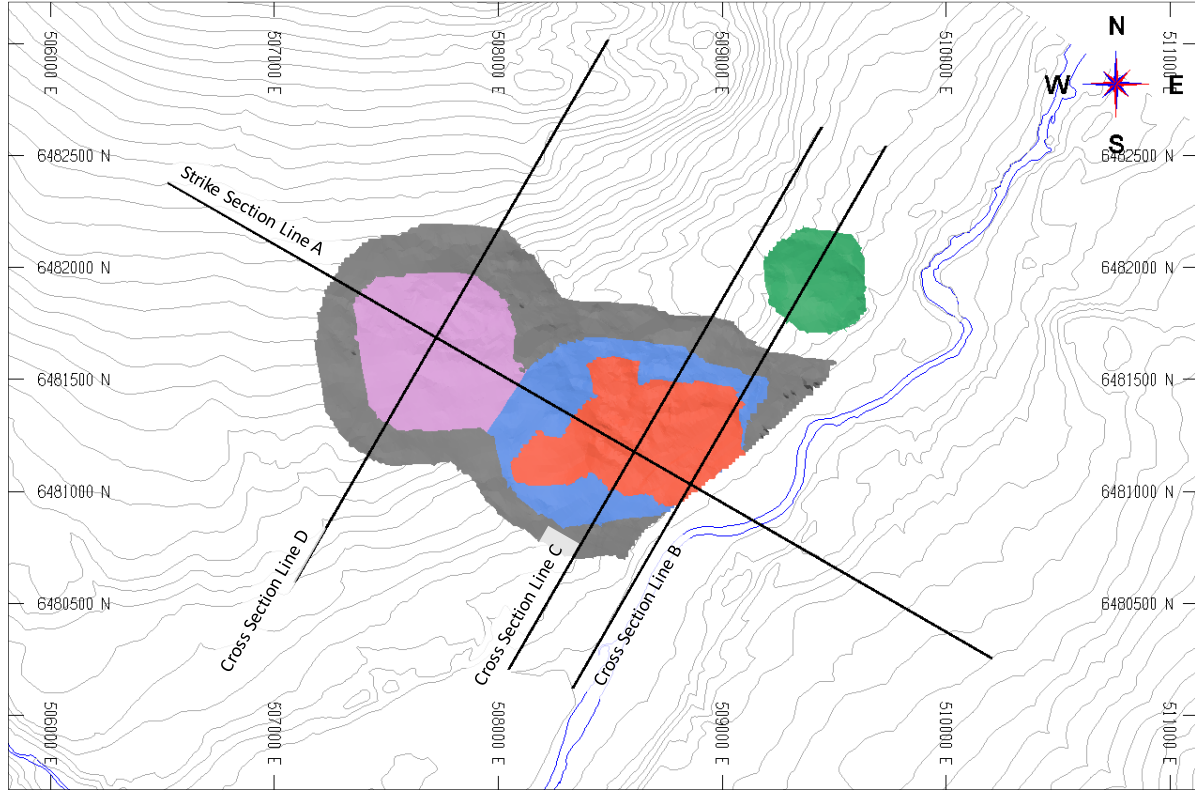


Source: Hatch, 2020.

The dimensions of the primary excavation containing Stages 1 through 4 (Figure 16-1 above) are approximately 2 km in length, and 1.1 km wide. Stage 5 is a circular pit with top diameter of 0.5 km. The bottom of the Stage 4 pit is at 645 m elevation; the highest point along the pit rim is 1,340 m elevation at the northwest end.

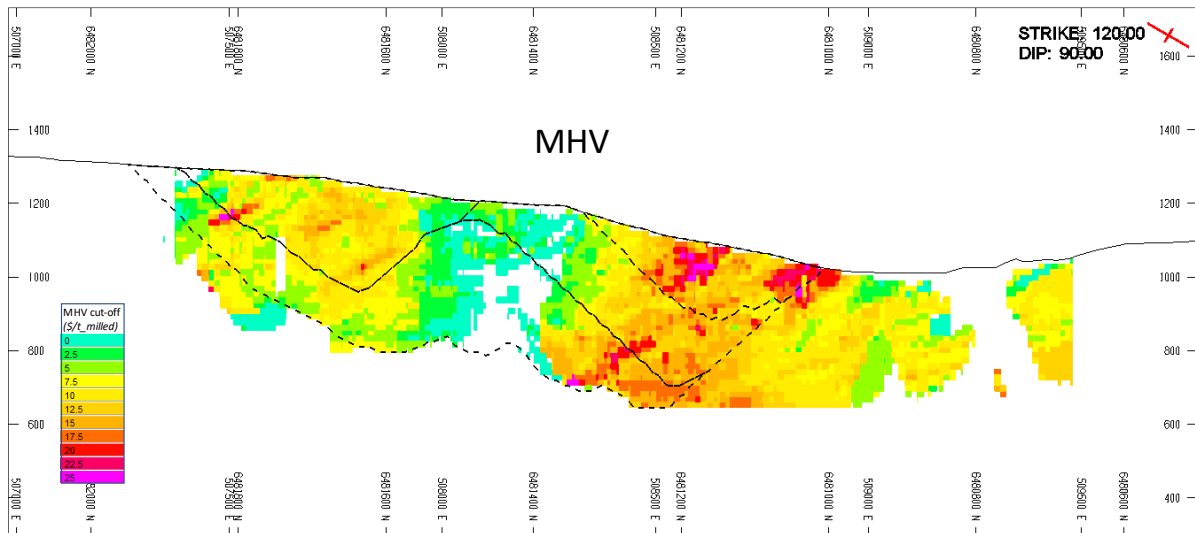
Figure 16-5 is a reference for the locations of the non-orthogonal cross-sectional views in Figures 16-6 to 16-11. The figures show the block model MHV (scheduled) and five scheduled pit stage shells overlain in all sections. Nickel (Ni%) and sulphur (S%) grades are shown in two respective figures to illustrate the impact of these grades on the MHV values along the primary deposit strike length (Section A).

Figure 16-5: Horsetrail & Ultimate Pit Shell Outlines with Reference Lines



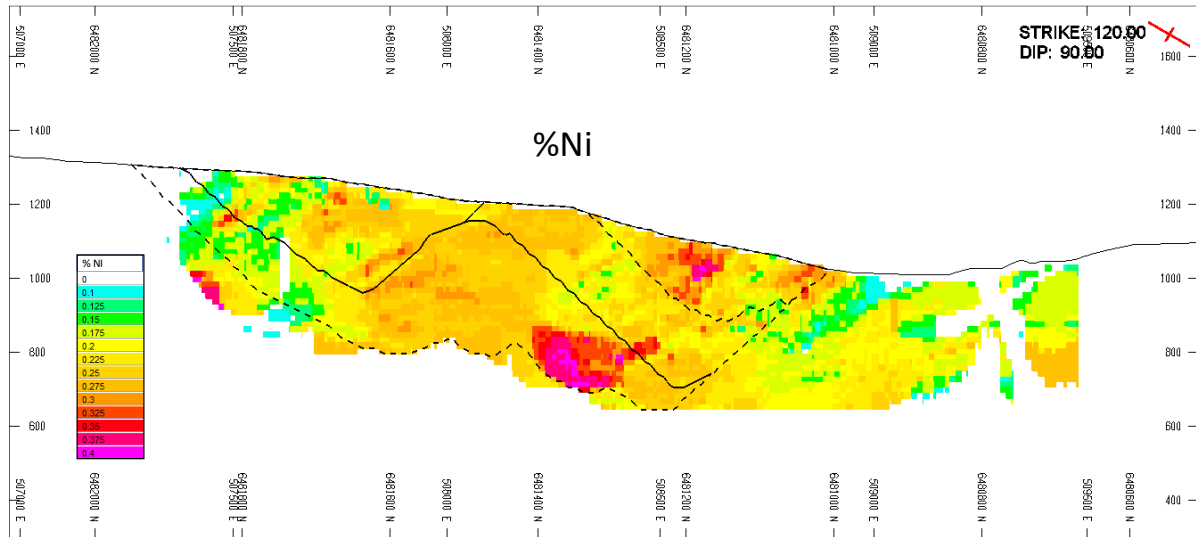
Source: Hatch, 2020.

Figure 16-6: Block Model MHV Values – Strike Section A Looking NE



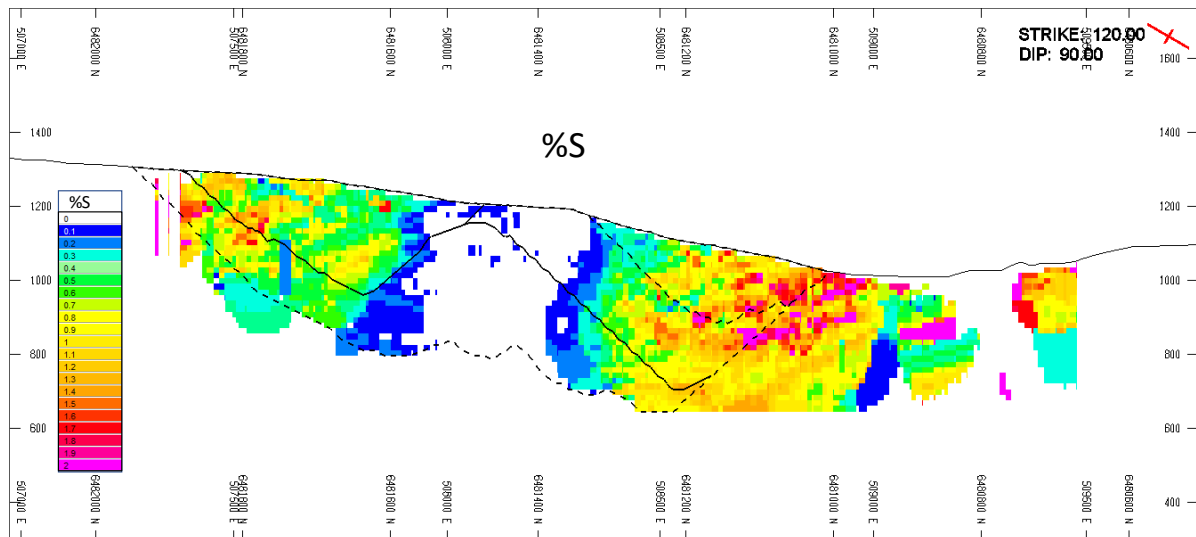
Source: Hatch, 2020.

Figure 16-7: Block Model Ni Values – Strike Section A Looking NE



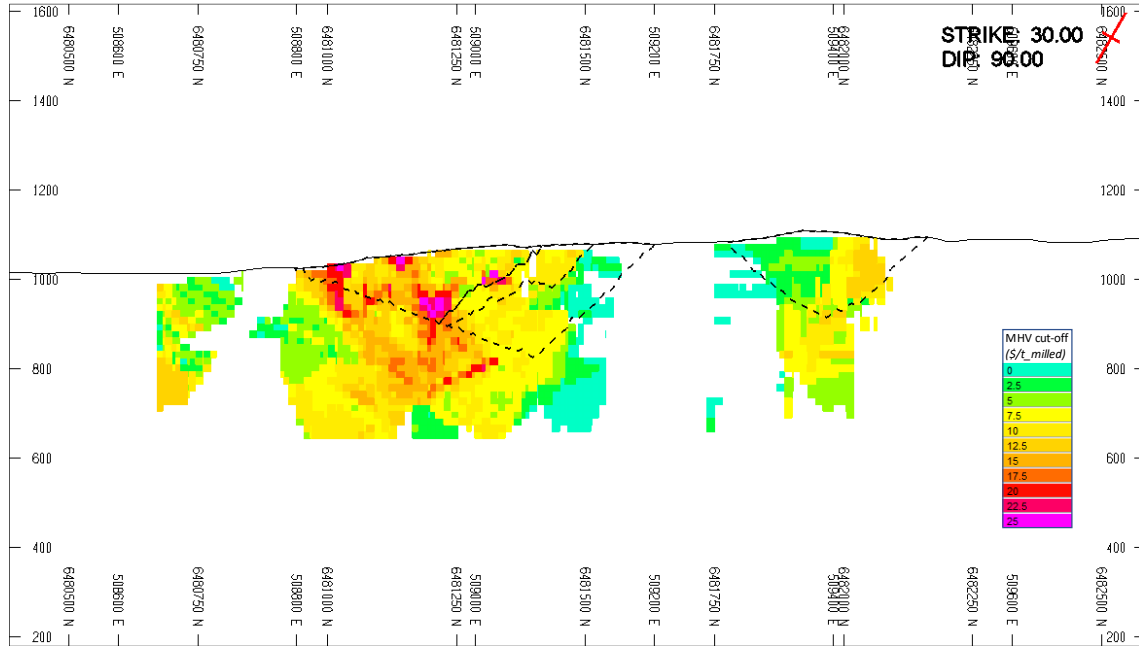
Source: Hatch, 2020.

Figure 16-8: Block Model S Values – Strike Section A Looking NE



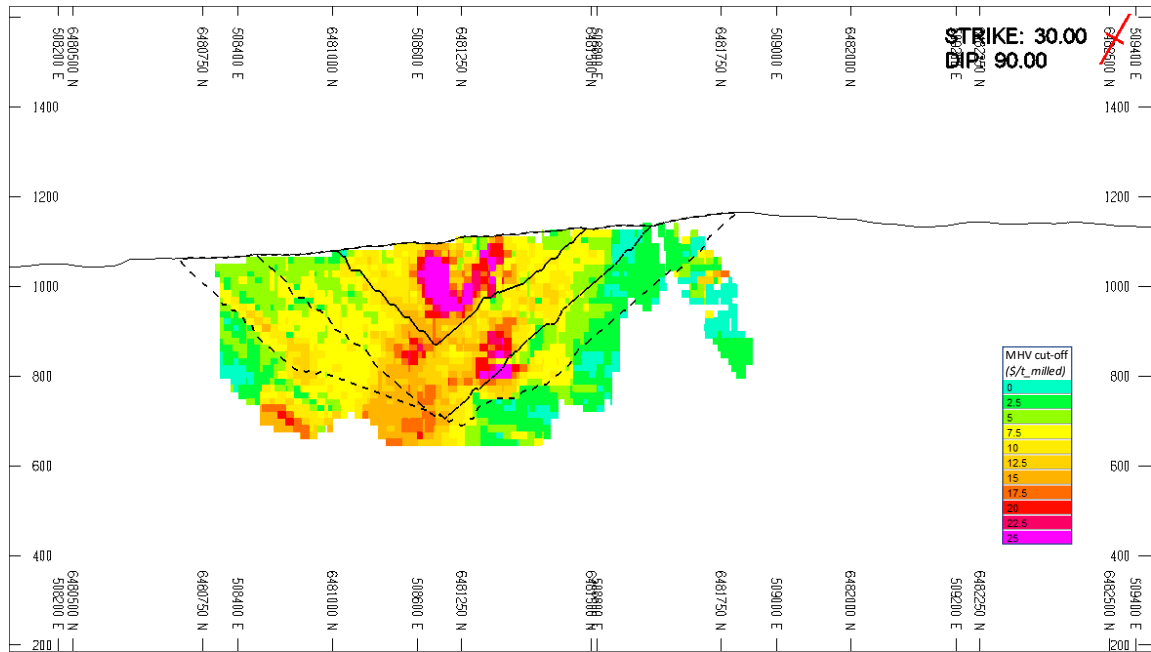
Source: Hatch, 2020.

Figure 16-9: Block Model MHV Values – Cross-section B Looking NW



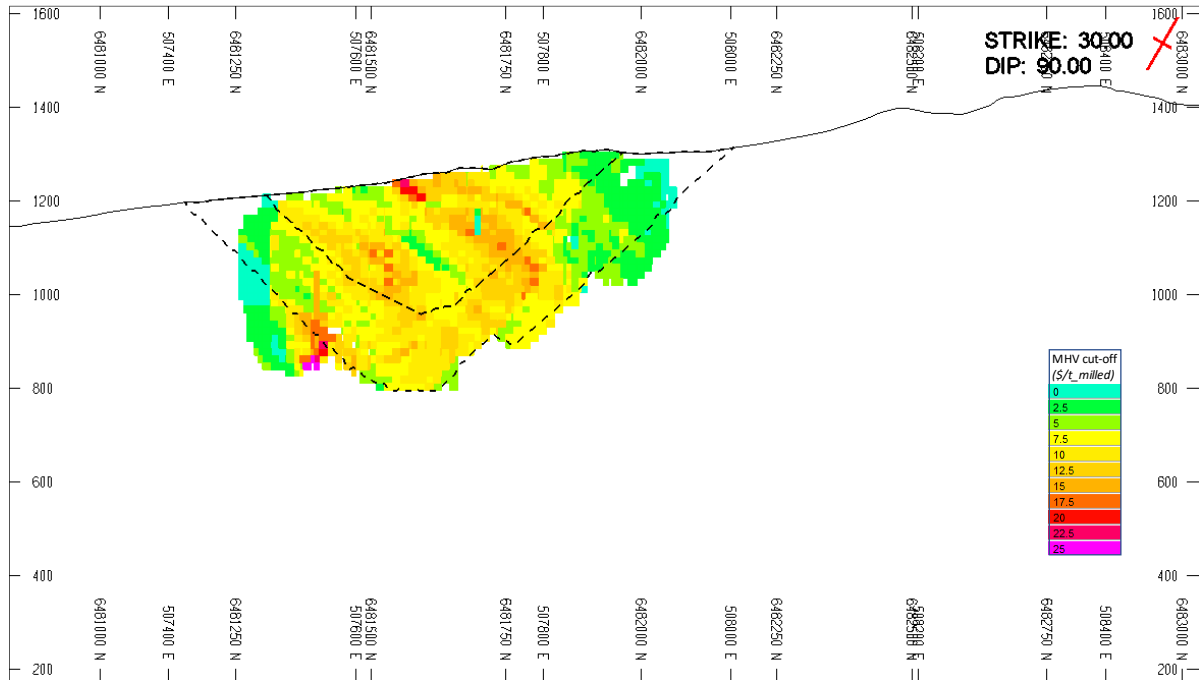
Source: Hatch, 2020.

Figure 16-10: Block Model MHV Values – Cross-section C Looking NW



Source: Hatch, 2020.

Figure 16-11: Block Model MHV Values – Cross-section D Looking NW



Source: Hatch, 2020.

16.3.1 Pit Slope Assumptions

The overall pit slopes have been assigned to an overall maximum angle of 45°. For preliminary open pit analysis, 45° is a typically assumed value and preliminary geotechnical assessments (Piteau, 2008) support this assumption. Pit slope angles and design parameters will require further review and geotechnical assessments for the next level of study.

Groundwater conditions will affect the stability of the pit slopes. It is anticipated that the bedrock is competent and the highwalls will be stable if an effective dewatering plan is implemented to keep them well drained. Limited hydrogeological studies have been undertaken; these will be important during the next level of study, particularly with regard to the proximity of Turnagain River.

16.3.2 In-Pit Resource Potential

The potential resource estimate by mineralisation domain and classification contained within the ultimate scheduled Horsetrail pit is summarised in Table 16.6.

Scheduled tonnes and grades are different from the values listed in the pit optimisation shell selection phase (Section 16.2.1), because of the changes in input parameters during the intermediate parameter and recovery update that occurred during the course of this PEA. Additionally the application of a LG minimum cut-off accounting for rehandling affected the total tonnes available for scheduling.

Table 16.6: Horsetrail Pit Potential Resource

Domain	Classification	Mineralisation (Mt)	MHV (\$/t Milled)	Ni (%)	Co (%)	S (%)
Dunites and Serpentinised_Wehrlites	Measured	142	12.21	0.235	0.014	0.796
	Indicated	388	9.38	0.222	0.013	0.610
	Inferred	248	7.66	0.230	0.013	0.396
Green Dunite	Measured	61	9.93	0.235	0.014	0.601
	Indicated	92	7.33	0.231	0.013	0.409
	Inferred	47	4.78	0.233	0.013	0.159
Pyroxenes	Measured	44	11.28	0.202	0.014	1.086
	Indicated	63	7.84	0.170	0.012	1.006
	Inferred	20	6.14	0.158	0.012	0.988
Dyke	Measured	0	3.99	0.135	0.009	0.599
	Indicated	3	4.69	0.165	0.007	0.411
	Inferred	0	3.16	0.146	0.007	0.315
Volcanics	Measured	1	2.92	0.120	0.008	0.653
	Indicated	6	3.50	0.129	0.009	0.608
	Inferred	7	2.79	0.100	0.009	1.130
Grand Total	Measured	249	11.42	0.228	0.014	0.798
	Indicated	551	8.78	0.216	0.013	0.621
	Inferred	322	7.03	0.223	0.013	0.414

16.3.3 Reported Grade Items

The reported grade items are:

- MHV: this is the mill head value combined net smelter return value for contained metal as \$/t mineralisation less processing, TMF and G&A unit costs (i.e., the total value at the crusher pocket)
- Ni: total nickel grade percentage
- Co: cobalt percentage
- S: sulphur percentage

16.3.4 Cut-off Grade

The scheduled minimum MHV cut-off grade is estimated to be the minimum value of the mineralisation contained in the designed ultimate pit that is sufficient to cover the cost of stockpile handling, stockpile maintenance, and the incremental costs for the haul distance from the stockpile to the crusher. The potential pit scheduled resource estimate is calculated as:

$$\text{MHV LG (minimum) cut-off grade} = \$1.20/t.$$

For the purposes of mine production scheduling, elevated (HG) cut-off grades were implemented based on total in-shell tonnes/grade resources ratios and expected mine fleet productivities. The respective applied schedule cut-off grades are summarised in Table 16.7.

Table 16.7: Scheduling MHV Material Cut-off Grades

Pit Stage	LG Cut-off (MHV \$/t)	HG Cut-off (MHV \$/t)
Stage_1	1.20	10.00
Stage_2	1.20	8.00
Stage_3	1.20	6.50
Stage_4	1.20	4.00
Stage_5		1.20

During scheduling two categories of LG were applied with the intention of making higher value stockpiled material available for periods where strip ratios were naturally higher and to supplement grades when direct feed grades dipped. The bulk of LG material is intended for processing during the late stages of the mine life.

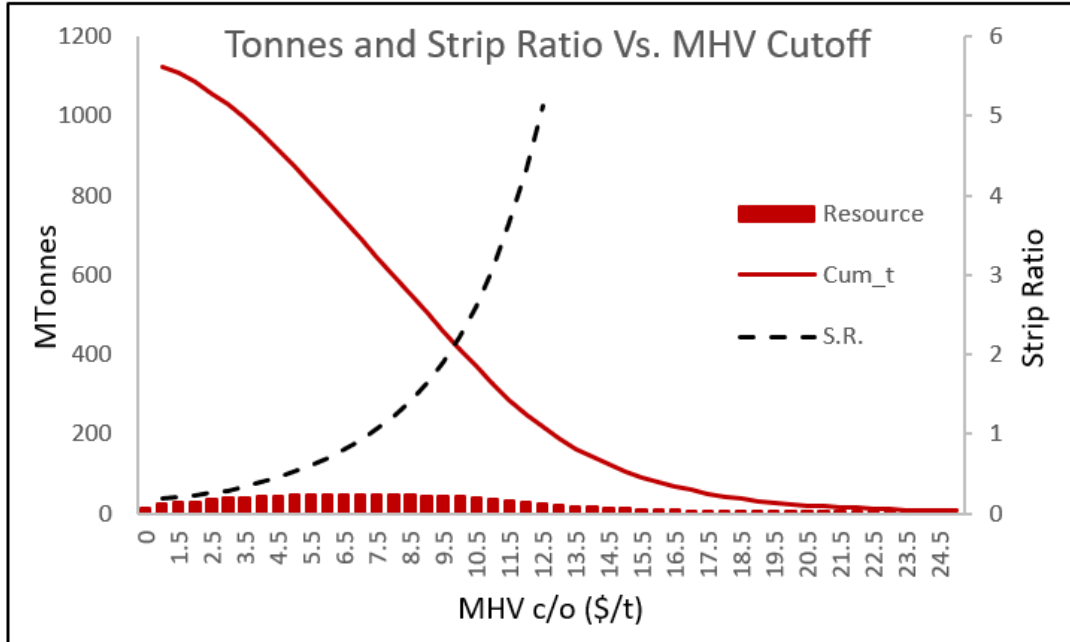
The relatively low strip ratio of the Horsetrail deposit provides significant opportunity to utilise strategic stockpiling to improve dynamic feed values as the pits are developed over the life of mine. However, the opportunity is relatively limited to the immediate circumstances involved, as illustrated by the grade tonnage and strip ratio curves shown in Figure 16-12. The strip ratio curve is extremely steep particularly after a cut-off grade of \$7.50 MHV, where the effective strip ratio is 1:1 (i.e., stripping ratios are very sensitive to increased cut-off grades above MHVs of \$7.50).

Figure 16-12 summarises the total scheduled tonnes contained in the ultimate shell, while the applied cut-offs listed in Table 16.7 were determined through the respective shell tonne grade curves. The analysis on the cut-off grades will be re-assessed in future studies.

16.3.5 Mineralisation Dilution

The Turnagain deposit will be mined by open pit with large trucks and shovels. Large mining equipment will be used to achieve high mining rates, ensuring the lowest possible unit costs for mine operations. The waste and mineralisation will require blasting and typical grade control methods using blast-hole sampling. Some dilution is anticipated, specifically when waste is mixed with mineralisation during blasting and excavation activities. The modelled block dimensions are 15 m x 15 m x 15 m, which in consideration of the fleet unit sizes is a mineable unit; therefore, dilution and recovery factors for this evaluation have been set at 0% and 100%, respectively.

Figure 16-12: Scheduled Ultimate Shell Grade & Tonnage Relationships



Source: Hatch, 2020.

Waste is defined to be material below the cut-off grade. The resource model suggests that the dilution material will generally consist of metal grades that are marginally less than economic. The minimum cut-off grade applied in this study is an MHV value that is above the calculated economic cut-off value. Therefore, potential dilution material will most likely be of economic value. It is anticipated that the overall grade of the in-pit resource will not be significantly impacted by dilution. Therefore, for this scoping-level study, it is assumed that dilution and mineralisation losses will not be material. This assumption will be evaluated in more detail at the next level of study.

16.4 Mine Plan Development

16.4.1 Preliminary Mining Phases

For the purpose of this study, all pit development will be on the west side of Turnagain River. Pit phases are determined to allow for mine development that will generate maximum cash flow in the initial years and balanced pushbacks thereafter.

The first pit stage, Stage_1, will be in the central zone of the Horsetrail pit with minimal waste stripping. This stage targets near-surface higher value material (Figure 16-6 and Figure 16-10). The second phase, Stage_2, will be a second separate excavation phase to the north that targets the next most accessible source of higher value material. Stage_3 is a pushback of Stage_1 that connects with Stage_2, while Stage_4 is the final pushback encapsulating the previous mine phases and limited by the Turnagain River boundary. Stage_5 is a standalone pit located to the southeast of the main Horsetrail pit. The Stage_5 is the lowest grade (value) phase of the five.

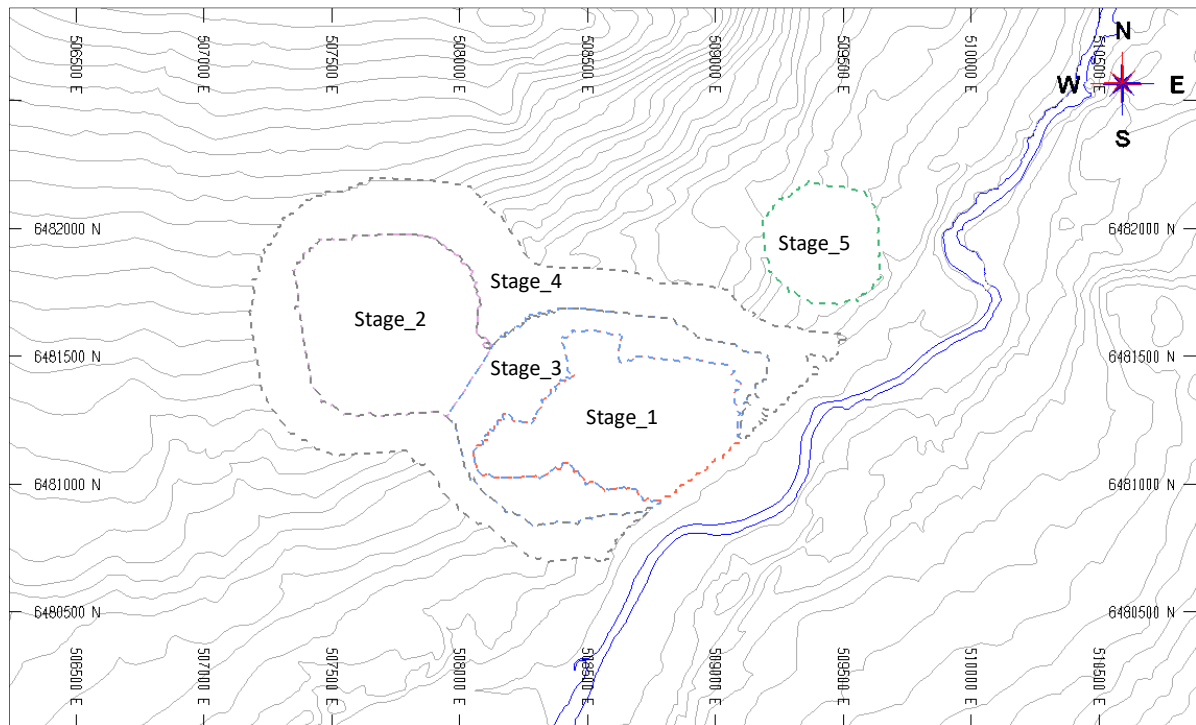
The potential and scheduled Horsetrail pit resource by phase is shown in Table 16.8 and Figure 16-13. A further 66 Mt of material above break-even MHV, but below the applied LG cut-off value (Table 16.7), is also contained within the scheduled optimisation shells.

Table 16.8: Potential Resource by Horsetrail Pit Phases

Pit Phase	Mineralisation (kt)	Waste (kt)	SR (t:t)	MHV (\$/t)	Ni (%)	Co (%)	S (%)
Stage_1	102,322	7,195	0.07	14.1	0.25	0.02	0.99
Stage_2	155,009	10,183	0.07	10.3	0.22	0.01	0.69
Stage_3	237,436	18,084	0.08	10.0	0.22	0.01	0.72
Stage_4	596,710	159,292	0.27	7.3	0.22	0.01	0.48
Stage_5	30,498	13,125	0.43	6.2	0.22	0.01	0.28
Total Horsetrail	1,121,976	207,880	0.19	8.86	0.22	0.01	0.60

Note: Includes Inferred Resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

Figure 16-13: Horsetrail Pit with Mining Phases – Plan View



Source: Hatch, 2020.

16.5 Mine Production Schedule

The annual mill steady state feed rate for the plant Phase_1, Years 1 through 5, is set at 45 kt/d (16.4 Mt/a) and for the balance of the mine life, Years 6 through 37, at 90 kt/d (32.9 Mt/a). Previous studies implemented variable feed rates with the SAG mill comminution circuit configuration, while for this study an HPGR circuit has been implemented. This is understood to be less sensitive to material hardness as per throughput rates.

Implementing a cut-off grade strategy is commonly used to optimise the mineralisation feed to the mill so that the NPV of the project is maximised. During the life of mine, mineralisation mined above the respective pit shell cut-off grades listed in Table 16.7 will be directly fed to the mill. Mineralisation below the HG cut-off but above the respective LG cut-offs will be stockpiled. In developing the mine production schedule, LG has been further split into material above \$6.00 MHV and below. The higher value LG material is scheduled for rehandling intermittently when beneficial to boost grades and or reduce required stripping. The lower value LG material is scheduled for rehandling after completion of the pits. Due to the low strip ratio of the deposit, it is foreseen that operators will be able to take advantage of a variable direct feed cut-off based on equipment productivities on site and the active proportion of waste material for any given period to maximise income.

Oxidation of mineralisation that has been stockpiled over a long period may be a concern, as process recoveries on the reclaimed material may be affected. Metallurgical tests will determine whether the assumed recoveries are sustainable after re-handling and long-term storage and verify that the cut-off grade(s) and stockpiling strategy is viable.

A preliminary production forecast is shown in Table 16.9. Pre-stripping will not be necessary, as the initial mineralisation feed will be near the surface and accessible when the plant starts up. Over the life of the pit, approximately 1,122 Mt of mineralisation will be fed to the mill, of which 881 Mt will be directly from the pit and 241 Mt will be stockpiled and reclaimed largely at the end of mine life when the pits are depleted. The average strip ratio (waste/mineralisation) is 0.2 for LOM and peaks in Year 17 at 0.7. This ratio may be somewhat misleading, as mineralisation stockpiling activity is not represented. Table 16.10 summarises the actual and effective strip ratios by grouped periods incorporating stockpile material.

Table 16.9: Production Forecast

Period	Direct Feed (Mt)	To Stockpile (Mt)	Stockpile Reclaim (Mt)	Plant Feed (Mt)	Ni (%)	Co (%)	S (%)	Waste (Mt)	Recovered Ni (kt)	Strip Ratio (t:t)
Pre-prod	-	-	-	-	-	-	-	-	-	-
1	10.68	5.62	-	10.68	0.252	0.015	0.782	4.16	14.3	0.3
2	16.43	7.39	-	16.43	0.253	0.015	0.978	2.35	23.2	0.1
3	16.43	4.97	-	16.43	0.26	0.016	1.148	0.67	24.7	0
4	16.43	2.74	-	16.43	0.261	0.016	1.313	0.01	25.4	0
5	16.43	7.46	-	16.43	0.272	0.016	1.206	3.13	26.1	0.1
6	31.21	10.5	-	31.21	0.234	0.014	0.703	3.65	38.0	0.1
7	32.85	13.21	-	32.85	0.231	0.013	0.761	1.96	40.1	0
8	32.85	8.3	-	32.85	0.232	0.013	0.808	2.82	40.8	0.1
9	32.85	11.2	-	32.85	0.241	0.014	0.586	5.04	39.4	0.1
10	32.85	15.18	-	32.85	0.224	0.013	0.577	7.67	36.5	0.2
11	32.85	14.09	-	32.85	0.211	0.013	0.767	3.36	36.7	0.1
12	32.85	7.86	-	32.85	0.214	0.014	0.811	0.64	37.8	0
13	32.85	2.14	-	32.85	0.224	0.014	0.893	0.01	40.4	0
14	32.85	4.35	-	32.85	0.242	0.015	1.046	9.35	45.1	0.3
15	27.85	9.14	5	32.85	0.232	0.014	0.606	25.4	38.2	0.7
16	17.85	7.62	15	32.85	0.211	0.012	0.44	14.61	32.2	0.6
17	12.85	9.46	20	32.85	0.206	0.012	0.507	16.63	32.6	0.7
18	25.35	9.85	7.5	32.85	0.202	0.012	0.554	13.33	32.6	0.4
19	32.85	14.24	-	32.85	0.194	0.012	0.676	9.08	32.9	0.2
20	32.85	14.66	-	32.85	0.201	0.012	0.675	10.22	34.0	0.2
21	32.85	15.53	-	32.85	0.208	0.012	0.575	11.53	33.9	0.2
22	32.85	12.89	-	32.85	0.211	0.012	0.509	9.11	33.5	0.2
23	32.85	5.6	-	32.85	0.212	0.012	0.516	3.94	33.6	0.1
24	32.85	9.95	-	32.85	0.212	0.012	0.532	6.54	33.9	0.2

25	32.85	3.61	-	32.85	0.216	0.012	0.522	3.11	34.3	0.1
26	32.85	5.9	-	32.85	0.22	0.013	0.5	6.01	34.7	0.2
27	32.85	3.52	-	32.85	0.225	0.013	0.482	5.89	35.1	0.2
28	32.85	2.83	-	32.85	0.232	0.013	0.497	7.26	36.5	0.2
29	32.85	0.7	-	32.85	0.251	0.014	0.519	3.86	40.0	0.1
30	32.85	0.61	-	32.85	0.266	0.015	0.612	7.27	44.0	0.2
31	30.09	-	2.76	32.85	0.23	0.014	0.341	9.28	32.7	0.3
32	2.28	-	30.57	32.85	0.201	0.012	0.355	-	28.9	0
33	-	-	32.85	32.85	0.199	0.012	0.33	-	28.1	
34	-	-	32.85	32.85	0.199	0.012	0.33	-	28.1	
35	-	-	32.85	32.85	0.199	0.012	0.33	-	28.1	
36	-	-	32.85	32.85	0.199	0.012	0.33	-	28.1	
37	-	-	28.89	28.89	0.199	0.012	0.33	-	24.7	
38	-	-	-	-	-	-	-	-		
Total	880.85	241.12	241.12	1,121.98	0.221	0.013	0.601	207.88	1229.0	0.2

Note: Includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.

Table 16.10: Strip Ratio – Actual & Effective by Grouped Periods

Mining Strip Ratio	Ave LOM (t:t)	Max (t:t)	Years 1-5 (t:t)	Years 6-15 (t:t)	Years 16-21 (t:t)	Years 22-31 (t:t)	Years 32-38 (t:t)
Actual (waste/mineralisation)	0.19	0.7	0.10	0.14	0.33	0.17	0.00
Effective (waste+stockpile/feed)	0.40	1.1	0.50	0.48	0.74	0.30	0.00

16.6 Mine Equipment

16.6.1 Mobile Fleet

The mine fleet consists of the mobile equipment operating from the pit to the crusher berm, and to the waste dump. Crushing and conveying equipment have been included under the process plant section of the PEA.

Table 16.11 summarises the major equipment fleet, the number of units required at start-up, and the maximum fleet size during the life of mine.

Table 16.11: Major Mine Equipment Fleets

Major Mine Equipment	Purpose	Size	Units on Site	
			Years 1-2	Max.
Blast-hole Electric Drill	Primary drill	311 mm	2	5
Surface Crawler Percussion Drill	Pioneering/wall control	155 mm	1	1
Cable Shovel	Production loading	27 m ³	2	3
Wheel Loader	Backup loader & stockpile handling	21 m ³	1	1
Haul Trucks	Production haulage	221 t	5	22
Track Dozer (D10 Equivalent)	Road development & maintenance	425 kW	2	3
Track Dozer (D9 Equivalent)	Pit maintenance	302 kW	1	1
RT Wheel Dozer	Shovel support	597 kW	1	2
Grader (24' Blade)	Road maintenance	518 kW	1	2
Grader (16' Blade)	Road maintenance	216 kW	1	1
Water/Sanding Truck	Road maintenance	20,000 L	1	2

The size and production rate of the mine will accommodate large mobile equipment and will lead to lower unit mining costs. The primary load and haul equipment fleet will consist of 27 m³ electric rope shovels and 220 t trucks. The shovel size was selected to meet the annual mineralisation and waste production requirements from the pits. Each unit has the capacity to produce an average of 22 Mt/a. It is estimated that a maximum of three shovels will be required during the

life of mine. Electric rope shovels were chosen over hydraulic excavators due to their lower operating costs, long life and on the assumption that grid power will be provided to site. A production class front-end loader (21 m³) has been included in the fleet as a backup, construction, and ROM stockpile digging unit.

The size of the trucks has been selected to match the shovel output for four-pass loading. The size of the fleet is determined by estimating the haulage productivities for mineralisation and waste. Preliminary estimates on the haulage productivities indicate that 5 units will be required by Year 2, increasing to a maximum of 22 units by Year 15. The drill fleet will consist of three 311 mm diameter electric blast-hole drills for production drilling. One 155 mm diameter diesel track drill will be required for pioneering and potentially pre-shearing.

Pit support equipment will include rubber-tire dozers for pit floor maintenance near the shovel faces, track dozers, and backhoes for road development, maintenance, and ditching. The road maintenance fleet will also include motor graders and water/sanding trucks.

Ancillary mine equipment will include light-duty vehicles, service trucks, cranes, utility backhoes, blast-hole stemmers, lighting plants, and other equipment required to support the mine and maintenance areas of the operation.

16.6.2 Mine Buildings

On-site mine service buildings will include a heavy-duty truck shop, mine dry, light-duty vehicle shop, wash bay, warehouse, fuel depot and distribution, assay laboratory facility, process control room, and administration building,

Blasting explosives will be manufactured on site, and the explosives plant will be housed in a secure structure. The plant and storage facilities will be located a minimum distance away from the central plant site and pit, in compliance with regulatory requirements.

Further description of the respective mine support infrastructure is included in Section 18.0.

16.7 Waste Disposal & LG Stockpile Management Facility

Mine waste rock and long-term stockpile material will be hauled from the Horsetrail pit and placed on a waste and stockpile facility located southwest of the pit. The preliminary waste dump and LG stockpile design is constrained by Turnagain River, Hard Creek, and planned site infrastructure (Figure 16-2). Rock chemistry data indicate the waste rock to be non-potentially acid generating. The majority of the rock is assumed to be competent and able to be end-dumped on high lift intervals. The foundation under the waste dump has not been analysed for stability. It is necessary to confirm the geotechnical viability of the dumpsite and material geochemistry for the next level of study particularly with the proximity of Turnagain and Hard Creek rivers.

The end-of-mine waste dump will be approximately 45% of the volume shown in Figure 16-2 once all LG has been reclaimed. Previous studies had scheduled waste rock to be hauled and placed

as buttress material for the TMF main embankment located 4 km upstream from the mouth of Flat Creek in the Flat Creek Valley. Further analysis and trade-off studies are required to determine the viability of such a scenario; although if confirmed, the mine waste dump complex at the end of mine life might reduce to 50 Mt of waste or a reduction of 40% volume, as shown in Figure 18-2.

Overburden and soil will be stockpiled in separate piles accessible for ongoing or end-of-mine reclamation activities.

A ROM crusher stockpile will be located in close proximity to the primary crusher providing temporary storage for material not fed to the crusher directly (for various operational reasons).

17.0 RECOVERY METHODS

17.1 Introduction

The processing plant proposed for the Turnagain project was designed to overcome the challenges imposed by its highly competent nickel mineralization. To address these challenges, appropriate comminution equipment selection is vital to the overall economics of this project by ensuring proper size reduction and recovery of nickel-bearing minerals. Building from the previous 2011 AMC PEA and Hatch's previous 2018 conceptual study, the mineral processing plant was designed to treat 90,000 t/d of ROM mineralized material and consists of a crush-grind-flotation flowsheet.

Previous studies performed by Hatch for the design of the Turnagain concentrator considered the use of a semi-autogenous grinding (SAG) mill as the principal method of coarse grinding. This study considers the use of a high-pressure grinding roll (HPGR) as a tertiary crushing circuit and the use of two ball mill circuits in series for grinding in order to reach the particle sizes required for flotation.

HPGR technology has been selected primarily due to higher energy efficiency compared to SAG milling. In recent years, HPGR technology has seen wider acceptance and use in operations, specifically the application of large, high throughput HPGR systems. Recent operations, such as Freeport-McMoRan's Metcalf concentrator, have seen successful implementation of large HPGR systems as the principal comminution equipment.

One key consideration in the design of the processing plant is the phased concentrator construction approach, whereby the concentrator starts up at 50% capacity before expanding to full capacity (i.e., 45,000 t/d for the first five years, and 90,000 t/d thereafter). The implications of this are discussed briefly in Section 17.4.

17.2 Process Design Criteria

The process design criteria detail mineral processing design considerations for the Turnagain concentrator including annual mineralized material and product capabilities, plant availability, and capacities. Table 17.1 provides a summary of key design criteria.

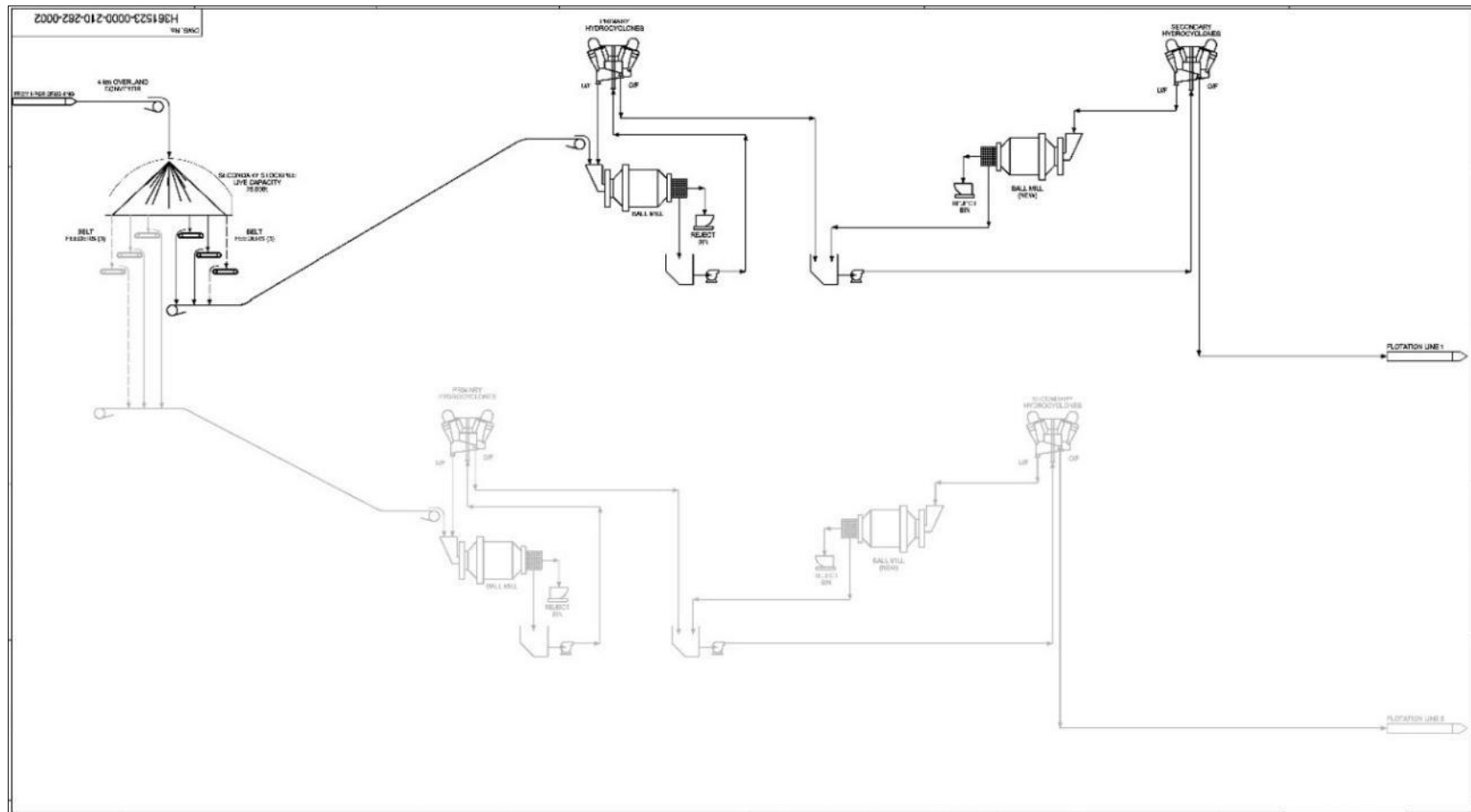
17.3 Process Description

The process flowsheets for the proposed plant are shown in Figure 7-1, Figure 7-2, and Figure 7-3.

Table 17.1: Key Process Design Criteria

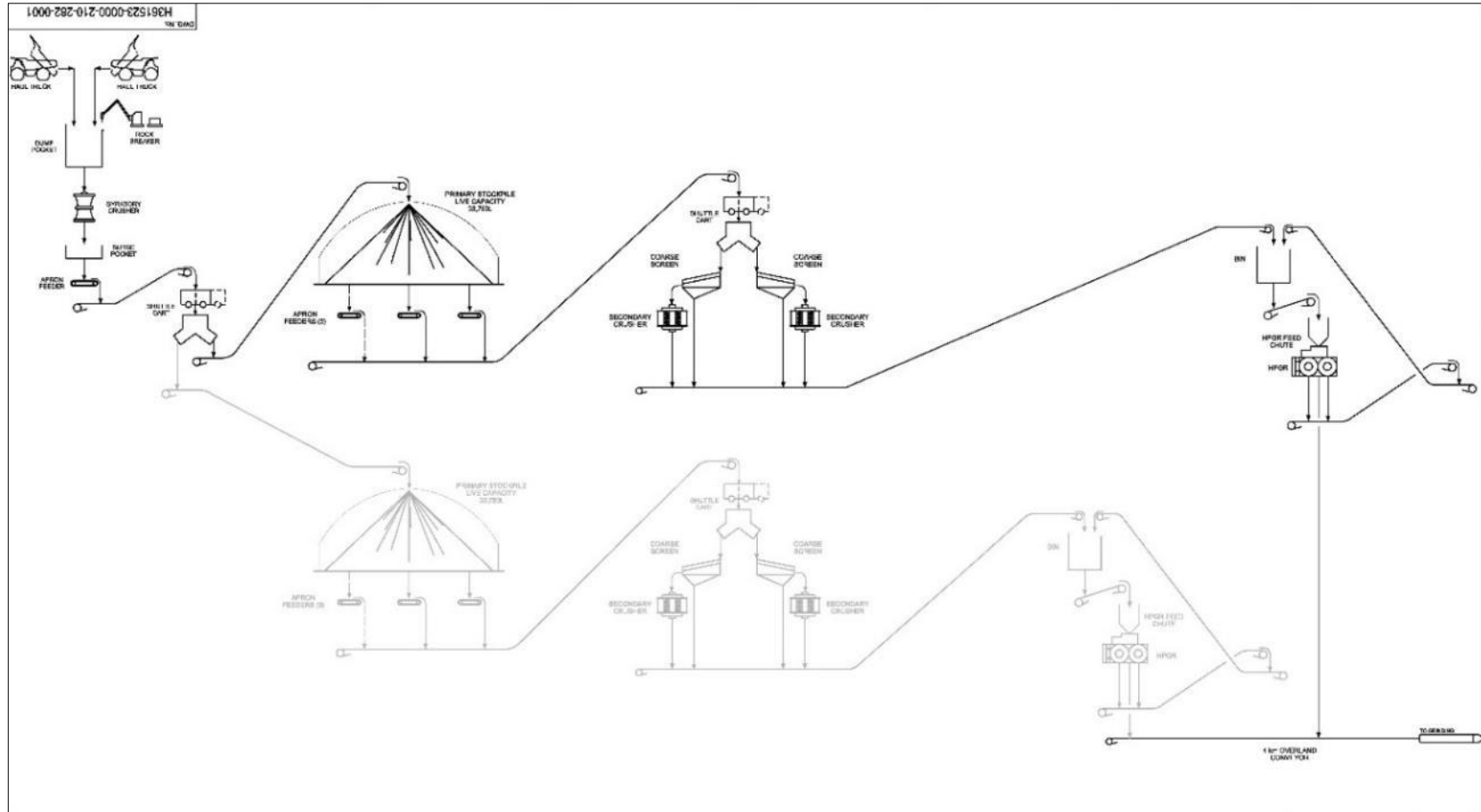
Area	Criteria	Unit	Nominal Value
General	Primary Crushing Availability	%	70
	Secondary Crushing Availability	%	88
	HPGR Circuit Availability	%	88
	Concentrator Availability	%	94
	Nickel Head Grade		
	45 kt/d (Year 2-5 Average)	%	0.261
	90 kt/d (Year 6-10 Average)	%	0.232
	Sulphur Head Grade		
	45 kt/d (Year 2-5 Average)	%	1.16
	90 kt/d (Year 6-10 Average)	%	0.69
	Average Nickel Recovery		
	45 kt/d (Year 2-5 Average)	%	57.9
	90 kt/d (Year 6-10 Average)	%	51.6
	Average Annual Concentrate Production (18% Ni)		
	45 kt/d (Year 2-5 Average, 9% moisture)	t/a	151,814
	90 kt/d (Year 6-10 Average, 9% moisture)	t/a	237,902
	Average Annual Nickel Production		
	45 kt/d (Year 2-5 Average)	t/a	24,867
	90 kt/d (Year 6-10 Average)	t/a	38,968
Crushing	Crusher Work Index	kWh/t	18.2
	ROM Mineralized Material Top size	mm	1000
	Crusher + HPGR Circuit Product size (P ₈₀)	mm	4.0
	Primary Stockpile Capacity (live)	hr	18
	Secondary Stockpile Capacity (live)	hr	13.3
Grinding	Bond Ball Mill Work Index	kWh/t	19.8
	Grinding Circuit Product size (P ₈₀)	µm	80 to 85
Flotation	Rougher Flotation Design Retention Time	min	67
	1 st Cleaner Design Retention Time	min	27
	1 st Cleaner Scavenger Design Retention Time	min	16
	2 nd Cleaner Design Retention Time	min	32
	3 rd Cleaner Design Retention Time	min	35
Concentrate Thickening & Filtration	Thickener Solids Loading	t/h/m ²	0.25
	Thickener Underflow Density	Wt%	55
	Filter Cake Moisture	Wt%	9

Figure 17-1: Process Flow Diagram – Crushing Circuit



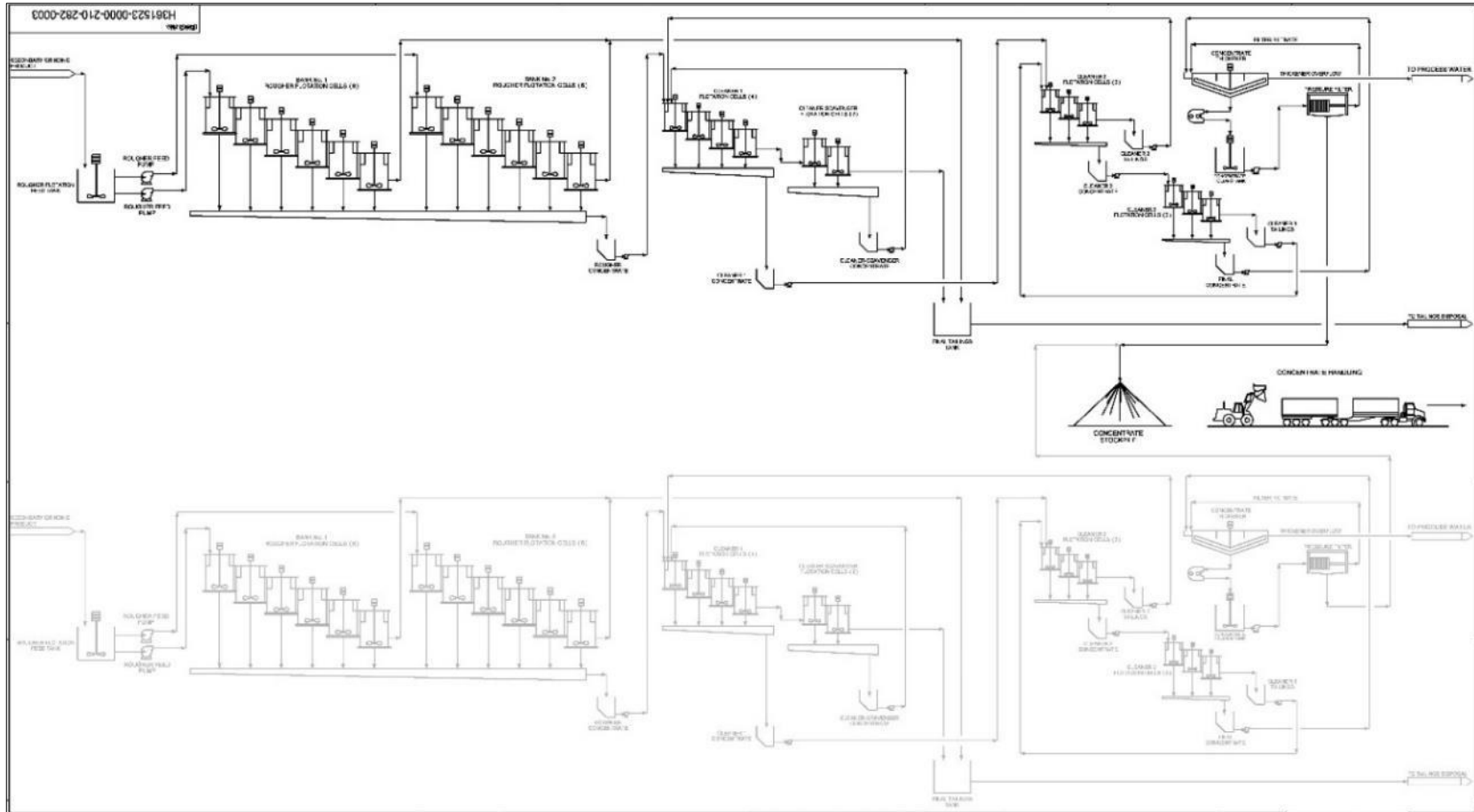
Source: Hatch, 2020.

Figure 17-2: Process Flow Diagram – Grinding Circuit



Source: Hatch, 2020.

Figure 17-3: Process Flow Diagram – Flotation Circuit



Source: Hatch, 2020.

The process plant, when running at full capacity (90,000 t/d), will consist of the following major unit operations:

- ROM crusher feed hopper
- one primary crusher and two crushed ore stockpiles including:
 - conveyors
 - ore reclaiming systems
- two parallel secondary crushing circuits, with each circuit consisting of:
 - two 3.0 x 7.3 m double-deck coarse screens in parallel
 - two cone crushers in parallel, each with 933 kW motors
- two parallel tertiary crushing HPGR circuits, with each circuit consisting of:
 - 2.6 m diameter x 2.4 m wide HPGR with 9,000 kW of installed power
 - one HPGR edge recycle conveying system
- two parallel primary ball mill grinding circuits, with each circuit consisting of:
 - 7.9 m diameter x 13.7 m long (26 x 45 ft) ball mill with 18,000 kW of installed power
 - one 14-place cluster of 0.84 m diameter cyclones
- two parallel secondary ball mill grinding circuits, with each circuit consisting of:
 - 7.9 m diameter x 13.7 m long (26 x 45 ft) ball mill with 18,000 kW of installed power
 - one 10-place cluster of 0.66 m diameter cyclones
- four parallel trains of rougher flotation, each with 6 x 630 m³ tank cells
- two parallel trains of cleaner flotation in three stages
- concentrate thickening and filtration
- tailings facility reclaim water system (part of the TMF) for process water
- fresh water will be used for pump gland seals, reagent mixing and other special requirements (e.g., hydraulic unit cooling).

All buildings and conveyors are enclosed with proper dust suppression and collection systems to address exposure to any silicates or fibrous materials.

ROM plant feed will be delivered to a dump pocket by haul trucks on top of the gyratory crusher. Crushed material from the gyratory crusher will be reclaimed by an apron feeder and conveyed to the primary stockpile.

Ore from the primary stockpile will be reclaimed using apron feeders and transported to the secondary crushing splitter chute via conveyor belt. A self-cleaning permanent magnet will be

installed along the conveyor belt to remove unwanted tramp metals from the bulk materials ahead of the secondary crushing circuit. The two secondary cone crushers are operated in an open circuit with fines scalping and parallel configuration. There is a double-deck, multi-slope, vibrating screen installed ahead of each of the secondary cone crushers with the crusher fed directly from the screen oversize. Conveyors will have variable speed drives to facilitate the crusher choke feed requirement. Subsequently, the crushed product will join the screen undersize onto a conveyor belt before being transported to the HPGR feed bin. The edge material from the HPGR discharge will be recycled back to the HPGR feed, while the HPGR product (centre) will proceed to the secondary stockpile at the concentrator plant via a 4 km overland conveyor.

Each grinding circuit consists of two closed-circuit (with hydrocyclones) ball mills operated in series for primary and secondary grinding. The primary ball mill will be operated in a “direct” closed-circuit configuration with a cyclone cluster; the primary ball mill will receive feed from the secondary stockpile reclaim. The primary ball mill discharge will pass through a trommel for ball scats removal and into the pump box prior to entering the primary cyclone cluster for size classification. Primary cyclone underflow will feed back to the primary ball mill. Primary cyclone overflow will flow by gravity to a pump box and be pumped to the secondary cyclone cluster. Secondary cyclone underflow will flow to the feed of the secondary ball mill. The secondary ball mill will be operated in an “indirect” configuration, as the secondary ball mill feed must first pass through the secondary cyclone cluster to scalp final-grind material to the overflow stream. The secondary ball mill product will pass through a trommel before entering back to the pump box ahead of the secondary cyclone cluster. Secondary cyclone cluster overflow will report to the rougher feed conditioning tank prior to being pumped to the rougher flotation circuit.

A conventional sequential flotation flowsheet consisting of a rougher, cleaner and cleaner scavenger will be used to produce the final Ni concentrate. Re-grinding is not currently included. Limited testwork has shown a potential increase in recovery, and ongoing testwork is intended to determine the magnitude of any such improvement. This will enable trade-off studies to be completed on possibly adding re-grinding to the flowsheet at a later stage. The concentrate cleaning has been designed with three stages in the plant, using conventional mechanical flotation cells.

The concentrate products will be dewatered in high-rate thickeners with the underflow feeding filter feed stock tanks. The pressure filter will dewater the Ni concentrate to a moisture content of 9%. The Ni concentrate will then be discharged directly from the pressure filter to the concentrate shed for truck load-out. The rougher tailings and cleaner scavenger tailings will flow by gravity to the TMF for deposition. Reagents consumed within the flotation circuits are prepared within the reagent handling and make-up area. This facility includes mixing and storage for MIBC as frother, SIPX as collector, Calgon as depressant, and flocculant.

17.4 Phased Expansion

The mineral processing plant is designed for two grinding trains, four rougher flotation trains, and two cleaner and cleaner scavenger trains at full capacity. This configuration allows for phased construction of the mill. The first phase at 50% of the full capacity will simply comprise one

crushing train, one grinding train, two rougher flotation trains, and one cleaner and cleaner-scavenger train. For the first five years, the plant throughput will average 16.4 Mt/a. Thereafter, for Years 6 to 35, the average throughput will be 32.9 Mt/a.

The primary crushing circuit is designed to operate during both phases, as it is larger than required for the first phase throughput. This design introduces the opportunity for optimising the operating schedule of the primary crusher during the first phase (to save on power and maintenance costs) which can be explored in future studies. The overland conveyor and secondary stockpile have also been designed to operate during both phases of plant operation.

This phased approach will provide site experience for the construction and ramp-up of the proposed concentrator design, allowing for optimisation of construction and ramp-up for the second phase expansion. There is potential to improve the economics of this project by altering this phasing plan, either by constructing at full scale immediately or by decreasing the time between construction of the two concentrator phases, in order to increase production rates as quickly as possible.

Other opportunities for improvements and alternatives to the Turnagain concentrator design are presented in Section 25.8.

18.0 PROJECT INFRASTRUCTURE

18.1 Site Access Road

The communities of Terrace and Smithers in BC, and Whitehorse in the Yukon, are all several hundred kilometres away and offer the best range of supplies and services. Supplies can be trucked via the Stewart-Cassiar Highway (Highway 37) to 8 km south of Dease Lake, a small community in northwest BC, approximately 250 km south of the Yukon border. The Turnagain property can be accessed by a trail extending east from Highway 37. The trail has been used by large, articulated four-wheel drive vehicles to access the Kutcho Creek area local jade extraction, Eaglehead gold-copper exploration, and to supply gold operations at Wheaton Creek. A branch of this trail network extends into the Turnagain property.

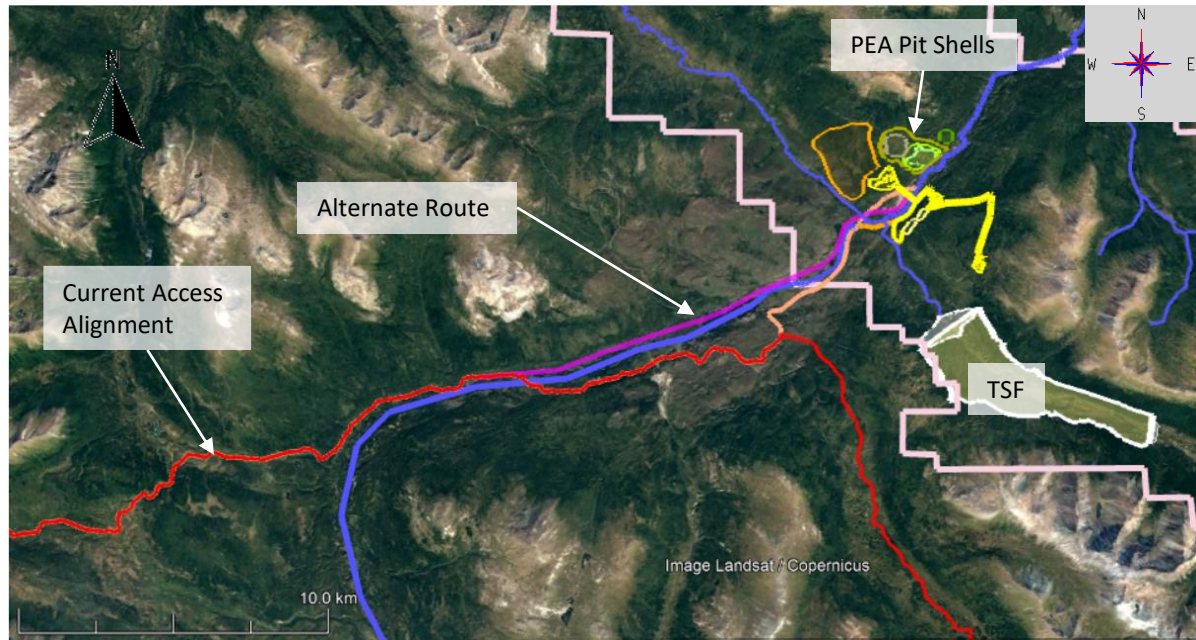
The road distance to the site from Highway 37 is approximately 78 km. The access trail from Highway 37 to the property will require upgrading. There are two major stream crossings and approximately 50 other minor crossings en route to the site. These crossings are currently passable with light vehicles, but will need upgrading for larger trucks. Bridges are required for the major crossings; culverts will likely be required for the minor crossings.

For safe travel with the anticipated volume of traffic, especially considering the potential for multiple uses of the road, an 8 m wide all-weather road built to BC Forestry standards to allow two-way traffic is envisioned. The existing access road would be widened and upgraded.

As shown on Figure 18-1, there is the possibility of an alternate route on the north side of the Turnagain River (instead of following the trail currently on the south side) for the last 16 km to the site to reduce the number of Turnagain River crossings (bridges) and reduce cost. This will be further considered in the next study stage of the project.

The progress of the Kutcho project and road user discussion group outcomes will also be considered. There may be an opportunity to share the cost of upgrading 54 km of this road with Kutcho Copper Corporation. With the current trail and road route, two river crossings will require bridges: one on the main access road and the other to the open pit side of the river. To be able to efficiently access all areas of the planned site, a network of internal roads will also be required. These roads will access the open pit mine, waste dumps, tailings storage facility, crusher building, plant site, and all permanent and service facilities that would support the mine.

Figure 18-1: Potential Access Road along North Side of Turnagain River



Source: Giga Metals, 2020.

18.2 Waste Management Facility Alternatives

In April 2006, KP completed a preliminary waste management facility alternatives study (Ref. No. VA06-00593), which identified a number of potential TMF sites in the vicinity of the Turnagain deposit (e.g., Flat Creek Valley was acknowledged as a potential option for a tailings impoundment). In July 2007, a preliminary mine development alternatives assessment was carried out (Ref. No. VA07-01017) to explore several mine development alternatives, including the location of the plant site, waste dumps, low-grade stockpile, haul and construction access roads, and tailings and water reclaim pipelines. This assessment of alternatives should be updated during the next phase of study.

In 2019, further site configuration and trade-off analysis was performed by Hatch (Siting Location Trade-off Study, H355439-00000-210-230-0001). Primary objectives of the study included the following:

- placement of the plant site within the same catchment as the TMF
- minimise footprint with regards to civil/earthworks
- incorporate dust considerations in site selection
- consider plant expandability
- minimise power consumption demands

Based on the study results, the plant site was relocated upslope to the north of the TMF main abutment to facilitate gravity tails flow, and the HPGR crushing facility was placed with the primary

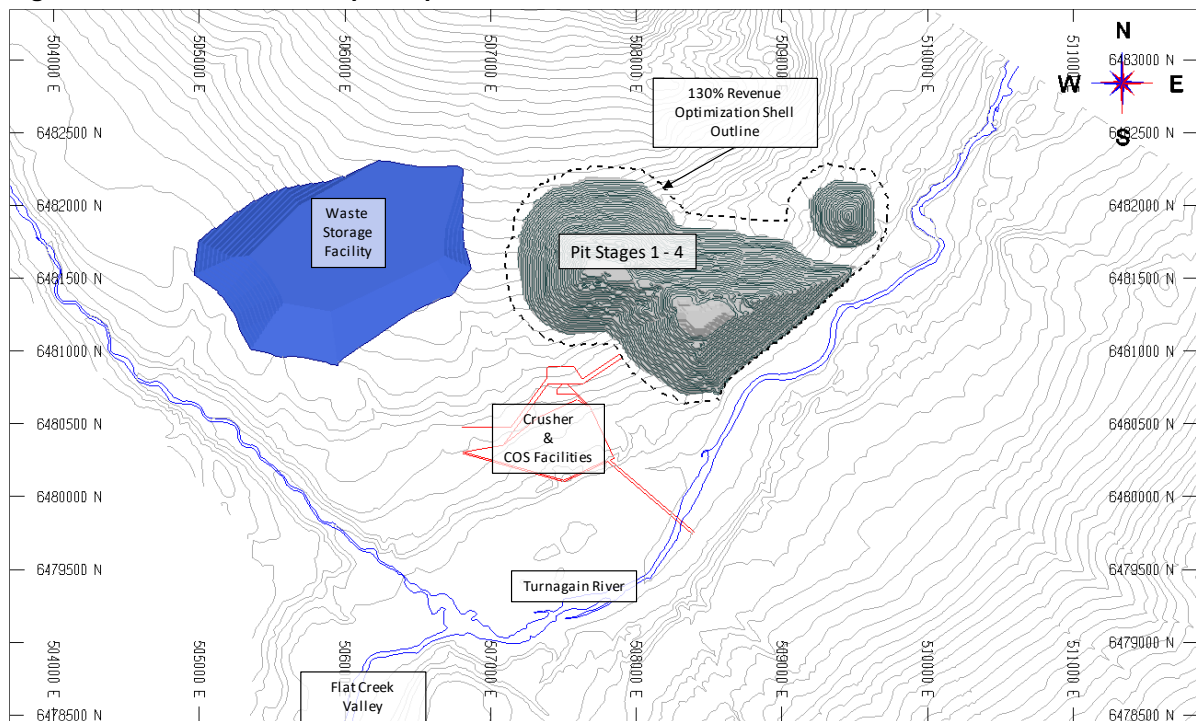
crusher system in the valley near the open pit operations. The HPGR product will be conveyed across the Turnagain River and upslope to the processing plant. Conveying instead of high-pressure slurry pumping across the Turnagain River reduces the risk of significant spills as well as power demand.

18.3 Waste Rock Management Facility

18.3.1 Non-Reactive Waste Rock

Non-reactive waste rock will be stored in a conventional sub-aerial (surface) dump or within the mined-out open pit later in the mine life. The approximate final waste dump footprint is shown on Figure 18-2. The waste dump is sized for the entirety of the expected waste rock; possible use of waste rock for TMF construction will reduce the required size of the waste dump. The potential re-use of waste rock will be investigated further (geotechnical, geochemical, economic) in the next stage of engineering.

Figure 18-2: Final Waste Dump Footprint



Source: Hatch, 2020.

18.3.2 Potentially Reactive Waste Rock

Potentially reactive waste rock will be stored in the surface waste dump and within the mined-out open pits using best management practices. The waste rock is generally not expected to exhibit acid generating properties but may be neutral metal leaching.

The waste rock characterisation to date is largely inconclusive on the acid generating potential of the waste rock, since most of the testwork was carried out on mineralised material. Although a small percentage of the waste may have acid generating potential, it is expected to be insignificant with respect to the overall neutralising potential of the waste rock pile. It is assumed that any potentially acid generating (PAG) material encapsulated in the dump would be surrounded by a sufficient quantity of rock with high neutralising potential. It is therefore highly unlikely that acid rock drainage would emanate from the dump, both during operations and post-closure. The risk posed by PAG waste for the project is accordingly low (AMC, 2011).

Additional characterisation work is under way but was not available for this study. This work will be incorporated in the next phase of study.

If necessary, a treatment process will be incorporated into the water management plan early in the mine life, to allow for treatment of any effluent from the waste dumps that may be affected by neutral metal leaching. The plant will produce a metal oxide precipitate with total metal content too low for effective recovery and therefore will be added to the plant tailings for pumping to the tailings management facility.

18.4 Tailings Management Facility

18.4.1 Design Basis & Operating Criteria

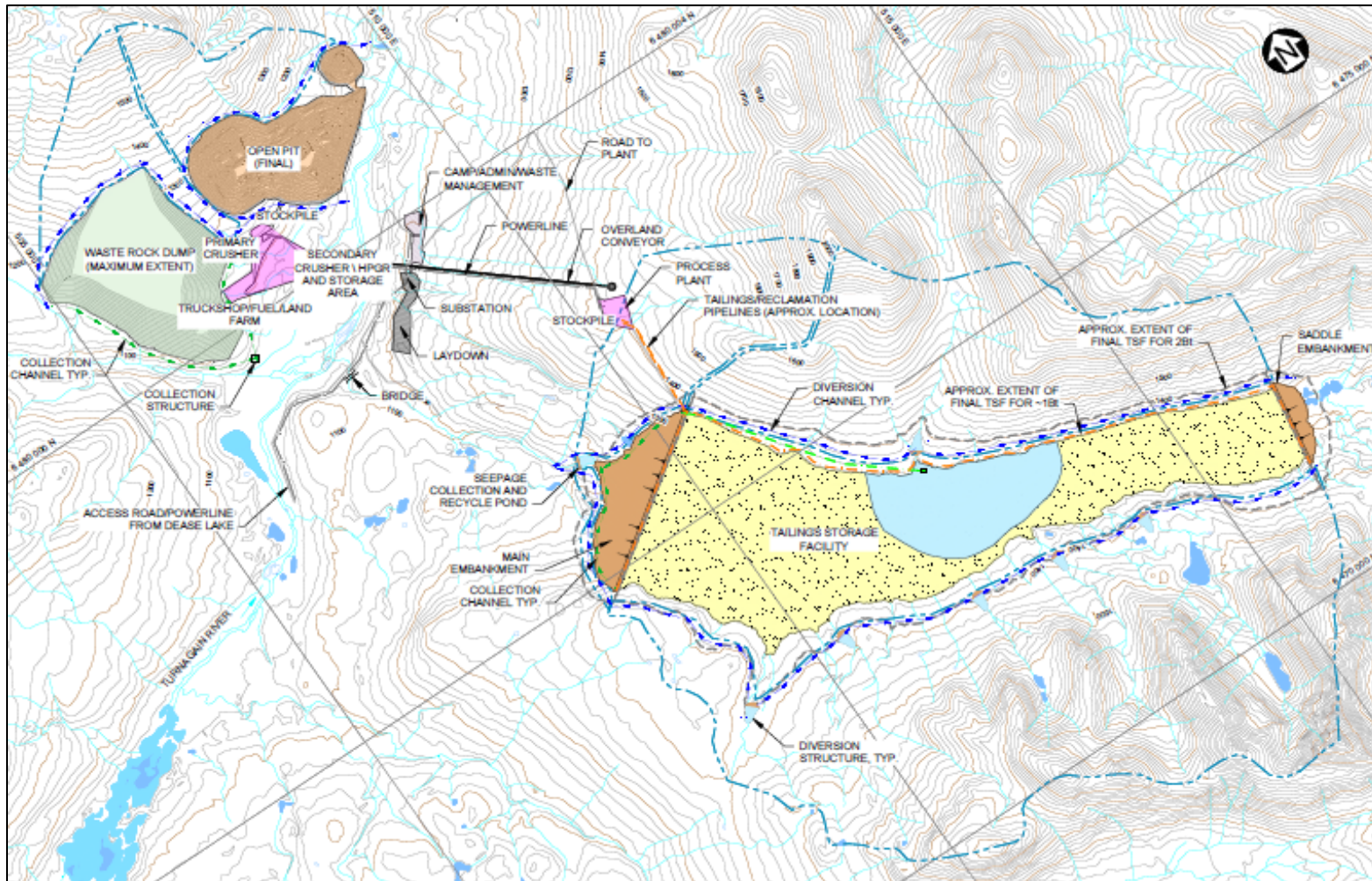
The principal objective of the design and operation of the TMF is to ensure secure containment for tailings solids and impounded process water. The TMF will serve as the primary water management facility for the project, providing a buffering volume for the mill process water demands, as well as collecting and storing the necessary quantities of precipitation and runoff for start-up and operations. The proposed TMF is located in Flat Creek Valley, as shown on Figure 18-3.

The mill throughput will be approximately 45,000 t/d for the first five years of operation and approximately 90,000 t/d starting in Year 6. The total tailings production is assumed to be approximately 1,122 Mt over 37 years of operation. Tailings from the mill will be discharged to the TMF as a slurry at an average un-thickened solids content of approximately 25% (by weight).

The TMF starter embankment is sized to provide water storage for start-up and to store the estimated volume of tailings produced during the first three years of operation.

The final facility is sized to store the estimated 1,122 Mt of tailings produced over the planned mine life. The facility makes use of the favourable topography to yield a relatively large storage volume, compared with the quantity of material required for embankment construction. Likewise, significant increases in storage capacity can be realised with moderate increases in the elevation of the confining embankments. The TMF storage capacity could be substantially expanded within the proposed location. A 2 Bt capacity scenario has been conceptually fit with the basic configuration shown on Figure 18-3.

Figure 18-3: TMF General Arrangement



Source: KP, 2020.

The presence of minerals in the tailings that can react with CO₂ is expected to provide a range of benefits to the project, as noted in Section 20.6. The potential presence of minor amounts of fibrous mineral forms of magnesium silicate in the tailings may require dust management on exposed beach areas through seasonal irrigation, additives, or other means. Although not part of the current design, the reaction with CO₂ tends to create hardened surfaces that reduce dust generation and create a stronger tailings material that is more resistant to low-stress flow. This will be further investigated in future studies.

18.4.2 Layout & Operating Strategy

18.4.2.1 Tailings Management Facility Embankments

The main TMF embankment will be raised in stages, with each stage providing the required capacity for that particular period until the next stage is completed, while always maintaining minimum storm water storage, wave run-up, and freeboard requirements. The staged design of the embankments will be reviewed and updated annually to accommodate the actual mine production, availability of construction materials, and to incorporate experience gained with local conditions and constraints.

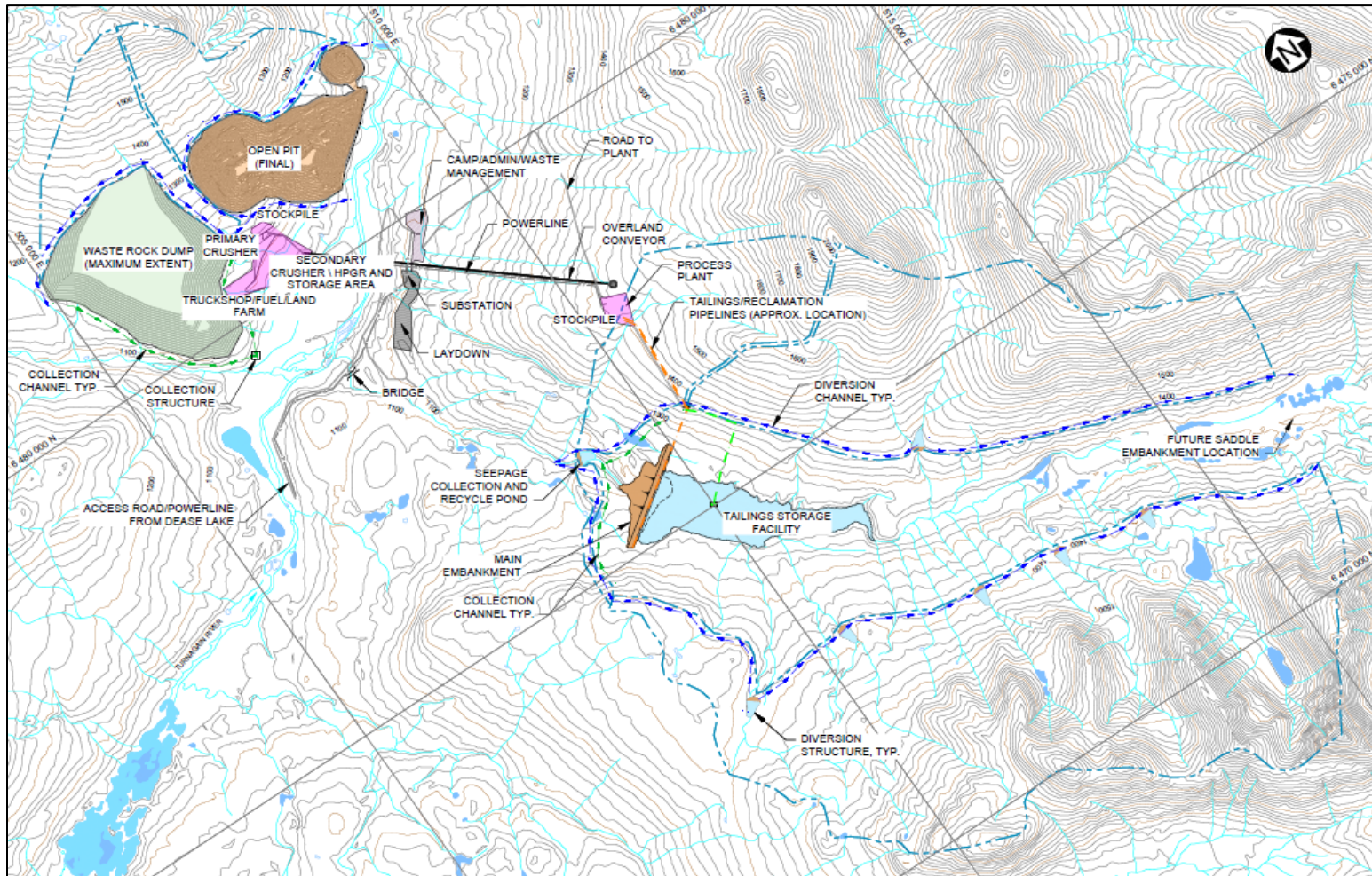
A small, temporary cofferdam will be initially constructed on Flat Creek upstream of the main TMF embankment footprint. This dam will allow the TMF starter embankment foundation area to be dewatered, cleared, and stripped in preparation for construction.

A drainage network of interceptor pipes placed in a dendritic or herringbone pattern will underlie each dam foundation. The drains will be surrounded by appropriate filter and drainage materials. The individual interceptor drains will connect to larger main collector pipes to transport embankment drainage and intercepted seepage to recycle ponds located at the topographic low points below each embankment. The underdrain network will be expanded as the staged embankments are constructed. They will also provide foundation dewatering during initial construction.

The TMF embankment construction will begin with a starter dam located at the northwest end of Flat Creek Valley, as shown on Figure 18-4. The starter embankment will be built as a water-retaining structure with 2H:1V upstream and 3.5H:1V downstream slopes.

The starter dam will be constructed in two phases (Stage 1a and Stage 1b) that are scheduled to provide storage for the first three years of operation. Stage 1a will be completed in Years -2 and -1, before mill start-up, and Stage 1b will be built as a downstream raise before the beginning of Year 2. A low permeability synthetic liner system will be placed on the upstream face of the starter dam to provide a continuous hydraulic cut-off. The liner will tie into a concrete plinth or slurry trench along the upstream toe of the starter dam. Blanket and curtain grouting may be employed up to the final elevation of the starter dam as required to ensure continuity of the hydraulic cut-off.

Figure 18-4: TMF Starter Embankment



Source: KP, 2020.

The initial embankment will be built using a combination of local borrow material and material from the mill site excavation. Suitable material will be placed and compacted to achieve the required permeability and satisfy embankment stability criteria. The embankment will impound an initial fresh water pond prior to start-up of processing operations.

The centreline method of embankment construction will be used for ongoing raises of both the northwest main embankment and the southeast saddle embankment. Each stage will have a minimum horizontal width of approximately 60 m to allow placement with large haul trucks. Rock will be dumped, spread, and compacted to the specified density. Both embankments will have a minimum final crest width of 30 m to allow for vehicle access and pipelines. The embankments will be designed as free-draining structures above the starter dam to enhance stability by promoting well-drained conditions in the dam fill material and the tailings beach upstream of the embankment. Large tailings beaches will be developed and the supernatant pond will be kept small and remote from the embankments during operations.

Appropriate filter zones will be raised with each stage of the dams to separate the tailings beach from the coarser rockfill in the downstream embankment shell. It is envisaged that these will be constructed in the summer months by a specialised contractor using locally sourced borrow material. Ongoing construction of the main northwest dam shell zone will make use of suitable low-sulphur, geochemically innocuous rock from a quarry within the TMF catchment area that will be progressively inundated by the stored tailings. The shell zones will need to be constructed prior to beginning work on the crest and filter zones to allow access for equipment. The final general arrangement at the end of the mine life is shown on Figure 18-2.

A smaller saddle embankment will be constructed at the southeast end of the TMF. It will be built using local borrow material in the same manner as the main embankment. The first stage of the saddle dam will need to be completed by about Year 15 of mine operations. The saddle dam will be constructed using the same centreline method as the main dam and will comprise similar fill zones. All materials used in construction of the saddle dam will be sourced from local borrow. Borrow material will be taken from within the TMF impoundment area or diversion channel excavations where possible to minimise the total project footprint. Borrow areas may also be developed in the hill slopes immediately above the TMF.

Seasonal construction restrictions for the various fill materials and zones should be considered. The coarse, free-draining rockfill that makes up the majority of the embankment volume can be placed year-round and in most climatic conditions. The finer-grained but free-draining filter zones should only be placed when temperatures are above freezing. Ice crystals in sandy materials are difficult to detect, even with manual-visual techniques, and must not be included in the embankment fill. It is anticipated that the proposed project schedule will provide sufficient time to place the required volume of material estimated for the current TMF design.

18.4.2.2 Mill Tailings Transport & Deposition System

The tailings transport system will be constructed in stages throughout the life of the project. Tailings will initially flow by gravity from the mill to the TMF main embankment and will be

distributed from off-takes (spigots) located along the embankment crest as shown on Figure 18-2 and Figure 18-3. Tailings will also be deposited along the northern shore of the TMF and the saddle embankment beginning in approximately Year 6. Although not included in the current mine layout, tailings discharge from the southern shore of the TMF would be possible if this is found to be a more practical approach during future studies. Two parallel pipelines will be operated concurrently for each 45,000 t/d mill train. Tailings pipelines will be constructed using HDPE wherever practical.

Gravity flow to the main embankment will be possible for the entire mine life. Tailings pumping may be required to discharge tailings to the saddle embankment after approximately Year 25 when the dam is raised past El. 1340 m. A booster pump station that can operate on one of the tailings pipelines (22,500 t/d) would be required in Year 25 and has been included in the conceptual design.

Tailings will initially be deposited from a series of valved off-takes along the embankments to develop long, low-angle sloped beaches away from the embankments. Beach development will be managed through rotational deposition to maintain the pond remote from the embankments. This approach has the added benefit of promoting CO₂ sequestration through the presence of freshly deposited tailings in contact with the atmosphere.

The advantages of the proposed layout are:

- Gravity discharge is possible through the entire mine life to the main embankment and most of the north side of the TMF.
- Pipelines are located within the TMF catchment and any leakage would be contained in the impoundment or the main embankment seepage collection pond.
- Pipelines can be drained and flushed by gravity into the TMF.

18.4.2.3 Reclaim Water System

The reclaim water system is illustrated on Figures 18-2 and 18-3.

Supernatant reclaim water will be pumped from the TMF to a head tank at the mill site. Reclaim pumps will be mounted on a floating barge in the TMF supernatant pond and will operate on level control from the head tank. Total pump power for the water reclaim operation will increase in Year 6 when the second mill train comes online, and gradually decrease over the remaining LOM as the TMF is raised. Additional pumps will be added in Year 5 to accommodate the increased throughput at the mill. The water reclaim pipeline will be constructed using a combination of steel and HDPE. Steel will be used for part of the higher pressure section near the barge for the starter layout. The required pumping pressure will be reduced as the supernatant water level in the TMF rises throughout the mine life and extensions to the reclaim pipelines will comprise HDPE.

18.5 Water & Waste Management

18.5.1 Site Water Management

Water management is an important component of the overall design, and the objectives include:

- provide adequate storage and freeboard in the TMF for secure containment of all process water and storm runoff
- intercept and divert clean water to the extent possible
- adequately collect and control of water within the mine affected area
- mitigate environmental impacts to the extent possible
- optimise the storage and use of water over the entire site to satisfy environmental, operational, and economic criteria

18.5.2 TMF Water Management

The TMF supernatant pond serves as the primary component in site water management, providing a buffering volume for process water, direct precipitation, and storm runoff.

A supernatant pond volume of between approximately 10 and 30 Mm³ is assumed to provide sufficient buffering volume to satisfy water requirements and account for seasonal variations. Twenty-five million cubic metres corresponds to approximately three months of reclaimed water required for a full mill production rate of approximately 90,000 t/d. Water runoff will be collected from the TMF catchment runoff during pre-production years to satisfy start-up pond requirements. A more detailed water balance will be completed in the next phase of study.

The diversion channels shown on Figure 18-3 and Figure 18-4 will be required along both banks of the TMF to maintain a neutral water balance condition in the facility. The water will be diverted to and released downstream of the TMF directly to Flat Creek to minimise impacts to the natural downstream flow regime. Seepage through the TMF dams will be intercepted and collected by the embankment underdrain and seepage collection systems to the extent practical.

The minimum freeboard requirement for the TMF is assumed to be 5 m. Further studies, including determining the inflow design flood and potential seismic deformations from the maximum design earthquake, will be needed to define the required freeboard throughout the life of the facility.

18.5.3 Waste Dump, Low-Grade Stockpile, Open Pit & Plant Site Water Management

Collection and control of the surface and groundwater at all mine facilities is an important part of the overall water management plan. The water collected at the waste dump, low-grade mineralisation stockpiles, open pits, and plant site represents a significant portion of the overall site water balance.

Out-of-pit dewatering wells will be pumped to local collection ponds for water quality monitoring. It is anticipated that the water will be of sufficient quality for discharge directly to the environment.

In-pit water will be pumped to a collection pond. The volume of in-pit dewatering will generally be dependent on direct precipitation and groundwater, and will be sized to contain the 1-in-100-year return period rainfall event that would report to each pit.

Runoff from the waste rock dump and low-grade mineralized material stockpiles will be collected in channels along the downstream toes and diverted into a collection pond located at topographic low points below the facilities.

A gravity-fed pipeline will be available to convey water from the waste dump and low-grade mineralisation stockpile collection ponds to the main pit collection pond. Water collected in the site water management ponds will be pumped to the plant site for reuse, or for treatment and discharge.

Surface water diversion channels will be constructed upstream of the waste dump, low-grade mineralisation stockpiles, and open pit to minimise the quantity of contact water to be managed at the site. The channels will divert runoff away from the mine facilities and back into nearby existing drainages. These channels will be sized to carry the estimated 1-in-10-year peak instantaneous runoff.

18.5.4 Site Water Balance

A water balance was completed to estimate the mean annual surplus or deficit that may be expected at the project site. The water balance model includes the mill, waste dump, open pits, and the TMF, as well as the external contributing catchments for each of the mine components. The conceptual site layout presented in this report, along with available information regarding annual hydrologic conditions were used as the basis for the modelling. Precipitation parameters are considered to represent reasonable site conditions; however, confirmation of these parameters and more detailed water balance calculations will be required in the next stage of the study.

The results of the water balance model suggest that the site could be operated in a water-neutral condition for most of the mine life, given the assumed climatic factors, production schedule, and facilities layout. This is beneficial to the project, as it is unlikely that surface water discharge from the site will be required during operations. It is similarly unlikely that additional make-up water will be required from outside the project area.

It is assumed that the catchment upstream of the final TMF impoundment area will be diverted to Flat Creek downstream of the main dam. These diversions could be deactivated if additional water is needed at the TMF during operations. It is estimated that approximately 20% to 30% of runoff collected by the diversion channels would be sufficient to satisfy make-up water requirements on mean annual basis. This system, combined with good water balance planning during operations, would provide substantial flexibility to maintain a water-neutral condition at the site.

18.5.5 Water Supply

It is assumed that fresh water will be collected from alluvial groundwater wells just north of the plant site near Turnagain River. This would supply the fresh water requirements at the mill as well as other mine facilities. Water will be pumped to a storage tank at the mill. The fresh water demand is currently estimated at approximately 13 m³/h.

18.5.6 Sewage Disposal

A sewage treatment plant is included in the mine infrastructure. Non-process wastewater from some of the site facilities, such as the mine dry and offices, would be treated in this plant.

The sewage treatment plant will be a pre-packaged rotating biological contactor (RBC) system. The plant will be manufactured off site and containerised for simple connection to the collection system on site. The solid and liquid material will be separated in the treatment plant, and the sewage treatment plant effluent will be discharged to the environment in accordance with the requirements of the Environmental Impact Assessment and effluent permits or approvals.

18.5.7 Refuse Disposal

Several forms of domestic and industrial solid waste will be generated over the life of the mine. All avenues of reuse, reduction, and recycling of materials will be examined and implemented prior to any waste disposal.

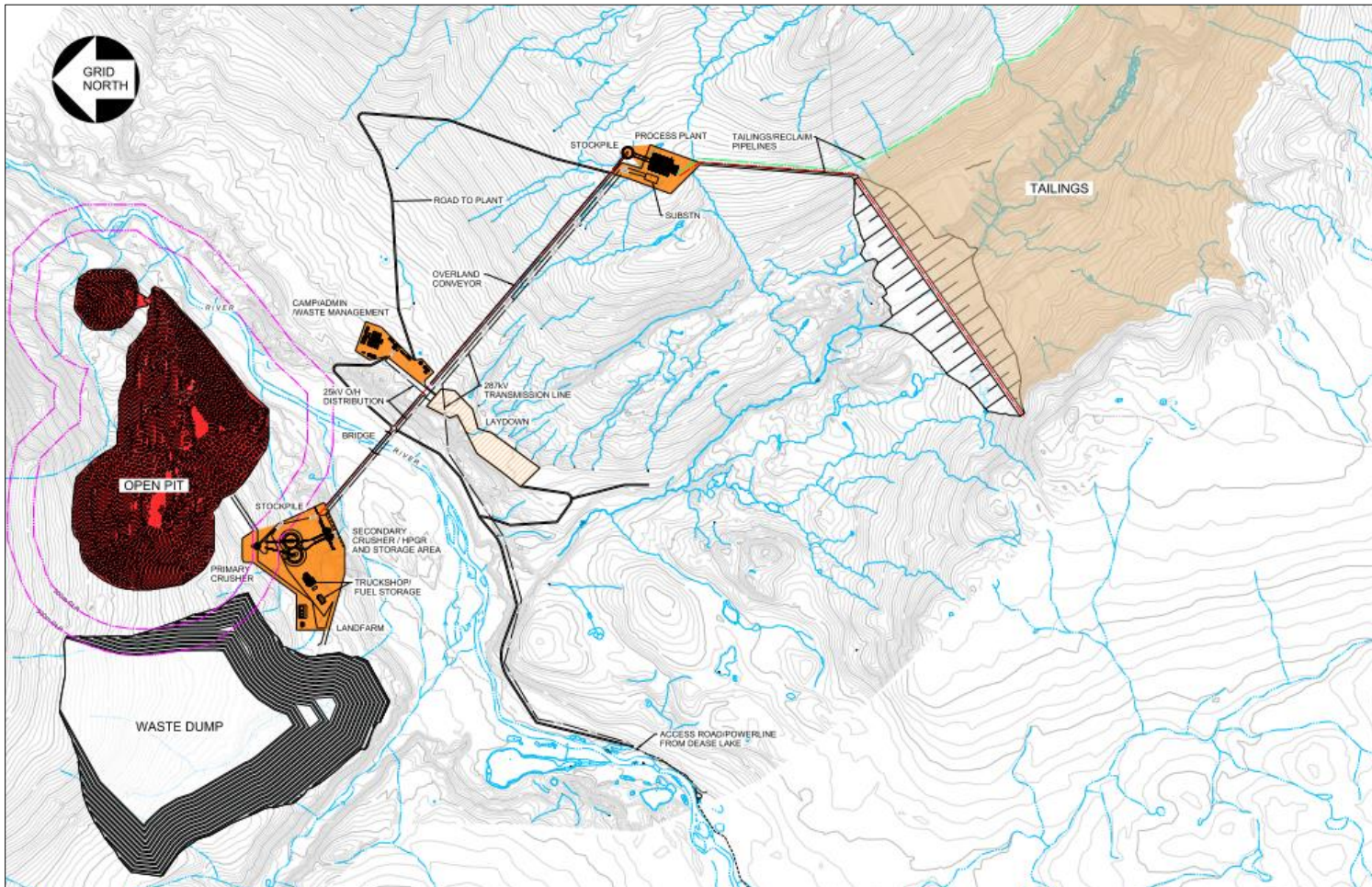
Domestic waste will be incinerated on site, with clean efficient combustion supported by a waste oil-fuelled dual chamber incinerator.

18.6 Plant Site Layout

The plant site layout in Figure 18-5 shows the open pit area, camp infrastructure area, and main concentrator plant.

Site development is divided into these three areas to place facilities in the most efficient location for site operation; mine infrastructure area (including truck shop and fuel storage), camp infrastructure area (including camp, administration buildings, waste management) and process plant infrastructure (main substation, process water and tailings).

Figure 18-5: Plant Site Layout



Source: Hatch, 2020.

18.7 Ancillary Facilities

Project infrastructure and services have been designed to support a 90,000 t/d operation. Infrastructure and ancillary facilities will consist of the following modular, pre-engineered, or stick-built structures:

- administration building
- camp
- warehouse building
- mine dry
- open storage area
- truck shop
- assay lab and metallurgical laboratory
- fuel storage and distribution facilities, including fuel station
- security / gatehouse
- power supply and distribution
- communications system
- sewage system
- water supply

The facilities will be located to minimise the overall footprint and excavation effort and maximise operational efficiency. Wherever possible, the layout takes advantage of the flattest slope in the area.

18.7.1 Administration Building

The administration building will be a modularised structure that provides working space for management, supervisors, geology, engineering, and other operations support staff.

18.7.2 Camp

A modularised accommodations facility will be located in the infrastructure area between the open pit facilities and the concentrator. This camp will be installed for construction personnel, and refurbished as necessary at the start of operations.

18.7.3 Mine Dry

A mine dry facility, including lockers and shower facilities, will be provided. The mine dry will be a modularised structure located near the camp.

18.7.4 Truck Shop

The truck shop building will be a pre-engineered building with an overhead clearance of at least 10 m. The building will be designed to provide facilities for maintenance and repair, minor office space, clean and dry areas, and general storage. It will be erected at the crushing plant area near the mining haul road and the warehouse.

The truck shop will house light- and heavy-vehicle maintenance bays, a welding and machine shop, and an electrical and instrument shop. The truck wash and tire change building is included within the truck shop. The building will contain a wash bay, maintenance bay, tool crib, compressor room, hot water pressure system, and an oil separator. Waste oil will be used as fuel in the refuse incinerator with any remaining oil removed and discarded at an approved facility. The tire change area will be nearby, but set apart from the other areas for safety.

18.7.5 Light Vehicle Maintenance/ Warehouse

A light vehicle and plant equipment maintenance/warehouse facility will be provided near the open pit and crushers. The maintenance area will be equipped with a crane. The warehouse area will be sized to accommodate all the mine fleet equipment spares and maintenance shop supplies. Process materials will be stored separately near the concentrator building.

18.7.6 Open Area Storage

Open area storage areas will be provided for construction laydown and operations, as well as maintenance storage for equipment and materials at the mine site area, camp and infrastructure area, and at the concentrator area.

18.7.7 Assay Laboratory

An assay/environmental laboratory will be located in a separate modular building. The laboratory will be a single-storey structure equipped to perform daily analyses of mine and process samples.

18.7.8 Fuel Storage & Distribution

An area will be designated near the truck shop for fuel storage and dispensing. The fuel storage and dispensing facility will have a lined containment area, so that spills are confined and can readily be cleaned up. This will prevent the need for costly remediation during site closure.

Diesel fuel will be required for mobile mine equipment, some small trucks, and surface vehicles. The pumping station allows both light-duty vehicles and heavy-duty mining equipment to be refuelled. Approximately two weeks of fuel storage will be provided to accommodate interruptions in supply due to weather or road issues.

Propane storage vessels will be provided for field maintenance and space heating fuel.

18.7.9 Security/Gatehouse

A security/gatehouse will be located on the site access road at the plant site.

18.8 Power Supply

Giga Metals Corporation commissioned Kerr Wood Leidal Associates Ltd. (KWL) to review power supply options and undertake a preliminary assessment of power supply options to support the development and operation of the Turnagain Mine.

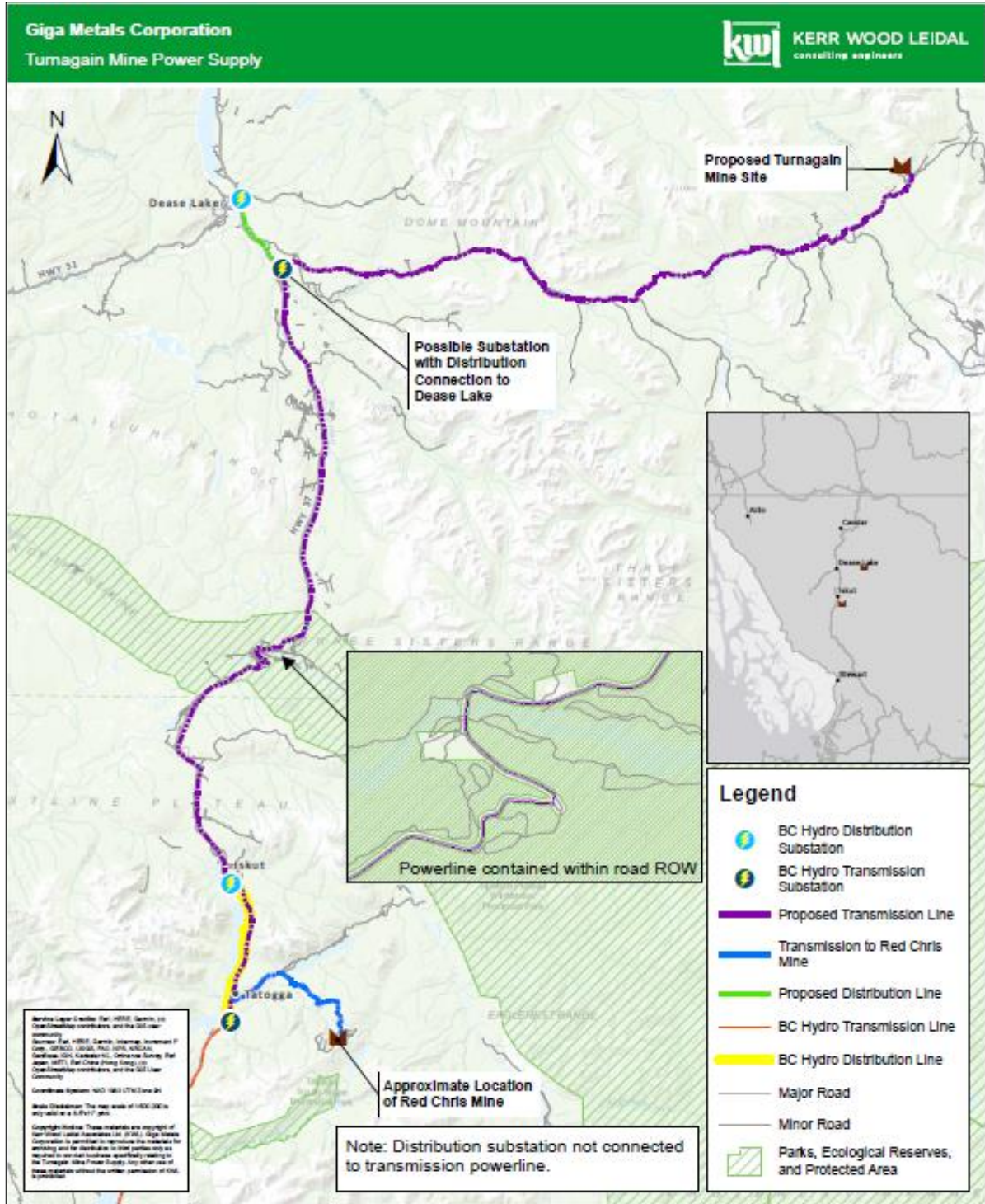
Since the 2011 PEA, BC Hydro completed the Northwest Transmission Line (NTL) from Terrace to Bob Quinn. In addition, the NTL Extension was built to Tatogga Lake to provide power for the Red Chris Mine, and a 25 kV line was built to serve the community of Iskut. The proposed Turnagain Mine is approximately 160 km (powerline route) from an existing operating BC Hydro 287 kV substation at Tatogga Lake (see Figure 18-6).

It is proposed that a 287 kV transmission line be built between the existing BC Hydro substation at Tatogga Lake and a new substation to be built south of Dease Lake near the mine access road. Once built, this line would be sold at a negligible price to BC Hydro to own and operate (sale of the transmission line is not a source of revenue). From the new substation near Dease Lake, a 25 kV distribution line could be built to serve the community of Dease Lake, and the 287 kV line extended to the mine site. The point of interconnection to BC Hydro's system would be the proposed new substation near Dease Lake. An operating voltage of 287 kV for the line has been assumed, as a lower voltage, such as 138 kV, would not be adequate for the Turnagain Mine electrical load in Phase 2.

In addition to the option of connecting to BC Hydro's grid through an extension of the NTL, the option of powering the mine with a natural gas-fired power plant was also assessed. In this option, liquefied natural gas (LNG) would be trucked to the mine site, gasified, and used to produce power through combustion turbines. A range of renewable power options was examined for use as potential fuel savers or alternatives to a BC Hydro connection or LNG combustion turbines. These options include variable wind, geothermal, hydroelectric, and connection to hydroelectric projects in Alaska. The initial screening of these options did not indicate they would be economically competitive with interconnection to the NTL or on-site natural gas-fired generation.

On-site LNG-fired power options have a higher cost and higher greenhouse gas emissions (CO₂e) than the BC Hydro tie-in. Although viable, this approach is not recommended unless regulatory hurdles for a BC Hydro tie-in are insurmountable (this is not expected). Renewable options, such as wind, could offer lower operating cost power than LNG with increased capital cost, and should be investigated as an operating cost reduction if the LNG power option is pursued. Alternative LNG supply options in northeast BC and coastal liquefaction facilities in the Prince Rupert-Kitimat area should also be reviewed if the LNG power option is pursued.

Figure 18-6: Proposed Transmission Line



Source: KWL, 2020.

Based on the NTL and other powerlines in BC, the construction of a 287 kV transmission line from Tatogga Lake to the Turnagain Mine is technically feasible. Optimisation of the transmission line route is required as additional project information becomes available. See Section 21 for capital and operating costs, and Section 26 for recommendations for further study.

18.9 Site Power Distribution

From the main substation (25 kV line up) located at the concentrator (which has the highest power draw), 25 kV overhead lines will deliver power to the following:

- two sets of electrical distribution equipment for 18 MW ball mills
- step-down locations consisting of 4 kV transformers, power distribution equipment, 4 kV motor control, and 4 kV variable frequency drives
- step-down locations consisting of 600 V transformers, power distribution centres, and 600 V motor control centres (MCCs)

From the 25 kV line up, 25 kV overhead lines will also extend to deliver power to:

- pit and mining equipment loads
- tailings pumping and reclaim areas
- camp and miscellaneous service facilities

In locations where loads are logically grouped, electrical rooms will be provided with area step-down transformers located outside the exterior walls. Within the electrical rooms will be located the relevant 4 kV and 600V electrical equipment, and the process control equipment.

A 4 kV emergency power system is provided to support critical process area loads, as identified in ongoing project planning. A Critical Process MCC is provided in each electrical room and connected to the area's stand-alone generator so that, should utility power fail, the critical equipment can be restarted after the emergency generator comes online.

Frequency of the power supply is 60 Hz alternating current (AC). Operating voltage levels are as follows:

- Medium voltage: original equipment manufacturer (OEM) equipment 4.16 kV, three-phase, four-wire, high-resistance grounded. Note that the ball mills will likely require 13.8 kV.
- Low voltage: motors larger than 0.5 hp 575 V, three-phase, three-wire 5A resistance grounded
- Area lighting: interior and exterior 120 V or 347 V, single phase, solidly grounded
- Room lighting: 120 V, single phase, solidly grounded
- Control voltage: A 120 V, single phase, solidly grounded
- Control voltage: B 24 V, direct current (DC) (if required to suit OEM equipment)

- Instrumentation loop voltage: 24 V direct current (VDC), 4 to 20 mA.

18.10 Communication System

The site communications systems will be supplied as a design-build package; the scope will be defined in future project phases.

19.0 MARKET STUDIES & CONTRACTS

19.1 Nickel Markets

19.1.1 Overview

After many years of annual surpluses, the global nickel market moved into deficit in 2016. Although the shortfall in that year was moderate, it was followed by larger deficits in 2017 and 2018. However, the ongoing ramp-up of nickel pig iron (NPI) production in Indonesia and China led to a small global surplus in 2019. With further capacity expansion in Indonesia and the impact of the Covid-19 pandemic on global nickel demand, the nickel market will be in significant surplus in 2020—a situation that is expected to prevail for much of the decade.

It is projected that supply will start to fall behind growth in demand in 2029 with the need for new nickel supply from unidentified resources beginning in 2032. The market requirement for new supply will increase rapidly from 133 kt (including probable projects) by 2030 to 1.30 Mt by 2040. To encourage investment to bring these projects to market, it is forecast that nickel prices will need to average at least US\$16,500/t (US\$7.50/lb) in the long term.

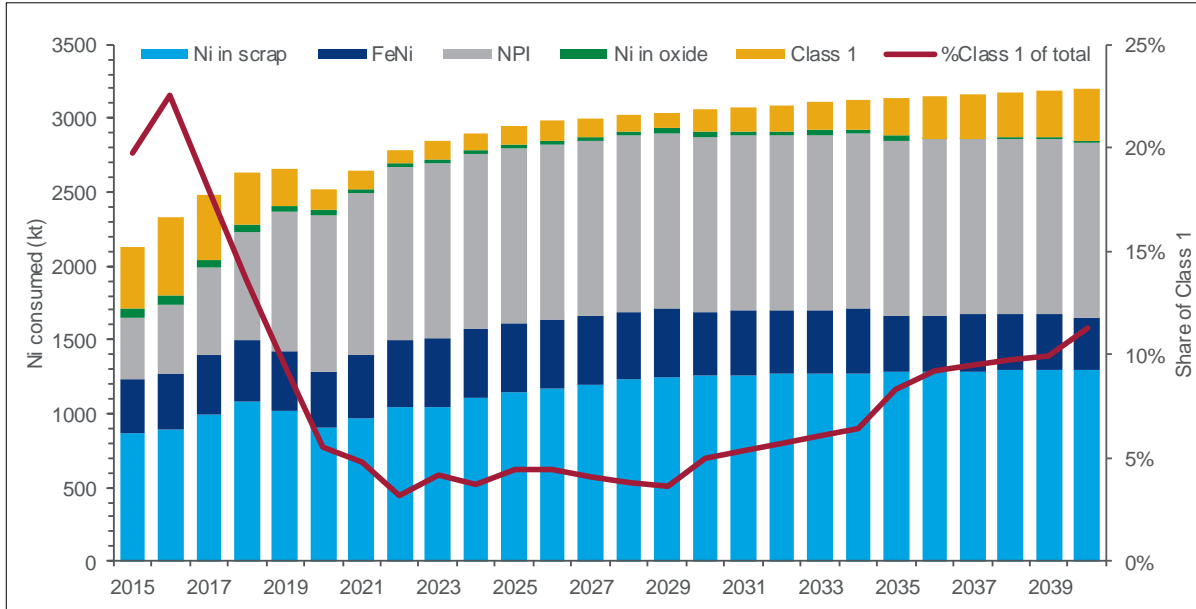
19.1.2 Uses & Marketing

Nickel is predominantly used in the production of stainless steel (~70% of nickel demand), with the balance being consumed for high nickel alloys, chemicals, plating, and batteries. The expected demand for nickel in stainless and non-stainless end uses is shown in Figure 19-1. Note that the scrap nickel inputs to stainless steel is not new nickel introduced to the market, but recycled nickel units, and is not counted in any other supply-demand calculations. At present and over the next few years, the portion of world nickel demand that will go to EV batteries remains comparatively small; it is only after 2025, and especially from 2030, that the potential quantities involved become more critical for the nickel market in general (Figure 19-2).

19.1.3 Supply/Demand

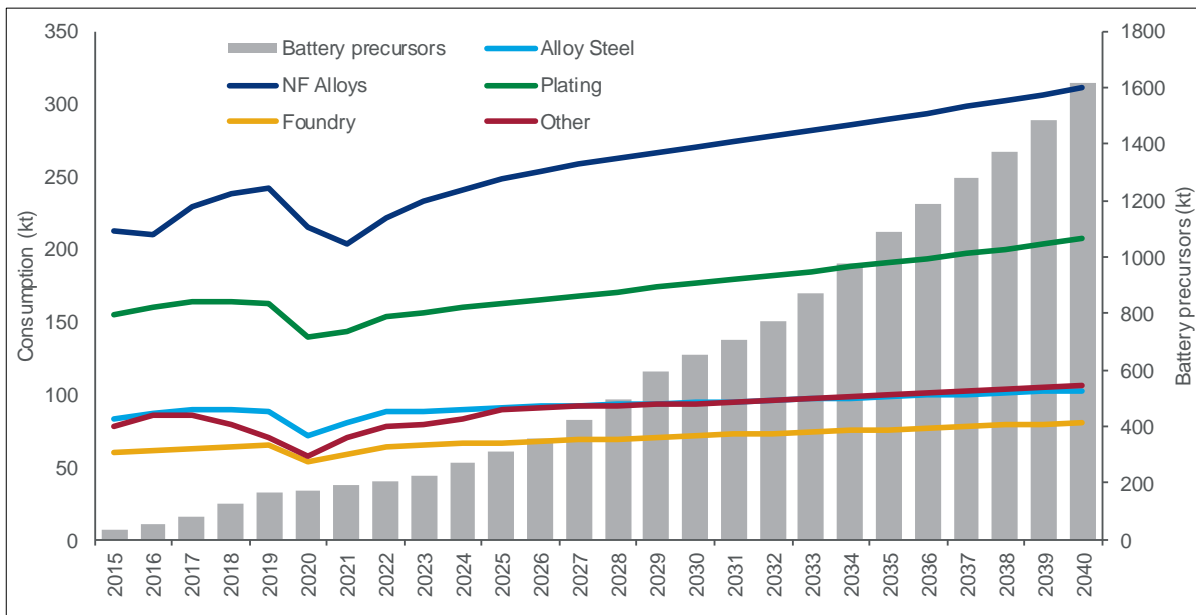
World nickel demand increased by 5.2% in 2019 to 2.43 Mt. However, the global impact of Covid-19 will lead to a forecast 4.7% contraction to 2.31 Mt in 2020. While China is forecast to show 0.9% growth, the world ex-China is hardest hit with a contraction of 12% (Figure 19-3). Despite this, growth at a CAGR of 2.7% will raise world demand to 2.78 Mt in 2025. Over the long term, a CAGR of 2.9% raises nickel demand to 3.15 Mt in 2030 and 4.33 Mt in 2040. Over the next 20 years, growth in nickel demand becomes increasingly dominated by an accelerating uptake in the battery segment due to the anticipated expansion in global electrification of transportation and energy storage systems (ESS). At the same time, primary nickel uptake in stainless will decelerate due to greater use of scrap in China. As a result, the stainless share of global nickel demand is projected to decline from 65% to 70% at present to less than 50% of demand in 2040, whereas that of batteries for EVs and ESSs will increase from 7% to 37% over the same period.

Figure 19-1: Consumption of Nickel in Stainless Steel by Nickel Product Type



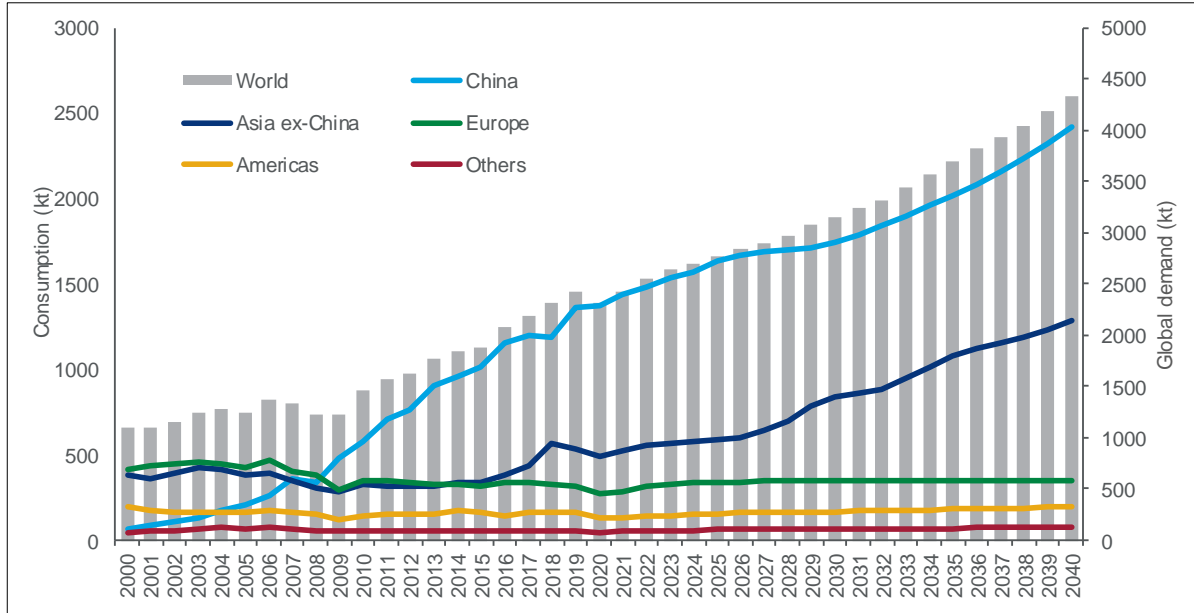
Source: Wood Mackenzie, 2020.

Figure 19-2: Nickel Demand for Non-Stainless Steel Uses



Source: Wood Mackenzie, 2020.

Figure 19-3: Global Nickel Consumption by Region



Source: Wood Mackenzie, 2020.

The forecast average annual increase in nickel demand in EV/ESS battery use (as Class 1 or chemicals) from 2025 to 2040 is 84 kt/a; nearly two Turnagain projects (at Phase 2 rates) every year.

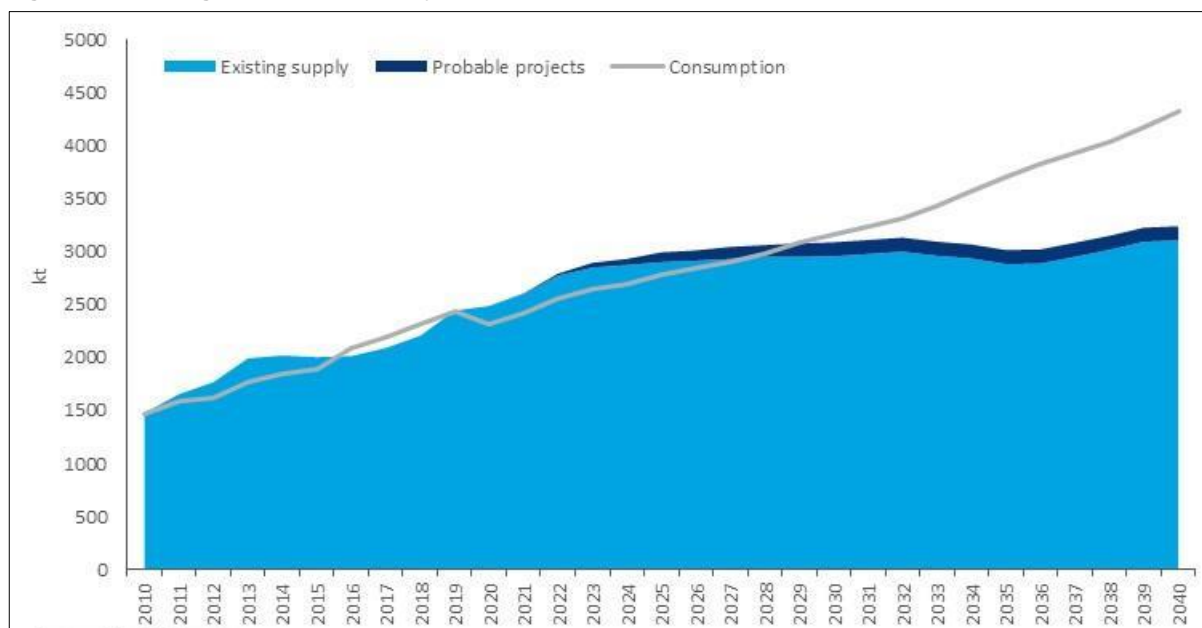
Over the midterm, the combined impact of sustained expansion in Indonesian NPI and declining growth in primary nickel use in Chinese stainless as scrap use accelerates is that the world nickel market is in surplus from 2020 through to 2028. However, from around 2027 we project a surge in demand for nickel in EV batteries, helping the market to return to deficit by 2029. This is exacerbated by anticipated closures, due to exhaustion of currently defined economic reserves, at Cerro Matoso (in 2029), Nickel West (2032), Murrin, Koniambo and Long Harbour (all 2034).

By 2030, the market needs around 133 kt of new supply which can be provided by projects in the Wood Mackenzie probable projects list. However, by 2035, a further 510 kt of new nickel supply will be required from (as-yet) unidentified resources. By 2040, the figures increase to 1.3 Mt of nickel, of which 1.17 Mt would need to come from unidentified resources. The forecast average annual increase in total nickel supply required from 2025 to 2040 is over 80 kt/a, or almost two Turnagain projects (at Phase 2 rates) every year.

Figure 19-4 shows that the long-term shortfall in nickel supply is 1.3 Mt/a. To supply such a large quantity of nickel by then will be a considerable challenge for investors and producers alike, especially given that the typical time required for development, construction and ramp-up of a new facility can take eight to ten years, and 2030 is only 10 years away. It is also noteworthy that this substantial shortfall is arrived at with moderate demand growth over the long term and a

reasonably conservative EV demand forecast. Clearly, more bullish estimates will only make the situation more untenable.

Figure 19-4: Long-term Nickel Supply & Demand



Source: Wood Mackenzie, 2020.

One main risk to this outlook is the considerable NPI expansion potential in Indonesia, where there is about 350 kt/a nickel capacity identified in proposed possible and probable projects. With the establishment of large industrial parks, such as Morowali and Weda Bay, brownfield capacity can now be added in less than 12 months and ramp-up completed in as little as three. Thus, new capacity can be added quickly with only modest capital outlay (e.g., Nickel Mines Australia’s RKEF lines in Morowali were added for around US\$10,000/t nickel a year).

One other risk is that our assumptions on EV battery recycling rates prove optimistic. We currently assume that ~25 kt Ni will be recycled in 2025, growing rapidly to 84 kt by 2030, 240 kt by 2035 and 540 kt by 2040. This is a significant tonnage of nickel to be returned to the supply pool. Without this recycle stream, the requirement for nickel by 2035 and beyond would be significantly higher than shown and would result in a higher long-term price requirement.

Aside from NPI, the main recent development signalling where future nickel supplies may come from, specifically those needed by the new EV battery segment, is the ongoing construction of three HPAL facilities in Indonesia (as announced in late 2018): QMB and Huaqing, both at Tsingshan’s Indonesia Morowali Industrial Park (IMIP); and Lygend on Obi Island. Planned capacity at each site is 50 to 60 kt/a nickel in either nickel sulphate or an intermediate for conversion to nickel sulphate. Officially reported schedules assume these facilities will enter production in 2021, although this may prove to be optimistic. None of the projects has obtained

permits for tailings impoundment or disposal, and recent news suggests that QMB is currently essentially on hold. The process flowsheet for the plants is apparently based around that of Ramu (PNG). It should also be noted that ore feed composition in Indonesia will be different to that at Ramu and will vary depending on the contracted ore source. This in turn could result in prolonged ramp-up periods due to ore variability and process instability. Two other HPAL projects have also been announced—a Sumitomo Metal Mining/Vale joint venture at Pomalaa, and PT Ceria at Kolaka—but neither are yet committed and will not be in production before 2025 at the earliest.

If these first three projects are successful, there is likely to be widespread, Chinese-led enthusiasm to invest in similar ventures, and these could provide the nickel the market will need over the next 10 years, perhaps even exceed requirements. However, although proliferation is a possibility, the challenge of waste disposal will be a major constraint. HPAL produces more waste than the ore feed it consumes (50 kt/a of Ni will produce approximately 5 to 6 Mt/a of waste slurry), and waste can only be discarded behind land-based tailings dams, requiring a huge amount of space (for fine chemically precipitated tailings materials in tectonically active areas), or by deep sea disposal. Both are likely to provoke considerable environmental concern warranting challenging legislation.

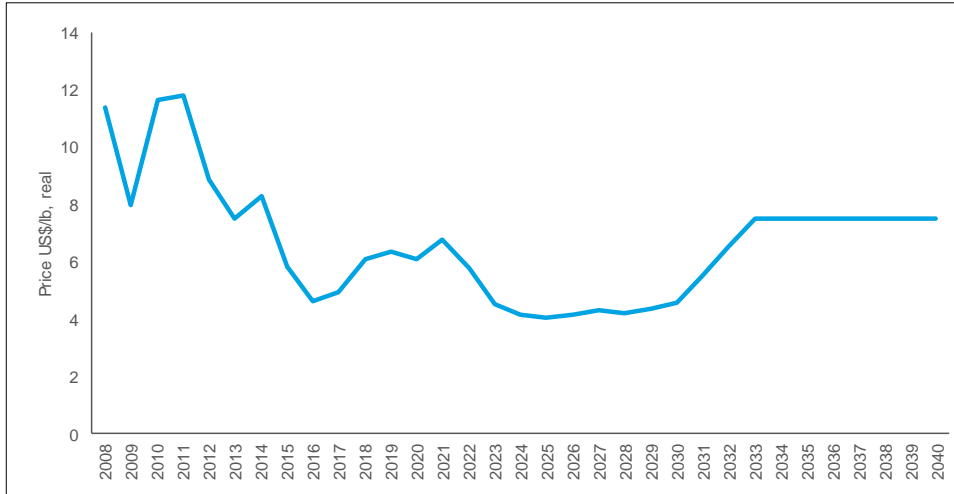
If these HPAL projects are delayed further by unforeseen technical issues, one alternative for those companies seeking to supply nickel to the battery segment could be to convert FeNi or NPI into a matte that can then be refined to nickel sulphate. This is an option under consideration by Huayou at Weda Bay. Certainly, there would be no shortage of a raw material for this process route, as there appears to be little stopping the continued expansion of NPI capacity, even if it is all currently earmarked for use in stainless steel. However, this process option does require additional smelting and refining facilities and has additional issues with slag and precipitated iron residues resulting from the high iron-to-nickel ratio in NPI.

19.1.4 Pricing

As shown in Figure 19-5, supply starts to fall behind growth in demand from 2029 with the need for a new nickel supply from unidentified resources in 2032. As noted above, the market requirement for new supply increases rapidly to 133 kt (including probable projects) by 2030 and 1.71 Mt by 2040. To encourage the investment to bring these projects to market, it is forecast that nickel prices will need to average at least US\$16,500/t (US\$7.50/lb) in the long term.

If one considers the growing requirement to source commodities that meet specific environmental, social and governance (ESG) criteria, then we are of the opinion that the long-term nickel price would need to be higher than our current base case forecast of US\$16,500/t to incentivise the development of such projects. Thus, narrowing down the projects evaluated based on jurisdiction, land-based tailings disposal and access to predominantly non-diesel generated power, we estimate that a long-term nickel price of at least US\$18,700/t (US\$8.50/lb) would be necessary to encourage sufficient capacity to the market to both meet our market requirement and satisfy ESG requirements.

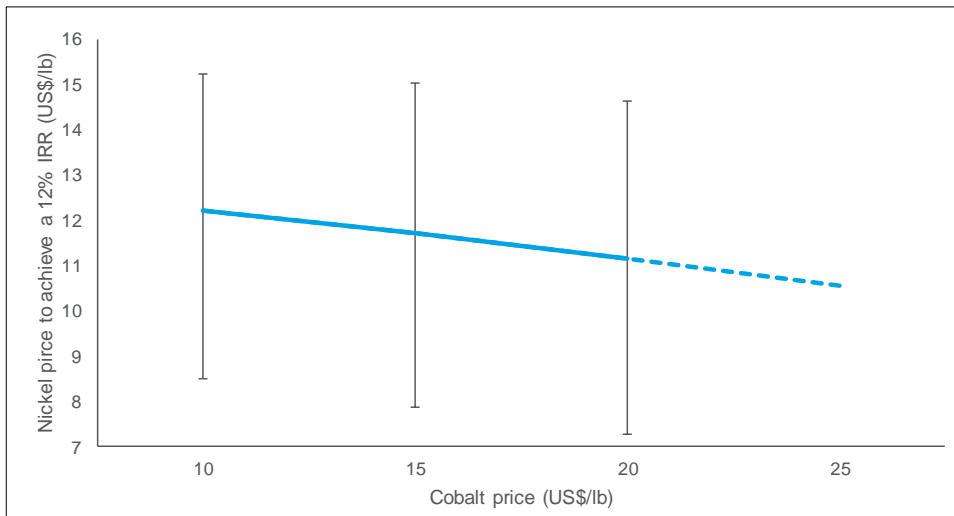
Figure 19-5: Nickel Price Forecast



Source: Wood Mackenzie, 2020.

Looking at current demand in the battery sector, approximately 30% of nickel units consumed are derived from laterite ore sources, and the bulk of this from intermediates produced from high-pressure acid leach (HPAL) operations (e.g., Ramu, Ravensthorpe, Gordes and VNC). Given that the bulk of nickel resources are in the form of laterite ores, it appears likely that much of the future supply requirement will be sourced from laterites and therefore through the adoption of HPAL technology. Wood Mackenzie has assessed a number of laterite projects (four in Australia and one in the Philippines). Figure 19-6 shows the average and range of nickel prices required by these projects to generate a 12% IRR with an extrapolation to the base long-term cobalt price of US\$22.30/lb.

Figure 19-6: HPAL Incentive Price



Source: Wood Mackenzie, 2020.

While the lower end of the nickel price range fits broadly with the ESG nickel price noted above, on average they are considerably higher. Wood Mackenzie would expect the long-term nickel price would need to be approximately US\$23,950/t (US\$10.86/lb) for the development of new nickel supply solely from HPAL projects.

19.2 Cobalt Markets

19.2.1 Uses & Marketing

Cobalt is used in a variety of applications broadly split into two groups: metallurgical (superalloys, high-strength steels, magnets, cemented carbides) and chemical (batteries, catalysts, paints, ceramics). The rechargeable lithium-ion battery sector accounts for the largest share of consumption at present and has by far the greatest growth potential.

We estimate refined cobalt demand reached 126 kt in 2019, up by 6% from 2018 levels. Of this total, we expect demand from batteries accounted for a 55% share. Consumer electronics remains the largest sub-sector for cobalt use within batteries; however, we expect electric vehicles (EVs) to surpass this in the next two years.

Cobalt mineralisation is focused around the African copper belt spanning the Democratic Republic of Congo (DRC) and Zambia; sulphide ore deposits in Canada, Scandinavia, Russia and Australia; and laterite ore deposits in Cuba and Asia Pacific. Though it is widespread, cobalt typically occurs at such low concentrations it is uneconomical to produce on its own. As such, it is mined mainly as a byproduct of other metals, primarily copper and nickel.

Traditionally, all cobalt was sold at so-called 'producer prices' set by the major refiners of the metal located in Zambia and the DRC (then Zaire). However, a deteriorating political situation in the DRC in the early 1990s and corresponding disruptions to production saw these reference prices start to lose relevance in the international market.

Eventually the producer pricing system broke down when Zambian producers started selling based on the Metal Bulletin prices for 99.8% (high grade) and 99.3% (low grade) metal. These prices, generated using journalistic price discovery methods, have become the benchmark reference prices in the industry since then. In 2010 the LME launched 2010 cash and futures contracts for cobalt.

19.2.2 Supply/Demand

Supply growth will outpace demand over the medium term, as a number of key copper-cobalt operations ramp up in the DRC. The DRC's share of global mined cobalt supply reached 71% last year, compared to 63% in 2015. This oversupply narrative over the medium term has been aggravated by a faster adoption of high-nickel battery chemistries. While the large surpluses we project will not materialise, the last year has demonstrated that large stocks of intermediates can build up through the supply chain and keep pressure on prices. Additionally, we expect this prolonged period of excess supply to see smaller suppliers increasingly squeezed out of the

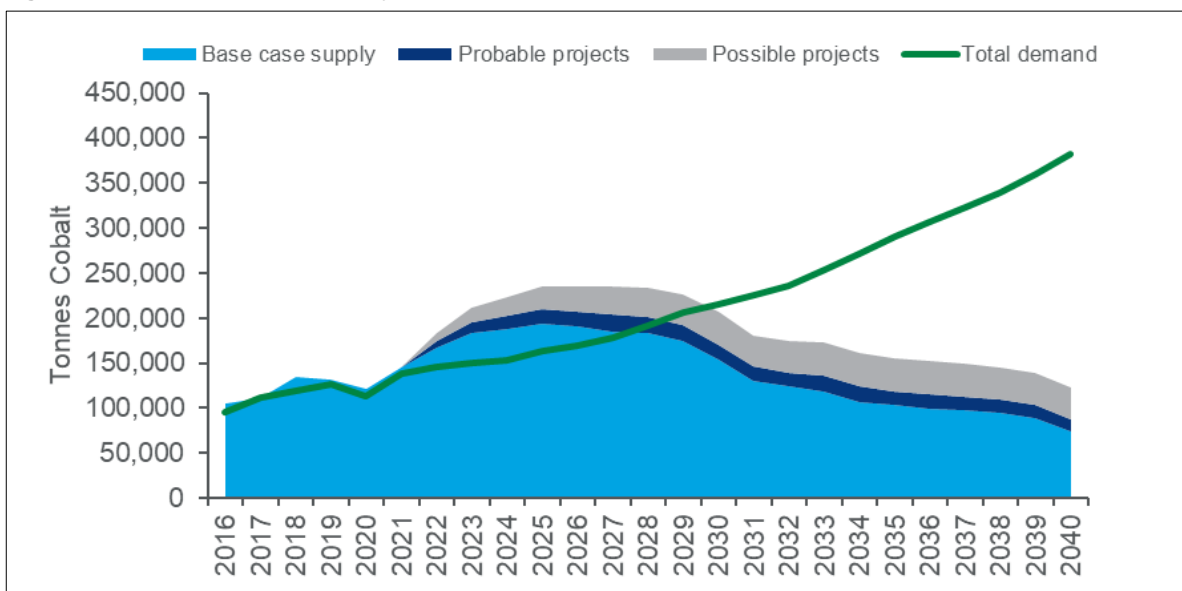
market, as lower prices render operations uneconomical and environmental, social and governance (ESG) risks affect refinery procurement strategies.

Long-term cobalt demand will be predominantly driven by growth in the lithium-ion battery sector. Portable electronics initiated the first ‘battery boom’ over a decade ago and we expect strong growth through the forecast. However, battery demand from the portable electronics and ESS sectors will be completely overshadowed by the scale of EV growth over the long term.

Under the Wood Mackenzie base case electric vehicle forecast, we expect passenger car EV (full-electric and plug-in hybrids) sales to reach 7% of total passenger car sales by 2025, and 14% by 2030. Importantly, nearly all OEMs have committed to utilising ternary battery chemistries (nickel-manganese-cobalt, NMC or nickel-cobalt-aluminum, NCA)—which contain cobalt—for their higher energy density and other properties. Different ternary cathode chemistries have varying lithium, nickel and cobalt consumption on a per kilowatt-hour basis. The trend towards NMC 811 will increase nickel and slow cobalt demand. Yet the overall shift towards ternary cathodes provides upside for all three metals.

Over the longer term, we see a notional deficit emerging in the cobalt market as EV-led demand starts to accelerate rapidly (Figure 19-7). We currently expect a deficit to emerge in the cobalt market by 2029, although this could be pushed out slightly by high stocks accumulated in preceding years. However, we would highlight this is predicated on a relatively conservative outlook for EV penetration, uninterrupted DRC mine supply and continued thrifting of cobalt from cell chemistries.

Figure 19-7: Global Cobalt Supply/Demand Balance



Source: Wood Mackenzie, 2020.

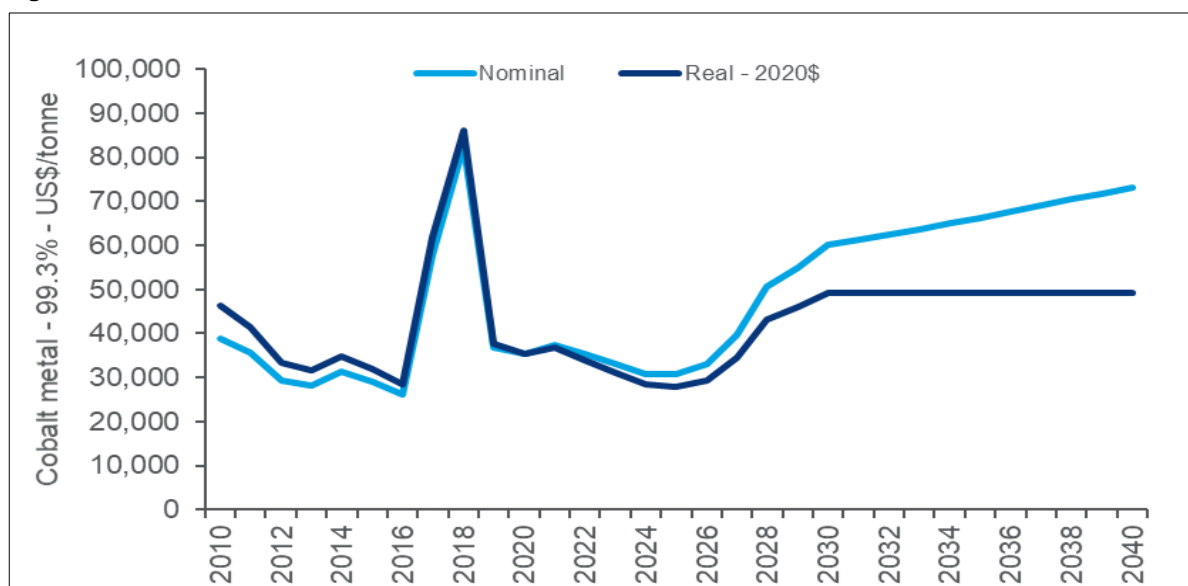
By 2030 cobalt demand reaches 216 kt. Factoring in the ‘probable’ and ‘possible’ projects we are just about able to meet demand, and the secondary supply of cobalt from recycling will become increasingly important to the industry.

With demand growing at ~13 kt/a between 2025 and 2035, the industry will essentially need a new greenfield mine to start up each year. Putting financing to one side, this assumes suitable cobalt deposits can be found to allow for this. Meanwhile, developments such as the DRC’s mining code are already discouraging long-term investment in cobalt.

19.2.3 Pricing

In terms of pricing, marginal cost and incentive pricing models are not appropriate for cobalt given it is mostly produced as byproduct of nickel and copper operations. As such, the economics of projects are much more dependent on nickel and copper prices than cobalt. Instead we look at the long-term average in real terms. Since 1950 this has averaged \$49,163/t (\$22.30/lb) and functions as Wood Mackenzie’s long-term price from 2028 (see Figure 19-8).

Figure 19-8: Cobalt Price



Source: Wood Mackenzie, 2020.

19.3 Concentrate Markets

19.3.1 Nickel Concentrate Supply/Demand

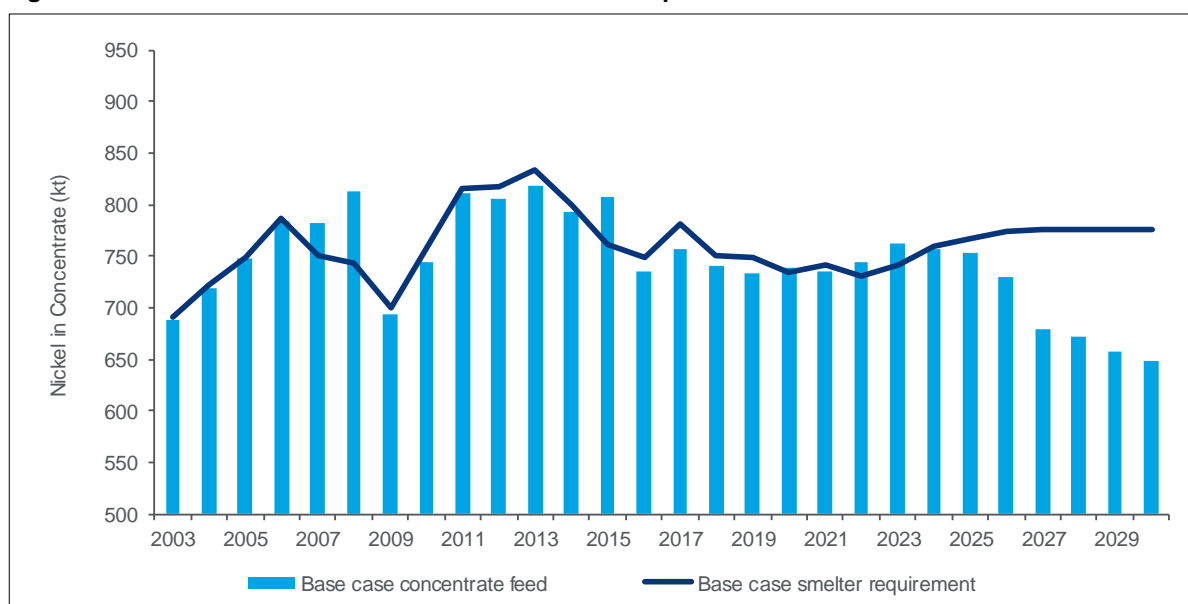
There are essentially 14 sulphide smelters in operation capable of processing concentrate from Turnagain. Of these, seven are actively procuring third-party concentrates and one has the potential to require material.

The concentrate analysis forecasts a balanced concentrate market through to 2024, at which point the market starts to turn to significant deficits (Figure 19-8). There are projects currently under evaluation that are considered probable projects, which could provide sufficient concentrate feed to maintain a balanced market from that time. Nevertheless, new sulphide mine development is needed to meet the forecast smelter output, be that from the current probable projects list or others.

19.3.2 Indicative Terms for Turnagain Concentrate

Historically, contracts were developed to match the specific smelter’s abilities with respect to metal recoveries and detrimental elements. For example, BHPB Group’s Kwinana refinery has no cobalt, copper or PGM (platinum group metal) recovery circuit, other than as a copper sulphide and mixed Ni:Co sulphides. Therefore, the plant has offered lower cobalt, copper and PGM payment terms than, for example, those offered by Falconbridge (now Glencore) or Inco (now Vale), both of which have cobalt, copper and PGM refining capability.

Figure 19-9: Global Nickel Concentrate Treated & Net Required



Source: Wood Mackenzie, 2020.

What is apparent from the available information is that tenders for concentrate have become more favourable to the miner in recent years. In the late 1990s, the combined treatment and refining charges (TC/RC) were equivalent to between 45% and 55% of the nickel price before the addition of transportation. More recently, this figure is in the range of 22% to 35%, and is a consequence, presumably, of smelters needing additional feed rather than taking concentrate because it is on offer.

Nickel concentrate contracts have taken several forms, such as a fixed treatment charge with a variable refining charge related to the LME nickel price, a variable percentage of nickel price payable, and a payable nickel percentage with a variable refining charge. This latter form may or may not also include a fixed treatment charge. The straight percentage of nickel price charge related to the LME price was favoured by the Chinese in their off-take deals and appears to have become the “benchmark” for current tenders.

Unlike, for example, the copper market, there are no global benchmark treatment and refining charges set for nickel concentrates, and each contract is negotiated on an individual, private, and confidential basis. As a result, it is generally difficult to obtain details relating to concentrate off-take agreements. The following indicative terms should therefore be viewed on a “best endeavours” basis and have been determined through various conversations with both buyers and sellers of concentrates.

The current terms for nickel concentrates indicate 78% payability for nickel, 30% to 40% pay on copper and 35% pay for cobalt (if above 0.3% in the concentrate, zero pay if below 0.3% Co), all CIF China port. There was no indication that higher grade nickel concentrate would command any preferential (higher) payabilities. However, it was acknowledged that there is currently a paucity of such material and therefore it has not been necessary to address this potential in the market. Concentrates with high Fe:MgO ratios are definitely seen as being desirable (e.g., Western Areas Flying Fox concentrates), as blending of such material improves the capability to take high MgO concentrates on which offered terms would be lower than those indicated and potentially a penalty applied for the elevated MgO.

While the above appear to be the current benchmark, there were clear indications that such high payabilities on nickel may not be sustainable going forward. While specific details as to why this was the case were not provided, it seemed to relate to the potential for the concentrate market to move to surplus in the next few years, making it more difficult to miners to place material at smelters with available capacity. As such, we would recommend evaluating the Turnagain project at nickel payabilities in the range of 68% to 75% to ensure robust economics under such circumstances.

At the currently envisaged initial production level of 22 kt Ni/a in concentrate by 2025, it could be possible to have a single off-take agreement with any of the indicative preferred smelters of Jinchuan, Boliden (Harjavalta), Glencore (Sudbury), and Vale (Sudbury). However, a combination of at least two off-takers would be the most likely viable option; this is typical for current third-party sellers at such levels of nickel in concentrate production.

BHP Group (Kalgoorlie) may also be a viable off-take option. Tsingshan, which was processing sulphide concentrates through a roaster at its Fuan plant as feed to produce nickel pig iron, has ceased to be active in the market, but could provide an opportunity in the future.

Should production levels be raised to the proposed 44 kt Ni/a in concentrate by 2030, then numerous off-takes would almost certainly be necessary to place the material successfully. Wood

Mackenzie's current forecasts indicate that there will be sufficient demand for such tonnages of nickel within the concentrate market at that time.

One factor that Wood Mackenzie has considered is the potential for high-grade (~20% Ni) concentrates to be treated directly by hydrometallurgical processing. This has been demonstrated commercially at Sherritt's Fort Saskatchewan facility (which treated concentrate from 1954 to 1990), at BHP's (then Western Mining Corporation) Kwinana refinery, and is currently being employed at Vale's Long Harbour refinery (which is treating 100% of the Voisey's Bay concentrate). Hydrometallurgical processing has also been evaluated more recently by Independence Group and Western Areas, both in Australia, to process all or part of their concentrate production from the Nova-Bollinger and Flying Fox operations. The processing of high-grade nickel concentrates to directly produce nickel chemicals or Class 1 nickel has the potential to improve the revenue generated from a mine's output. However, this option has been excluded from the scope of this study, as insufficient data currently exist on the commercial and technical feasibility to allow a sound evaluation of the economic viability.

20.0 ENVIRONMENTAL BASELINE STUDIES, PERMITTING & SOCIAL OR COMMUNITY IMPACT

20.1 Environmental Baseline Studies

In preparation for an environmental assessment of the project, selected baseline environmental studies were initiated in 2004 and are ongoing. Several additional baseline environmental studies will be required to fully satisfy the requirements of an environmental impact assessment, as well as to support the necessary permits, approvals, and licences for the project. This will include studies or monitoring of fish and aquatic habitat, wildlife, vegetation, soil, noise, groundwater, air quality, and archaeology. Monitoring programs have various timelines, and some may be required to be in effect for the life of the project. An adaptive management program may also be required to address potential issues as they are identified. The environmental baseline programs carried out to date are described in the subsections below.

20.1.1 Aquatic Life

In 2007, an initial fish and fish habitat baseline study that was conducted for late summer/fall provided an initial understanding of species diversity and abundance as well as habitat features. Additional fisheries and aquatic studies will be required during the environmental assessment process and other permitting processes. The proposed conceptual design for waste management involves displacement and alteration of productive aquatic habitat in Flat Creek Valley. To meet the requirements of the “no net loss of fish habitat” principle of Fisheries and Oceans Canada (DFO), mitigation and compensation measures will be required to replace any lost productivity. Additional seasons and detailed studies of the existing fish species, their life cycle, and utilisation of the physical aquatic habitat will be necessary to design and propose acceptable fisheries compensation plans. The following investigations may be required:

- investigation, mapping, and quantification of existing aquatic habitat and its utilisation (spawning, rearing, overwintering) by resident species in Flat Creek and its fish-bearing tributaries
- estimation of existing number of fishes in Flat Creek and population composition by species
- estimation of present level of production in the aquatic environment (primary production, fish production, etc.) to establish baseline levels and to set goals for mitigation/compensation plans
- Based on fish species inventory in the project area, appropriate design criteria should be incorporated in diversion channel(s) to provide support for fish communities in perpetuity. Depending on negotiations with the BC Ministry of Environment and Climate Change Strategy (MOE) and DFO, additional fisheries compensation options may be expected. To prepare for this outcome, a list of potential compensation options will be compiled during baseline studies. A habitat balance analysis will be required

to delineate achievement of the "no net loss" principle for the project and its components.

20.1.2 Surface Water Quality

Preliminary surface water quality surveys were completed in the project area between 2003 and 2011. Monthly surface water sampling was re-started in late 2018 and 2019 at 13 sites and ongoing monitoring is planned. The program includes sampling sites in Flat Creek, its tributaries, and control sites (AMC 2011).

20.1.3 Soil Quality

Soil geochemical surveys were first conducted by Falconbridge in 1971 and by Bren-Mar in 2003, followed by a comprehensive geochemical soil sampling program initiated by HNC in 2004 involving the collection of more than 2,000 soil samples. Results highlighted two strong copper-in-soil anomalies 2.5 km northwest of the Horsetrail Zone with values exceeding 430 ppm copper and peaks to 3,219 ppm copper. These anomalous areas flank the hornblende diorite-granodiorite intrusion that cuts the older ultramafic rocks in this area. Anomalous platinum-palladium values in soils, in part coincident with the DJ Zone, extend from the northern part of the larger copper-in-soils anomaly. Anomalous nickel values in soils are widespread over the northern part of the Turnagain ultramafic intrusion and within and adjacent to the Horsetrail Zone. The 2004 geochemical program also included the collection and analyses of 330 rock float and 243 bedrock samples from within, and adjacent to, the soil geochemical grid. Results for total nickel and platinum + palladium indicated significant total nickel results (>0.20% to a maximum of 1.9%) in both float and bedrock samples, which are mainly clustered in the area of the Horsetrail Zone and in a smaller area north of the DJ Zone, known as the "central area". Future investigations of soil quality are required to support the environmental impact assessment and permitting efforts.

20.1.4 Groundwater Flows

Groundwater levels in the project area were collected in September 2008 and June 2009 within the main pit with negligible information collected from beyond the pit area. Being spatially constrained, there is insufficient groundwater level data across the project site to enable a characterisation of groundwater resources and flow across the local study and regional study areas (e.g., to identify recharge / discharge zones, or to quantify mine / pit de-watering rates). Although data was collected over two individual years, the data set does not capture the seasonal variation within a particular year. Due to the age of the data (collected more than 10 years ago), information may not be representative of current groundwater flow conditions. Future hydrogeological investigations are required to support the environmental impact assessment and permitting efforts.

20.1.5 Groundwater Quality

Eight groundwater wells, also predominantly from the pit area, were monitored for water quality (i.e., physical parameters, anions and nutrients, and total and dissolved metals) between 2004 and 2011, and limited groundwater quality samples were collected in 2018 and 2019. Although

data were collected over seven years at different locations in the Hard Creek Sub-Catchment, the data set does not capture seasonal variation within a particular year. Based on a preliminary review, groundwater quality data are insufficient to establish baseline groundwater quality conditions across the local study and regional study areas, or to understand the interaction between surface and groundwater quality emergent zones. Additional groundwater quality monitoring is required to establish baseline groundwater quality conditions and support the environmental impact assessment and permitting efforts.

20.1.6 Archaeological Studies

Exploration pre-clearing was completed in 2018 and 2019. Archaeological impact assessment studies are being conducted with the help of Tahltan and Kaska members.

20.2 Regulatory Requirements

20.2.1 Environmental Impact Assessment

The project is subject to a provincial review under the *British Columbia Environmental Assessment Act* as it exceeds the following threshold under Part 3 (Table 6) of the Reviewable Projects Regulation: “A new mine facility that, during operations, will have a production capacity of >75,000 tonnes/year of mineral ore”. The project will also be subject to a review under the federal *Impact Assessment Act*, as it exceeds the following threshold prescribed in the Schedule of Physical Activities specified in the Physical Activities Regulations (SOR/2019-285): Section 18(c): “The construction, operation, decommissioning and abandonment of a new metal mine, other than a rare earth element mine, placer mine or uranium mine, with an ore production capacity of 5,000 t/day or more”. The Environmental Impact Assessment (EIA) process is expected to be conducted in one review process through a substitution agreement between the provincial and federal agencies, and will involve public and First Nations consultation as well as detailed studies of baseline environmental settings and an assessment of potential project impacts. A comprehensive study of potential impacts of the project and its facilities and components on the surrounding environment was initiated by HNC in 2004, as well as public and First Nations consultation efforts.

20.2.2 Permits & Approvals

Options for tailings storage facilities at Hard Creek and Flat Creek were evaluated during the preliminary assessment and conceptual design stages, all of which involved alteration and possible loss of aquatic habitat. Based on the analysis and a mill throughput of 87,000 t/d over a mine life of 25 years, preferred options for a tailings management facility (TMF) have been identified at both Hard Creek and Flat Creek. The possible impact on the either drainage will require authorisation under Section 35(2) of the federal *Fisheries Act* for harmful alteration, disruption, or destruction (HADD) of fish habitat. As part of the authorisation process, mitigation and compensation measures as guided by DFO’s “no net loss” principle will be required. Supporting data and scientific evidence will be provided to satisfy the regulatory bodies that all possible design alternatives have been considered and evaluated, and that fish utilisation and

connectivity would be maintained through implementation of appropriate mitigation and compensation strategies.

The proposed TMF design will likely also require an amendment to Schedule 2 of the Metal Mine Effluent Regulations (MMER) of the *Fisheries Act*, to allow the deposition of tailings to fish-bearing waters. An application for amendment of MMER Schedule 2 must be submitted subsequent to environmental assessment certification of the proposed project.

Other permits, approvals, and regulatory requirements that may apply to the project at various stages include, but are not limited to, the following:

- Migratory Birds Convention Act Authorisation, for vegetation clearing during migratory bird nesting season
- Species at Risk Act Permit, for activities that may affect a listed species or its habitat
- Explosives Act License and Permit, for explosives transportation and magazines
- Transportation of Dangerous Goods Act and Regulations Permits, for transport of dangerous goods by rail, road or air
- Mines Act Permit, for approval of the Mine Plan and Remediation and Closure Plan
- Environmental Management Act Waste Discharge Permit, Waste Storage Approval, for authorisation of waste storage and discharge of wastes to water, land or air
- Heritage Conservation Act Concurrence Letter stating that the assessment is complete
- Wildlife Permit Act Approvals for wildlife salvages and bird nest removal or relocation
- Drinking Water Protection Act Permits for potable water wells, water system construction, and water system operations
- Water Sustainability Act Approvals and Licenses for changes in and about a stream, management of nuisance water from mining operations, and activities requiring surface or groundwater resources for potable or process water
- Forest Act Licence to Cut and Special Use Permit for harvesting, and for use of Crown Land within a Provincial Forest
- Transportation Act Industrial Access Permit, for new roads joining onto public roads
- Public Health Act Permit for regulated activity such as managing septic systems and processing wastewater.

20.3 Indigenous Groups & Local Communities

The project is located within the traditional territories of both the Tahltan First Nation and the Kaska Dena, and roughly 65 km east of the Township of Dease Lake.

Giga Metals is committed to creating and sustaining constructive dialogue and relationships with indigenous groups and local and regional stakeholders to support the environmental, social, and

economic sustainability of the project. Key components of Giga Metals' consultation and engagement strategy will include:

- communication of information in a timely, consistent manner to indigenous groups, local community members, stakeholders and regulators throughout the lifecycle of the project
- early identification and understanding of project issues and concerns, as well as responsive engagement regarding indigenous groups and stakeholder interests
- early, frequent, open, and honest communication to build strong relationships with interested parties, particularly those who will be most affected by the project
- fostering strong, collaborative, long-term partnerships with indigenous groups, regulators, community groups, and other stakeholders

Giga Metals has established consultation and engagement processes with indigenous groups, communities, and stakeholder groups. Further consultation and engagement will be required for the purposes of conducting baseline socioeconomic studies; assessing and reviewing potential environmental effects during the environmental assessment process; developing agreements; developing environmental and social management plans; closure planning; environmental monitoring; providing regular project development updates; and ensuring optimal economic development opportunities and participation during construction and operations.

20.3.1 Indigenous Groups

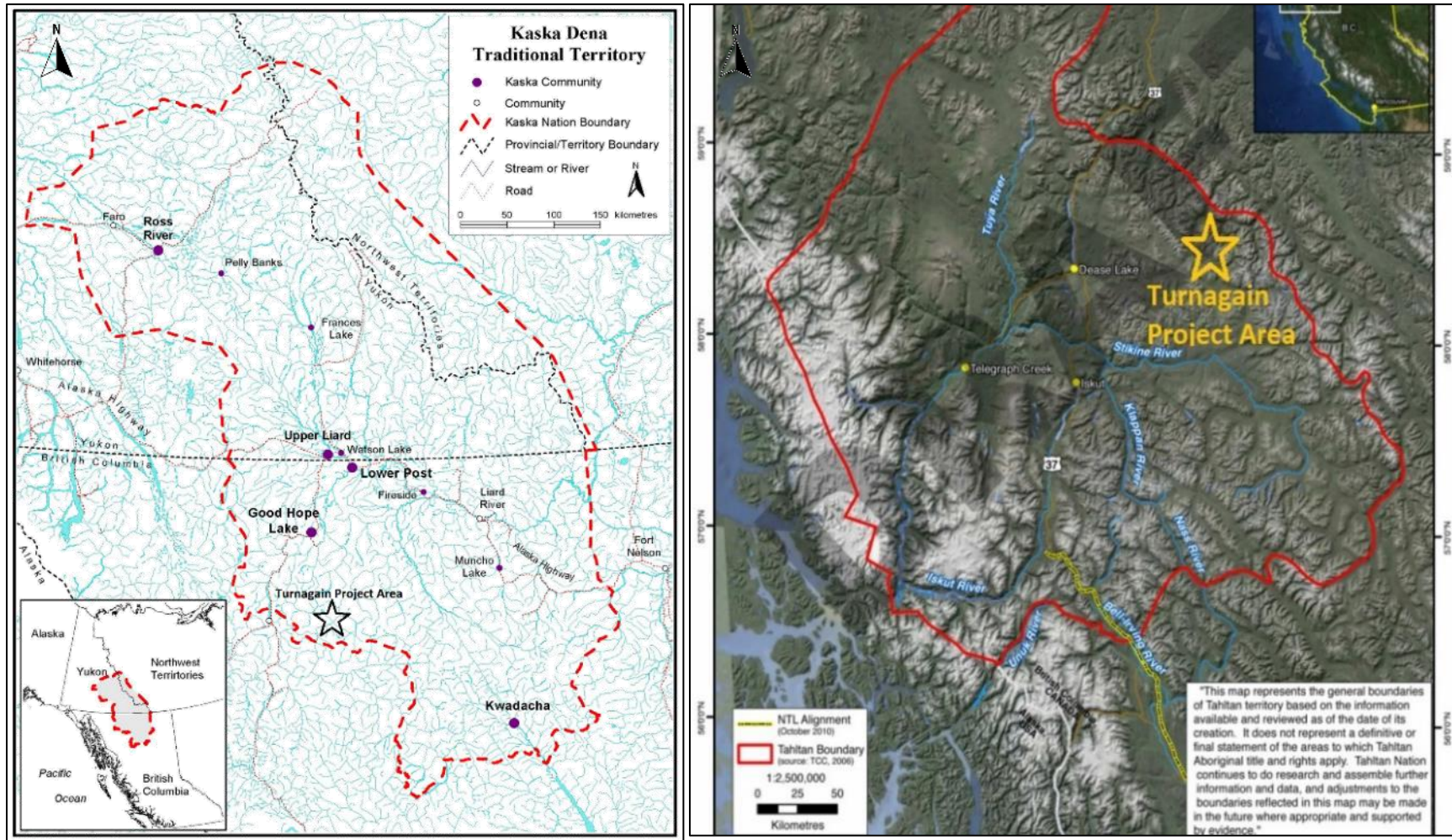
The Tahltan Nation is represented by the Tahltan Central Government (TCG) for aspects related to indigenous rights and title, and natural resource development within Tahltan traditional territory (Tahltan Territory). The TCG represents the Tahltan Band, Iskut Band, and roughly 5,000 members of the Tahltan Nation, and governs according to the principles enshrined in the Declaration of the Tahltan Tribe (1910). Tahltan Nation members comprise over half of the residents in Tahltan Territory, and primarily live in three communities: Telegraph Creek, Dease Lake, and Iskut. The TCG is located in Dease Lake.

Tahltan Territory is unceded, and comprises roughly 95,933 km², or 11% of British Columbia. Tahltan Territory includes the Stikine Watershed and headwaters, ranging from the lower Yukon boreal forest to the Cassiar Mountains to the east, the Skeena and Nass River headwaters in the south, and the Central Mountains in the West.

The Kaska Dena traditional territory and people are represented and governed by the Kaska Dena Council, which is headquartered in Lower Post and represents the five bands of the roughly 3,000 Kaska Dena people, located in the communities of Lower Post, Good Hope Lake, Watson Lake, Ross River and Kwadacha. The area covered by the Kaska Dena traditional territories includes portions of the Yukon Territory, Northwest Territories, and British Columbia. Within BC, the territory range includes Lower Post, Good Hope Lake, and Kwadacha.

Figure 20-1 shows the project location in relation to the Tahltan and Kaska Dena traditional territories.

Figure 20-1: Turnagain Project Relative to Traditional Territories of Kaska Dena & Tahltan



Source: Giga Metals, 2020.

The Kaska Dena Council and TCG are increasingly entering into shared decision-making agreements with the province of BC, regarding land and resource use development in their territory. The Kaska Dena Council (including Dease Lake First Nation) and the TCG have plans, agreements, and protocols to govern land and resource use in their asserted traditional territories. These include the Kaska Dena Land Use Framework; the FLNRO Dease-Liard Sustainable Resource Management Plan (2012), which includes the Dease River First Nation's Principles and Policy For Mineral Exploration and Mine Development Outline; the Kaska Dena Ne'áh', Gu Cha Duga, and the Strategic Land Use Plan Agreement; and the Tahltan Nation's Klappan Plan (2017) to guide land and resource management in the Klappan Area, among others.

The Klappan Plan defines and describes areas of Tahltan traditional territory that are considered acceptable or unacceptable for resource development activities, and defines activities (such as jade and placer mining) that are considered unacceptable for their territory. The Turnagain Project is north of Klappan Area Sacred Headwaters Zone and Zone B North. No industrial activities are considered acceptable for Sacred Headwaters. Industrial activity and resource extraction could occur in Zones B and C, subject to extensive engagement with Tahltan Nation. Tahltan Nation is developing its Tahltan Land Stewardship Plan, with a land use planning process currently under way.

Giga Metals' Indigenous Engagement strategy will be multifaceted and developed in consultation with Indigenous Groups to incorporate their engagement priorities and timelines. A detailed Indigenous Engagement Plan will be developed to formalise the following elements of Giga Metals' Engagement Strategy: Indigenous Group identification; participation in Technical Working Groups; in-person meetings; Open Houses; Notifications (including newsletters); documentation review; issues tracking and reporting; participation in assessments; and mechanisms for capacity building for both Giga Metals (including cultural awareness training) and indigenous groups.

As part of the project's environmental assessment, detailed Indigenous Knowledge and Traditional Land Use (TLU) studies will be completed in partnership with indigenous groups. Indigenous Knowledge studies completed previously for the project (e.g., Dena Kayeh Institute, 2010) will be updated as required. All archaeological and heritage assessments will be conducted in partnership with indigenous groups. Giga Metals will respect and work in partnership with indigenous groups to incorporate into baseline data, the environmental assessment, and mitigation and management plans any information provided by indigenous knowledge holders and keepers, land guardians, elders, and representatives.

Treaty 8 First Nations and the Métis Nation of BC may also be interested in the project. The project is located inside the Western boundary of Treaty 8 traditional territory, as recently determined by the BC Supreme Court (*West Moberly First Nations v. British Columbia*, 2017).

Figure 20-1 shows the Turnagain Project location in relation to this Western boundary of Treaty 8 traditional territory. Treaty 8 representatives participated as observers on the BC Muskwa-Kechika Advisory Board to which Giga Metals presented the project in October 2018.

20.3.1.1 Indigenous Consultation & Engagement Activities

Hard Creek Nickel Corporation first initiated engagement with the Tahltan Nation and Kaska Dena in 2004, during development of the preliminary environmental baseline program. Engagement since then has included in-person meetings, telephone calls, letters and email correspondence.

Giga Metals has entered into a Communications Agreement with the TCG that establishes a framework for communications with the Tahltan Nation, and is renewed annually. Giga Metals also has an Opportunities Sharing Agreement with the TCG that establishes a framework for communications and cooperation on employment, contracting and community opportunities. This agreement was transferred from Hard Creek Nickel Corporation to Giga Metals and was updated in April 2020.

In October 2008, the Daylu Dena Council, Dease River Band Council, Kwadacha First Nation and Kaska Dena Council, and Hard Creek Nickel Corporation entered into a Cornerstone Agreement that outlined the intentions and obligations of the parties regarding BC Kaska's initial participation in the Turnagain Project. The Cornerstone Agreement expired on December 31, 2010.

Hard Creek Nickel Corporation had previously entered into a Protocol with the Daylu Dena Council, Kaska Dena Council, Dease River Indian Band, Kwadacha First Nation, and the Dena Keyeh Institute (signed June 9, 2009) which included commitments by the parties regarding environmental protection, economic opportunities and benefits, Kaska knowledge, education and training. This Protocol expired when the Cornerstone Agreement expired.

Following the Cornerstone Agreement expiration, Giga Metals is negotiating an exploration agreement with Kaska Dena Council, with Dease River First Nation leading the negotiations on behalf of Kaska Dena Council. Giga Metals is maintaining a positive working relationship with the Dease River First Nation and the Kaska Dena Council.

Giga Metals has shared draft management plans with the Tahltan Nation and Kaska Dena for their review and input. For example, a draft Wildlife Mitigation Plan prepared by EDI on behalf of Giga Metals and an Archaeological Chance Find Procedure were provided to the Tahltan, Kaska Dena, and provincial government for review.

20.3.2 Local Communities

The closest community to the project is Dease Lake (unincorporated), which is a town of approximately 335 people (BC Census Data, 2016) located on Highway 37 at the south end of Dease Lake. Other local communities include Telegraph Creek, Iskut, and Good Hope Lake. There are no residences near the project property.

The cities of Terrace (population 15,700) and Smithers (population 10,600) are 580 km and 600 km to the south of Dease Lake, respectively.

Throughout the environmental assessment process, Giga Metals will engage with local and regional stakeholders interested in and potentially affected by the project. These will include local communities, local and regional governments, recreational organisations and users, community

groups, rights holders, utilities, and local and regional businesses. Giga Metals will solicit input on the project through project notifications, a project website, Open Houses, and in-person meetings.

20.4 Government Agencies Consultation & Engagement

Consultation and engagement with federal and provincial government agencies will continue during the environmental assessment process through to construction, operations and decommissioning. Table 20.1 provides a record of government consultations to date.

Table 20.1: Government & Stakeholder Consultation & Engagement Completed to Date

Government Organisation	Consultation Method(s)	Date	Summary
Impact Assessment Agency of Canada (formerly CEAA)	Presentation	May 2008 August 2018	Discussions regarding federal involvement in the project
BC Environmental Assessment Office	Presentation	November 2007 June 2018	Introductory project meetings. Inquiries about project guidance
BC Ministry of Energy, Mines and Petroleum Resources (MEM)	In-person meetings	2018 and 2019	Project discussions, and intent to enter the EA process for major projects
BC Ministry of Environment and Climate Change Strategy (MOE)	In-person meeting	March 2019	Introduction of the company and project.
BC Ministry of Forests, Lands, Natural Resource Operations and Rural Development (FLNRORD)	Telephone meetings	2018 and 2019	Permit discussions Indigenous Referral discussions
BC Muskwa-Kechika Advisory Board	Presentation in person	October 23, 2018	Introduction to Giga Metals and the Turnagain Project
Department of Fisheries and Oceans (DFO)	In-person meeting	January 2008	Discussions of best management practices, and the terms of reference and timeline for major projects.

20.5 Reclamation & Closure Plan

The main objective of closure is to minimise adverse environmental and social impacts associated with the mine development, and to return disturbed site areas to conditions consistent with an approved end-use plan.

Preliminary closure planning will be carried out concurrently with the various stages of project development and design in order to integrate the post-closure objectives into the design, construction, and operation of all mine infrastructure and facilities. The closure and reclamation plan will be developed in consultation with the project team, local stakeholders, and the appropriate regulatory authorities.

It is anticipated that the following objectives will be incorporated into the design of the project to facilitate an acceptable closure and reclamation plan:

- long-term stability of the embankments and other engineered structures, including the waste rock dump
- long-term preservation of water quality within and downstream of decommissioned operations
- construction of a spillway at the TMF
- construction of a protective berm or wildlife fence around the open pits
- removal and proper disposal of all access roads, pipelines, structures, and equipment not required beyond the end of mine life
- long-term stabilisation of all exposed erodible materials
- natural integration of disturbed lands into surrounding landscape, and restoration of the natural appearance of the area after mining ceases, to the extent possible
- establishment of a self-sustaining vegetative cover consistent with existing wildlife needs
- routine monitoring to evaluate facility performance

Groundwater monitoring wells and geotechnical instrumentation will be retained for long-term monitoring and performance assessment.

Post-closure requirements will include annual inspections of the TMF and waste rock dumps, and ongoing evaluation of water quality, flow rates, and instrumentation records to confirm the design assumptions adopted for closure.

Approximate bonding requirements for premature closure, final closure, and post-closure have been included in the capital cost estimate based on the objectives outlined above.

20.6 Greenhouse Gases (GHGs)

20.6.1 Sequestration of Carbon Dioxide with Mine Tailings

The host rocks of the Turnagain deposit contain a variety of minerals, such as olivine and serpentine, which are known to react with carbon dioxide (CO₂) under atmospheric conditions to sequester the greenhouse gas as mineral carbonates over geological timeframes. For individual minerals, the reaction rate is influenced by a variety of factors, including particle size (specific surface area), temperature, CO₂ pressure, moisture, and water chemistry. With the fine grinding of the Turnagain material for froth flotation and deposition of the tailings sub-aerially in a large tailings management facility, some level of carbonation is expected. At this time, insufficient information is available to quantify the expected sequestration, and no approved quantification protocol exists that would allow an economic valuation, but CO₂ sequestration by the TMF is expected to help achieve the goal of CO₂ neutrality in future years. The company is actively working on quantifying CO₂ sequestration rates through ongoing independent scientific research at the University of British Columbia by Dr. Greg Dipple, with an ultimate goal of better defining

the quantity of CO₂ that can be sequestered and the optimal tailings management strategies. Giga Metals will seek to develop a sequestration offset protocol under either regulatory (provincial or federal) or commercial (i.e., Canadian Standards Association, the Gold Standard, American Carbon Registry) standards. Demonstration of sequestration of significant quantities of CO₂ with appropriate management of the Turnagain mine tailings may also provide benefits through enhanced social acceptance of the project with local stakeholders, international stakeholders, and customers.

20.6.2 GHG Reduction Opportunity through Fleet Electrification

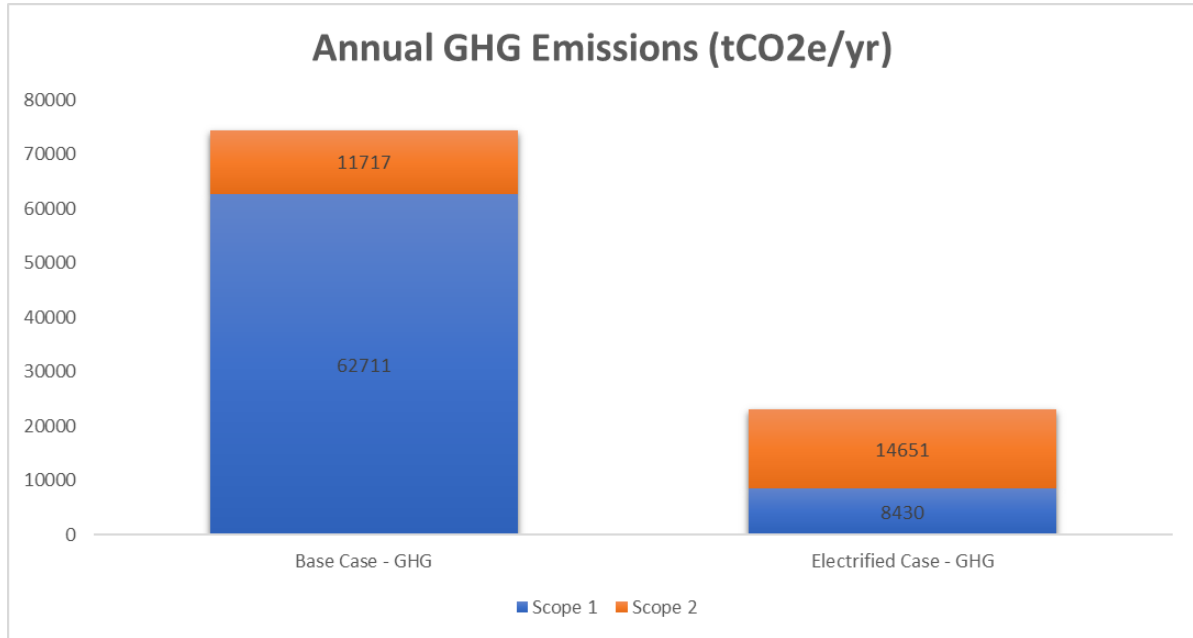
Based on the diesel and electricity consumption for mining and processing activities, the carbon intensity calculated for the operations is estimated to average 74,428 tCO₂e per year. Most of the emissions are direct emissions (scope 1) coming from diesel consumption of the mining fleet. There is an opportunity to reduce the carbon intensity through electrification of the mining fleet and shift the majority of the fleet emissions to indirect emissions (scope 2).

In an electrified fleet scenario, the model assumes that mining trucks and loaders would run on hydrogen, and the support fleet will be fully battery electric, based on technological feasibility, upcoming market offerings, and recognising the limitations of battery-only powertrains for such heavy duty applications.

These opportunities could result in reducing the carbon emissions to 23,080 tCO₂e per year. Most of the emissions for the electrification case would be indirect, coming from electricity generation from the BC grid, which has a grid emissions intensity factor of 12 tCO₂e/GWh based on the rolling average of the last three years for average emission factor (AEF) for BC electricity consumption. The average emission factors were published in Canada's National Inventory Report (NIR).

It should be noted that BC has published a different grid factor than the average emission factor for the integrated grid of 29.9 tCO₂e/GWh (British Columbia, 2020). The published factors, which are different than those used for public sector entities, are to be used by grid-connected entities in quantifying and the official reporting of GHG emissions of electricity which is not self-generated. Hatch has not confirmed with the authorities which emission factors should be used for GHG quantification. It is understood that some of the electricity consumed in BC can be purchased from less clean generation sources in other jurisdictions, which can greatly influence the grid emissions factor. If these neighbouring jurisdictions reduce their grid carbon intensity, it would be expected that the reporting differential would be reduced over time. Figure 20-2 shows the annual GHG emissions for both scenarios using the 12 tCO₂e/GWh grid factor from NIR. The average project carbon intensity is estimated to 2.24 tCO₂e/t Ni for the base case and 0.69 tCO₂e/t Ni for the electrified case.

Figure 20-2: GHG Reduction Opportunity through Fleet Electrification (tCO₂e per year)



Source: Hatch, 2000

21.0 CAPITAL & OPERATING COSTS

21.1 Capital Cost Estimate

The capital cost estimate is in the range of an AACE Class 5 Capital Cost Estimate with a targeted level of accuracy of +30 to +50% and -20% to -30%. All costs are provided in Q1 2020 US dollars. The initial and expansion capital is summarised in Table 21.1.

Table 21.1: Project Initial/Expansion Capital Cost Summary

Item	Units	Phase 1	Phase 2	Life of Mine
Mine Directs	US\$M	133	45	178
Process Plant Directs	US\$M	307	245	551
Tailings Storage Facility Directs	US\$M	87	20	107
On-site Infrastructure Directs	US\$M	77	-	77
Indirects	US\$M	204	104	308
Contingency	US\$M	191	99	290
Owner's Cost and EA	US\$M	63	20	83
Electrical Supply	US\$M	278	-	278
Site Access Road	US\$M	42	-	42
Total Initial/Expansion Capital	US\$M	1,381	532	1,913

The sustaining and closure and reclamation capital is summarised in Table 21.2.

Table 21.2: Project Sustaining Capital & Closure & Reclamation Cost Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mine	US\$M	0	348	148	496
Process Plant	US\$M	31	165	187	384
Tailings Storage Facility	US\$M	107	377	335	819
On-site Infrastructure	US\$M	8	23	26	57
Electrical Supply (Tariff Supplement 37)	US\$M	90	82	-	172
Total Sustaining Capital	US\$M	236	996	697	1,928
Closure and Reclamation	US\$M	38	15	18	72
Total	US\$M	274	1,011	715*	2,000

* Includes \$2.8M in TMF and closure costs in Year 38.

21.1.1 Mining

The summary for the mine capital costs is shown in Table 21.3 and Table 21.4.

Table 21.3: Mine Capital Cost Estimate

Item	Units	Phase 1	Phase 2	Life of Mine
Mining Equipment	US\$M	123	45	168
Mining Pre-production Costs	US\$M	9	-	9
Total	US\$M	133	45	178

Table 21.4: Mining Sustaining Cost Estimate

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mining Sustaining	US\$M	0	348	148	496

The cost for the initial mine equipment includes the fleet requirements to meet steady-state production in Year 2.

Most unit prices are based on Hatch internal and external benchmark data including recent budgetary pricing for the major production units. Equipment pricing is based on new units delivered to the mine, with transportation and erection costs included. Used equipment, if available, will reduce these equipment capital costs, and have not been considered for this study.

Pre-stripping will not be necessary, as the initial mineralisation feed will be near surface and accessible when the plant starts up. It is anticipated that land clearing and road access work will be performed by a mining contractor(s). Site preparation includes clearing and grubbing, site drainage, initial access roads, and the main haul road from the pit to the crusher. No detailed designs have been undertaken for this estimate.

A 10% factor of the support equipment fleet totals is included to account for ancillary items such as engineering supplies, light plants and pumps. A 5% critical spares factor was added to the initial equipment capital acquisitions.

21.1.2 On-Site Infrastructure & Process Plant

The on-site infrastructure and process plant direct capital costs are summarised in Table 21.5.

The concentrator capital cost estimate was prepared as a factored cost estimate based on a priced mechanical equipment list:

- Vendor budget prices provided 47% of the equipment costs.
- The remaining equipment was priced using Hatch database prices or factors to cover a percentage of minor equipment
- Earthworks, concrete, equipment support steel, pre-engineered buildings, piping, electrical and instrumentation/control costs were factored per area.

Infrastructure costs were taken from a recent similar project and allowances were made for some items.

Table 21.5: On-site Infrastructure & Process Plant Direct Capital Cost

Items	Units	Phase 1	Phase 2	Life of Mine
Truck Shop/ANFO Plant	US\$M	21	-	21
Site Infrastructure (Camp, Utilities, etc.)	US\$M	57	-	57
Direct On-site Infrastructure Capital Cost	US\$M	77	-	77
Crushing/HPGR/Conveyor	US\$M	133	77	210
Grinding/Flotation/Concentrate	US\$M	174	168	342
Direct Process Plant Capital Cost	US\$M	307	245	551

21.1.3 Off-Site Infrastructure

21.1.3.1 Electrical Power Line

Based on preliminary cost estimates, the 287 kV transmission line connection to BC Hydro, including the transmission line and substations, would require approximately US\$278 M in capital expenditure. The annual operating cost of Giga Metals' portion of the transmission line would be approximately US\$1.2 M/a. The operating costs include electrical losses as well as line and vegetation management.

BC Hydro's Tariff Supplement 37 requires customers connected to the NTL to pay a charge linearly scaled to their usage compared to the capacity of the line. The above capital cost is based on Tariff Supplement 37 costs being financed through BC Hydro with monthly payments over the first five years of Phases 1 and 2.

Electricity would be purchased from BC Hydro under Rate Schedule 1823 – Transmission Service – Stepped Rate, with a demand charge of C\$8.609/kVA and an energy charge of C\$50.47/MWh. The resulting blended rate is approximately C\$65/MWh (US\$51/MWh). The annual cost of electricity from BC Hydro is estimated at US\$56 M/a at full build-out. Refer to Table 21.6 and Table 21.7 for a summary of these costs.

Table 21.6: Electrical Supply Capital Cost

Electrical Supply	Units	Phase 1	Phase 2	Life of Mine
Transmission Line from Tatogga to Turnagain	US\$M	278	-	278
Tariff Supplement 6 Allowance	US\$M	-	-	-
Tariff Supplement 37	US\$M	90	82	172
Total	US\$M	368	82	450

Table 21.7: Electrical Supply Sustaining Capital Cost

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Electrical Supply (Tariff Supplement 37)	US\$M	90	82	-	172
Total	US\$M	90	82	-	172

21.1.3.2 Site Access Road

The project's contribution to the cost of the access road was estimated as a direct cost of approximately C\$500,000 per kilometre. No engineering was done for the access road. This should be reviewed in more detail in the next phase study.

21.1.4 Waste / Tailings Management Facilities (TMF)

The total initial capital costs associated with the TMF and other environmental management items are summarised in Table 21.8 and Table 21.9. The main components of the costs are listed by principal category in the following subsections.

Table 21.8: TMF Capital Costs

Item	Units	Phase 1	Phase 2	Life of Mine
Tailings Management Facility	US\$M	75	20	95
Water Management	US\$M	12	-	12
Direct	US\$M	87	20	107

Table 21.9: TMF Sustaining Capital & Closure & Reclamation Costs

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-38)	Life of Mine (Y1-38)
Tailings Storage Facility	US\$M	107	377	335	819
Closure and Reclamation	US\$M	38	15	18	72
Total	US\$M	145	392	353	891

21.1.4.1 TMF

Capital cost estimates have been completed for the following components of the TMF:

- earthworks and foundation preparation for the main (northwest) and saddle (southeast) dams
- tailings pipelines and fittings
- reclaim water system (including pipes and pumps)
- local roads for TMF access, construction, and borrow source development
- seepage control and sediment control for both dams

- geotechnical and hydrogeological instrumentation
- surface water diversions

Costs related to mitigating unmapped terrain hazards associated with debris flows, avalanches, major stream crossings, and other geo-hazards have not been considered in this estimate. A project contingency is included to account for unanticipated items.

21.1.4.2 Site-wide Water Supply & Water Management

Capital costs for site-wide water management include the following items:

- surface water diversion channels
- collection channels
- collection ponds
- transfer pipelines and pumps
- groundwater wells and pumps

21.1.4.3 Closure & Reclamation

Direct costs for closure and reclamation include the following items:

- TMF spillway
- building demolition and removal
- pipeworks removal
- re-sloping of waste rock dump
- rock and soil haulage and revegetation
- environmental monitoring during active reclamation

Indirect costs include:

- mobilisation and demobilisation
- agency administration
- site labour and management
- materials and service (power, insurance, etc.)
- engineering and specialist services

Annual post-closure operating expenses include:

- annual environmental monitoring
- annual site maintenance costs
- annual water treatment costs

The construction closure bond is estimated based on the closure costs at the end of the construction period, or the beginning of Year 1. An annual bond contribution for premature closure has been estimated based on expenses that would be incurred at the end of each successive five-year period following start-up, including an allowance for expenses that are incurred in perpetuity. A discount rate of 4.3% has been assumed for bonding cost calculations.

21.2 Operating Cost Estimate

The overall operating costs are summarised in unit cost terms in Table 21.10, which shows the life-of-mine costs as well as the costs during Years 1 to 5 at reduced throughput and Years 6 to 20 and 21 to 37 at full capacity.

Table 21.10: Unit Operating Cost Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mining	US\$/t milled	3.52	2.89	2.46	2.72
Processing & Site Infrastructure	US\$/t milled	4.90	4.39	4.38	4.42
G&A	US\$/t milled	1.13	0.68	0.68	0.71
Electrical Supply O&M	US\$/t milled	0.08	0.04	0.04	0.04
Total	US\$/t milled	9.63	7.99	7.56	7.89

21.2.1 Staffing Numbers

The Turnagain mine will be a fly-in/fly-out camp operation. Use of available local labour will be prioritised. Mine labour estimates are based on a four-crew rotation with management and technical staff on a two-crew rotation. The hourly labour workforce reflects estimated equipment hours and annual quantity of material mined. During the first five years of lower production, the total mine labour count averages 233; it then increases to an average of 324 during the peak period between Years 14 to 33. When the pit is completed and the mill is fed from the mineralisation stockpiles after Year 32, the mine labour force will be reduced significantly.

The mine staffing numbers developed in Section 16 are summarised in Table 21.11.

Table 21.11: Mine Operations Staffing – Average for Periods

Department	Years			
	1 to 5	6 to 13	14 to 33	34 to 37
Hourly Labour				
Mine Operations (hourly)	113	158	175	67
Mine Maintenance (hourly)	54	77	85	34
Subtotal	168	235	259	101
Salaried Staff – Mine & Maintenance Operations				
Senior Mine Management	4	4	4	2
Senior Maintenance Management	2	2	2	2
Mine & Maintenance General Foremen	4	4	4	0
Mine & Maintenance Foreman/Lead Hands	13	13	13	5
Mine & Maintenance Dispatch/Clerks/Planners	16	16	16	4
Subtotal	39	39	39	12
Mine Technical				
Supervisor/Senior Engineers & Geologists	6	6	6	1
Engineers & Geologists	4	4	4	1
Surveyors, Assayers, Helpers & Staff Coverage	16	16	16	3
Subtotal	26	26	26	5
Total Salaried Staff	65	65	65	17
Total Mine Workforce	233	300	324	118

Processing staffing numbers at full capacity are summarised in Table 21.12.

Table 21.12: Processing Staffing Numbers

Job Description	Hourly	Staff
Mill Operations Staff		7
Mill Maintenance Staff		9
Maintenance	40	
Electrical	10	
Milling - Operations	44	
Metallurgy		8
Assay Lab	6	
Total	100	24

21.2.2 Mining

The average mine operating cost is estimated to be US\$2.30 per tonne of material mined (including life-of-mine rehandling costs) or US\$2.72 per tonne milled over the life of mine. The cost estimate consists of all mining activities from the pit to the crusher pocket berm, and includes the waste and low-grade stockpile facilities. Table 21.13 shows the estimated operating costs for each of the areas.

Table 21.13: Mine Operating Cost Estimate

Item	Unit Cost (\$/t Mined)	Unit Cost (\$/t Milled)
Drilling	0.16	0.19
Blasting	0.22	0.26
Production Loading	0.14	0.16
Production Hauling	0.86	1.02
Pit Operations Support	0.16	0.19
Shop Equipment	0.02	0.03
Subtotal Cost Centre (excluding labour)	1.56	1.84
Mine Operations Labour	0.35	0.41
Operations Technical/Supervision Labour	0.11	0.12
Coverage & Training - Mine Department	0.06	0.07
Maintenance Labour	0.18	0.22
Maintenance Supervision Labour	0.02	0.02
Coverage & Training - Maintenance Department	0.03	0.03
Subtotal Cost Labour	0.74	0.87
Total (including rehandling costs)	2.30	2.72

Preliminary equipment productivities were generated and applied against the annual production quantities to estimate equipment operating hours. Consumption rates for consumables and unit operating costs were applied to the equipment hours to calculate the total equipment operating costs for each period. The cost of parts and repairs are included in the operating costs for the major mining equipment.

Operating costs fluctuate annually and reflect the total material mined and haulage distances. Balancing waste quantities and haulage destinations will smooth the operating costs and minimise fluctuation. Some smoothing was applied to the production schedule in this study.

The costs for power and diesel are \$.050/kWh and \$0.90/L, respectively. These unit prices are consistent with those assumed in other areas of operation. Mine operations power costs were calculated utilising the estimated kilowatt-hours for each year of operation of the production electrified equipment. Peak annual power consumption is estimated to be 34 million kilowatt-hours (MkWh), with the average being 27 MkWh/a during the high usage period between Years 14 to 25. Peak annual diesel consumption for explosives and the mine equipment fleet is estimated to be 32 ML, with the average being 24 ML during Years 14 to 25.

Explosives quantities were calculated using typical powder factors from existing operations and projects similar in nature. Recently attained explosives and accessories unit costs were applied to the projected quantities to estimate costs for blasting materials. Ammonium nitrate/fuel oil (ANFO) usage has been assumed to be 75%, based on successful dewatering to ensure dry blastholes most of the time. If dewatering is not successfully implemented, emulsion explosives usage and blasting costs will increase substantially.

Salaries and hourly labour rates are based on Hatch's internal data sources. The labour rates were applied to the operating and maintenance workforce generated from the equipment fleet to determine the total hourly labour cost. Salaries were applied to the total staff estimate to arrive at the salaried cost.

21.2.3 Concentrator

Concentrator operating costs are summarised in Table 21.14.

Table 21.14: Concentrator Operating Costs (Steady State)

Item	Units	Phase 1	Phase 2
Operation Labour	US\$/t milled	0.28	0.16
Maintenance Labour	US\$/t milled	0.27	0.15
Power	US\$/t milled	1.59	1.56
Heating (Propane)	US\$/t milled	0.13	0.09
Operating Consumables	US\$/t milled	2.11	2.11
Maintenance	US\$/t milled	0.31	0.27
G&A	US\$/t milled	1.05	0.68
Total	US\$/t milled	5.73	5.02

21.2.4 Off-site Charges

Apart from the smelter terms detailed in Section 19, other off-site charges include concentrate trucking and shipping, amounting to approximately US\$108/wmt plus insurance equal to 0.15% of freight value. The main components are trucking to Stewart at US\$62.50/wmt, port charges and sampling at US\$13.50/wmt and ocean freight at US\$30.00/wmt.

21.2.5 General & Administration (G&A) Costs

G&A costs were estimated at US\$22.2 million at full capacity based on a labour complement of 46 staff, including access road maintenance and crew transportation.

21.2.6 Tailings Management Facility

The estimated life-of-mine power operating cost for the tailings management facility is US\$53 million.

22.0 ECONOMIC ANALYSIS

22.1 Introduction

The preliminary economic assessment is preliminary in nature. It includes inferred mineral resources that are too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that the preliminary economic assessment will be realised.

The economic analysis is based on a discounted cash flow model. The model includes the life-of-mine production plan, operating costs, capital costs, and market assumptions discussed in this report, in addition to financial assumptions introduced in this section. Net present value (NPV), internal rate of return (IRR) and payback period are calculated in the model and reported before and after taxes.

Returns are highly sensitive to input assumptions and should be viewed in the context of the sensitivity analysis provided in this section.

22.2 Returns Summary

The PEA base case is based on the long-term nickel and cobalt prices of US\$7.50/lb Ni and US\$22.30/lb Co, as provided by Wood Mackenzie, and does not achieve a positive NPV at an 8% discount rate. The returns are shown in Table 22.1.

Table 22.1: Returns Summary

Item	Unit	PEA Base Case:
		Wood Mackenzie Long-Term Price US\$7.50/lb Ni
Pre-Tax NPV @ 8%	US\$M	(269)
Pre-Tax IRR	%	6.3%
Pre-Tax Payback	years	13.7
After-Tax NPV @ 8%	US\$M	(443)
After-Tax IRR	%	4.9%
After-Tax Payback	years	14.8
Ni Price	US\$/lb	7.50
Co Price	US\$/lb	22.30
Exchange Rate	USD/CAD	0.77

*Inverse of 1.30 CAD/USD applied.

The nickel price applied is the long-term average forecast by Wood Mackenzie. The PEA base case economic outputs are summarised in Table 22.2.

Table 22.2: PEA Base Case Key Economic Outputs

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	LOM
Project Economics					
NPV@ 8% Before Tax	US\$M	-	-	-	(269)
NPV@ 8% After Tax	US\$M	-	-	-	(443)
IRR Before Tax	%	-	-	-	6.3%
IRR After Tax	%	-	-	-	4.9%
Payback Period Before Tax	years	-	-	-	13.7
Payback Period After Tax	years	-	-	-	14.8
Market Drivers					
Nickel Price	US\$/lb	7.50	7.50	7.50	7.50
Cobalt Price	US\$/lb	22.30	22.30	22.30	22.30
Exchange Rate	USD/CAD	0.77	0.77	0.77	0.77
Nickel Payable %	%	78%	78%	78%	78%
Cobalt Payable %	%	35%	35%	35%	35%
Physicals					
Effective Strip Ratio (incl. stockpile)	t:t	0.50	0.56	0.24	0.40
Mill Throughput: Annual Average	Mt/a	15.3	32.7	32.6	30.3
Nickel Head Grade	%	0.260%	0.220%	0.216%	0.221%
Cobalt Head Grade	%	0.016%	0.013%	0.013%	0.013%
Recovery: Nickel and Cobalt	%	57.3%	51.6%	46.5%	49.6%
Nickel Recovered	kt	114	557	558	1,229
Cobalt Recovered	kt	7	33	32	73
Financial					
Revenue	US\$M/a	317	517	456	462
Mining Cost	US\$/t milled	3.52	2.89	2.46	2.72
Processing and Site infrastructure	US\$/t milled	4.90	4.39	4.38	4.42
G&A	US\$/t milled	1.13	0.68	0.68	0.71
Electrical Supply O&M	US\$/t milled	0.08	0.04	0.04	0.04
Site Operating Costs	US\$/t milled	9.63	7.99	7.56	7.89
Site Operating Costs	US\$/lb Ni recovered	2.93	3.20	3.41	3.27
Concentrate Shipping	US\$/lb Ni recovered	0.31	0.31	0.31	0.31
Cobalt Credit	US\$/lb Ni recovered	(0.47)	(0.47)	(0.45)	(0.46)
Net Operating Cost	US\$/lb Ni recovered	2.77	3.04	3.27	3.12
Construction Capital Cost	US\$M	1,381	532	-	1,913
Sustaining Capital & Closure Cost	US\$M	274	1,011	715	2,000

22.3 PEA Base Case Assumptions & Inputs

22.3.1 General

The following general assumptions and criteria form part of this analysis:

- real 2020 US Dollars; no inflation applied
- costs in Canadian dollars converted to US dollars at a 1.30 CAD/USD exchange rate, equivalent to ~0.77 USD/CAD
- three-year Phase 1 construction period from Year -3 through Year -1, and a two-year Phase 2 construction period in Years 4 and Year 5
- mid-year discounting for NPV calculation
- 100% equity financing

22.3.2 Nickel & Cobalt Pricing

Wood Mackenzie's long-term prices of US\$7.50/lb Ni and US\$22.30/lb Co have been applied.

22.3.3 Ore Production & Processing

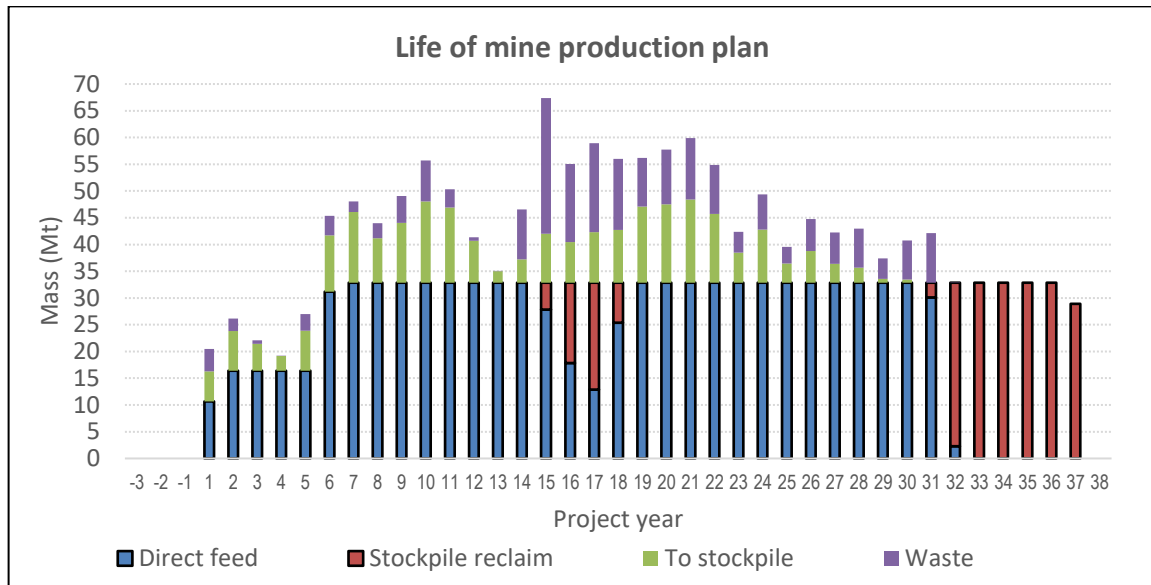
Average production statistics for Phase 1, Phase 2, and the life of mine are shown in Table 22.3.

Table 22.3: Average Production Statistics

Item	Unit	Phase 1 Operation (Y1-5)	Phase 2 Operation (Y6-20)	Phase 2 Operation (Y21-37)	LOM
Phase Duration	years	5	15	17	37
Material Mined	Mt	115	719	496	1,330
Material Moved	Mt	115	767	689	1,571
Effective Strip Ratio (incl. stockpile)	t:t	0.50	0.56	0.24	0.40
Ore Processed	Mt	76	491	554	1,122
Ore Processed (Annual)	Mt/a	15.3	32.7	32.6	30.3
Nickel Head Grade	%	0.260%	0.220%	0.216%	0.221%
Cobalt Head Grade	%	0.016%	0.013%	0.013%	0.013%
Recovery: Nickel and Cobalt	%	57.3%	51.6%	46.5%	49.6%
Nickel Contained	kt	199	1,080	1,200	2,479
Nickel Recovered	kt	114	557	558	1,229
Nickel Payable	kt	89	435	435	959
Cobalt Contained	kt	12	65	70	146
Cobalt Recovered	kt	7	33	32	73
Cobalt Payable	kt	2	12	11	25
Concentrate Produced	k dmt	632	3,096	3,100	6,828
Concentrate Produced	k dmt/a.	126	206	182	185
Concentrate Nickel Grade	%	18.0%	18.0%	18.0%	18.0%
Concentrate Cobalt Grade	%	1.09%	1.08%	1.04%	1.06%
Concentrate Moisture Content	%	9.0%	9.0%	9.0%	9.0%

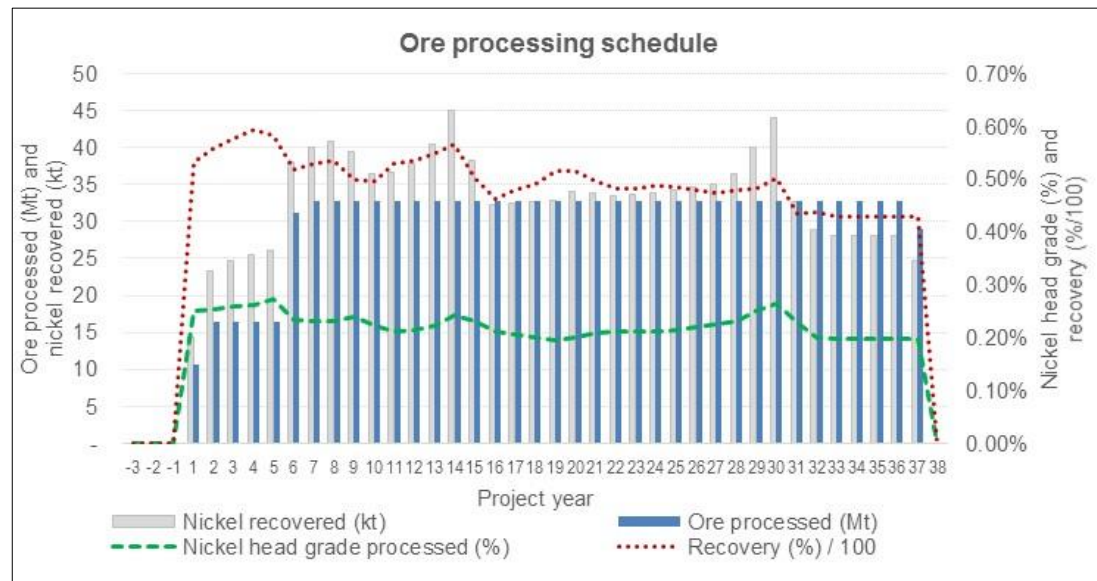
The life of mine production plan applied in the model from Section 16 is shown in Figure 22-1. The mill processing schedule applied in the model corresponding to the life of mine plan is shown in Figure 22-2.

Figure 22-1: Life-of-Mine Production Plan



Source: Hatch, 2020.

Figure 22-2: Mill Processing Schedule



Source: Hatch, 2020.

22.3.4 Concentrate Terms & Transportation Costs

The concentrate terms and transportation costs applied in the model are shown in Table 22.4. The concentrate terms are based on Wood Mackenzie's knowledge of nickel concentrate treatment via smelting and refining to Class I nickel. Nickel processing advancements in the nickel intermediate market (mixed sulphides, mixed hydroxides and higher-grade concentrates) may impact future terms. Section 19 states that current terms for nickel concentrates indicate 78% payability for nickel and 35% payability for cobalt (if above 0.3% in the concentrate). These payables are applied in the PEA base case. Copper payables are not applied as copper is not included in the PEA life-of-mine plan. The copper contribution to revenue would be marginal.

Table 22.4: Concentrate Terms & Transportation Costs

Item	Unit	Applied	Notes
Nickel Payable	%	78%	Source: Wood Mackenzie
Cobalt Payable	%	35%	Source: Wood Mackenzie. Applied above 0.3% Co grade
Treatment Charges	US\$/dmt	-	Part of payable deductions
Concentrate Transportation	US\$/wmt	112.66	China port
Trucking	US\$/wmt	62.50	Source: Hatch
Port Charges	US\$/wmt	15.38	Source: Hatch
Ocean Freight	US\$/wmt	30.00	Source: Hatch
Insurance	% of value	0.15%	Source: Giga Metals

22.3.5 Site Operating Costs

The average unit operating costs in the model are shown in Table 22.5.

Table 22.5: Site Operating Cost per Tonne of Mill Feed Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	LOM
Mining	US\$/t milled	3.52	2.89	2.46	2.72
Processing & Site Infrastructure*	US\$/t milled	4.90	4.39	4.38	4.42
Site Level G&A	US\$/t milled	1.13	0.68	0.68	0.71
Electrical Supply O&M	US\$/t milled	0.08	0.04	0.04	0.04
Total Site Operating Cost	US\$/t milled	9.63	7.99	7.56	7.89

*Includes tailings electricity costs.

22.3.6 Capital Costs

The construction capital costs from Section 21 applied in the model are shown in Table 22.6. The Phase 1 initial capital costs occur over three years from Year -3 to Year -1. The Phase 2 expansion capital costs occur from Year 4 to Year 5.

Table 22.6: Project Initial/Expansion Capital Cost Summary

Item	Units	Phase 1	Phase 2	Life of Mine
Mine Directs	US\$M	133	45	178
Process Plant Directs	US\$M	307	245	551
Tailings Storage Facility Directs	US\$M	87	20	107
On-site Infrastructure Directs	US\$M	77	-	77
Indirects	US\$M	204	104	308
Contingency	US\$M	191	99	290
Owner's Cost and EA	US\$M	63	20	83
Electrical Supply	US\$M	278	-	278
Site Access Road	US\$M	42	-	42
Total Initial/Expansion Capital	US\$M	1,381	532	1,913

Project sustaining capital costs, as well as closure and reclamation costs, are summarised in Table 22.7. Closure and reclamation costs correspond to the incremental growth of the reclamation liability for each period under a bonding scenario.

Table 22.7: Project Sustaining Capital & Closure & Reclamation Cost Summary

Item	Units	Phase 1 (Y1-5)	Phase 2 (Y6-20)	Phase 2 (Y21-37)	Life of Mine (Y1-37)
Mine	US\$M	0	348	148	496
Process Plant	US\$M	31	165	187	384
Tailings Storage Facility	US\$M	107	377	335	819
On-site Infrastructure	US\$M	8	23	26	57
Electrical Supply (Tariff Supplement 37)	US\$M	90	82	-	172
Total Sustaining Capital	US\$M	236	996	697	1,928
Closure and Reclamation	US\$M	38	15	18	72
Total	US\$M	274	1,011	715*	2,000

*Includes \$2.8 M in TMF and closure costs in Year 38.

22.3.7 Royalties

The following royalties are applied:

- Conic Metals royalty equal to 2% of net smelter return (NSR) for the life of mine
- Giga Metals buyout of the Schussler-Hatzl royalty discussed in Section 4 of this report: C\$4.0 M (US\$3.1 M) in Year 1

22.3.8 Taxes

Preliminary tax calculations are appropriate at the PEA stage and are applied at the project level. The BC mineral tax and federal and provincial corporate taxes are applied.

The BC mineral tax includes a 2% tax on net current proceeds and a 13% tax on net revenues after the current expenditures account balance becomes positive. An investment allowance rate based on the Bank of Canada rate is applied on the current expenditures account.

Federal and provincial corporate taxes are based on a 15% federal and 12% provincial tax rate. Capital cost allowance (CCA) Class 41 depreciation at 25% is applied and tax losses are carried forward.

The company's tax advisors reviewed the model tax calculation at a high level and did not identify any additional material tax deductions appropriate for a PEA level analysis, including the company's existing tax pools, which are not applied.

22.3.9 Working Capital

Working capital is based on 90 days of accounts receivable, 60 days of accounts payable, and 30 days of inventory. Working capital is reflected in the cash flow as changes in net working capital.

22.4 Cash Flow

22.4.1 Annual Cash Flow Summary

Tables 22.8 and 22.9 show the cash flow summary for the PEA base case.

Table 22.9: PEA Base Case Cash Flow Summary – Years 30 to 38

Item	Units	LOM	30	31	32	33	34	35	36	37	38
Prices											
Nickel Price	US\$/lb	7.50	7.50	7.50	7.50	7.50	7.50	7.50	7.50	7.50	7.50
Cobalt Price	US\$/lb	22.30	22.30	22.30	22.30	22.30	22.30	22.30	22.30	22.30	22.30
USD/CAD Exchange Rate	USD/CAD	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77	0.77
Physicals											
Material Mined	Mt	1,330	40.7	39.4	2.3	-	-	-	-	-	-
Effective Strip Ratio (incl. stockpile)	t:t	0.40	0.24	0.28	0.00	-	-	-	-	-	-
Ore Processed	Mt	1,122	32.9	32.9	32.9	32.9	32.9	32.9	32.9	28.9	-
Nickel Grade	%	0.221%	0.266%	0.230%	0.201%	0.199%	0.199%	0.199%	0.199%	0.199%	-
Recovery	%	49.6%	50.3%	43.4%	43.8%	43.0%	43.0%	43.0%	43.0%	43.0%	-
Nickel Payable %	%	78.0%	78.0%	78.0%	78.0%	78.0%	78.0%	78.0%	78.0%	78.0%	-
Nickel Payable	Mlbs	2,113	75.7	56.3	49.7	48.2	48.2	48.2	48.2	42.4	-
Cobalt Grade	%	0.013%	0.015%	0.014%	0.012%	0.012%	0.012%	0.012%	0.012%	0.012%	-
Recovery	%	49.6%	50.3%	43.4%	43.8%	43.0%	43.0%	43.0%	43.0%	43.0%	-
Cobalt Payable %	%	35%	35%	35%	35%	35%	35%	35%	35%	35%	-
Cobalt Payable	Mlbs	56	1.9	1.5	1.3	1.3	1.3	1.3	1.3	1.1	-
Concentrate Produced	k dmt	6,828	245	182	161	156	156	156	156	137	-
Concentrate Produced	k wmt	7,503	269	200	176	171	171	171	171	151	-
Cash Flow											
Nickel Revenue	US\$M	15,850	567.8	422.3	372.7	361.8	361.8	361.8	361.8	318.2	-
Cobalt Revenue	US\$M	1,249	41.9	33.5	29.8	28.9	28.9	28.9	28.9	25.4	-
Revenue Total	US\$M	17,099	609.7	455.8	402.5	390.7	390.7	390.7	390.7	343.6	-
Treatment & Refining	US\$M	-	-	-	-	-	-	-	-	-	-
Concentrate Transportation	US\$M	(845)	(30.3)	(22.5)	(19.9)	(19.3)	(19.3)	(19.3)	(19.3)	(17.0)	-
Net Smelter Return (NSR)	US\$M	16,254	579.4	433.2	382.6	371.4	371.4	371.4	371.4	326.7	-
Conic Metals Royalty	US\$M	(325)	(11.6)	(8.7)	(7.7)	(7.4)	(7.4)	(7.4)	(7.4)	(6.5)	-
Operating Costs	US\$M	(8,852)	(278.2)	(264.8)	(215.0)	(209.4)	(205.7)	(204.8)	(204.8)	(188.3)	-
Mining	US\$M	(3,048)	(111.1)	(97.8)	(48.0)	(42.4)	(38.8)	(37.9)	(37.9)	(34.8)	-
Processing & Site Infrastructure	US\$M	(4,962)	(143.6)	(143.6)	(143.6)	(143.6)	(143.6)	(143.5)	(143.5)	(130.1)	-
G&A	US\$M	(797)	(22.2)	(22.2)	(22.2)	(22.2)	(22.2)	(22.2)	(22.2)	(22.2)	-
Electrical Supply O&M	US\$M	(45)	(1.2)	(1.2)	(1.2)	(1.2)	(1.2)	(1.2)	(1.2)	(1.2)	-
EBITDA	US\$M	7,077	289.6	159.8	160.0	154.6	158.2	159.2	159.2	131.9	-
Changes in Net Working Capital	US\$M	-	(12.3)	36.9	9.0	2.4	(0.3)	(0.1)	(0.0)	10.2	69.3
Phase 1 Initial Capital Cost	US\$M	(1,381)	-	-	-	-	-	-	-	-	-
Phase 2 Expansion Capital Cost	US\$M	(532)	-	-	-	-	-	-	-	-	-
Sustaining Capital Cost	US\$M	(1,928)	(48.7)	(41.0)	(31.5)	(30.5)	(14.6)	(22.5)	(14.4)	(14.4)	(1.8)
Closure & Reclamation	US\$M	(72)	(1.0)	(1.0)	(1.0)	(1.0)	(1.0)	(1.0)	(1.0)	(1.0)	(1.0)
Schussler-Hatzl Royalty Buyout	US\$M	(3)	-	-	-	-	-	-	-	-	-
Pre-Tax Cash Flow	US\$M	3,161	227.6	154.5	136.5	125.5	142.4	135.6	143.8	126.7	66.4
BC Mineral Tax	US\$M	(372)	(32.7)	(16.4)	(17.6)	(17.0)	(19.5)	(18.6)	(19.7)	(16.0)	-
Corporate Tax	US\$M	(779)	(54.1)	(24.1)	(25.0)	(24.9)	(26.7)	(28.6)	(29.3)	(24.0)	-
After-Tax Cash Flow	US\$M	2,010	140.8	114.0	93.9	83.6	96.2	88.4	94.8	86.7	66.4

22.4.2 Unit Cash Flow Summary

Table 22.10 summarises the life-of-mine cash flow on a unit basis in terms of US\$/t mill feed and US\$/lb of payable nickel.

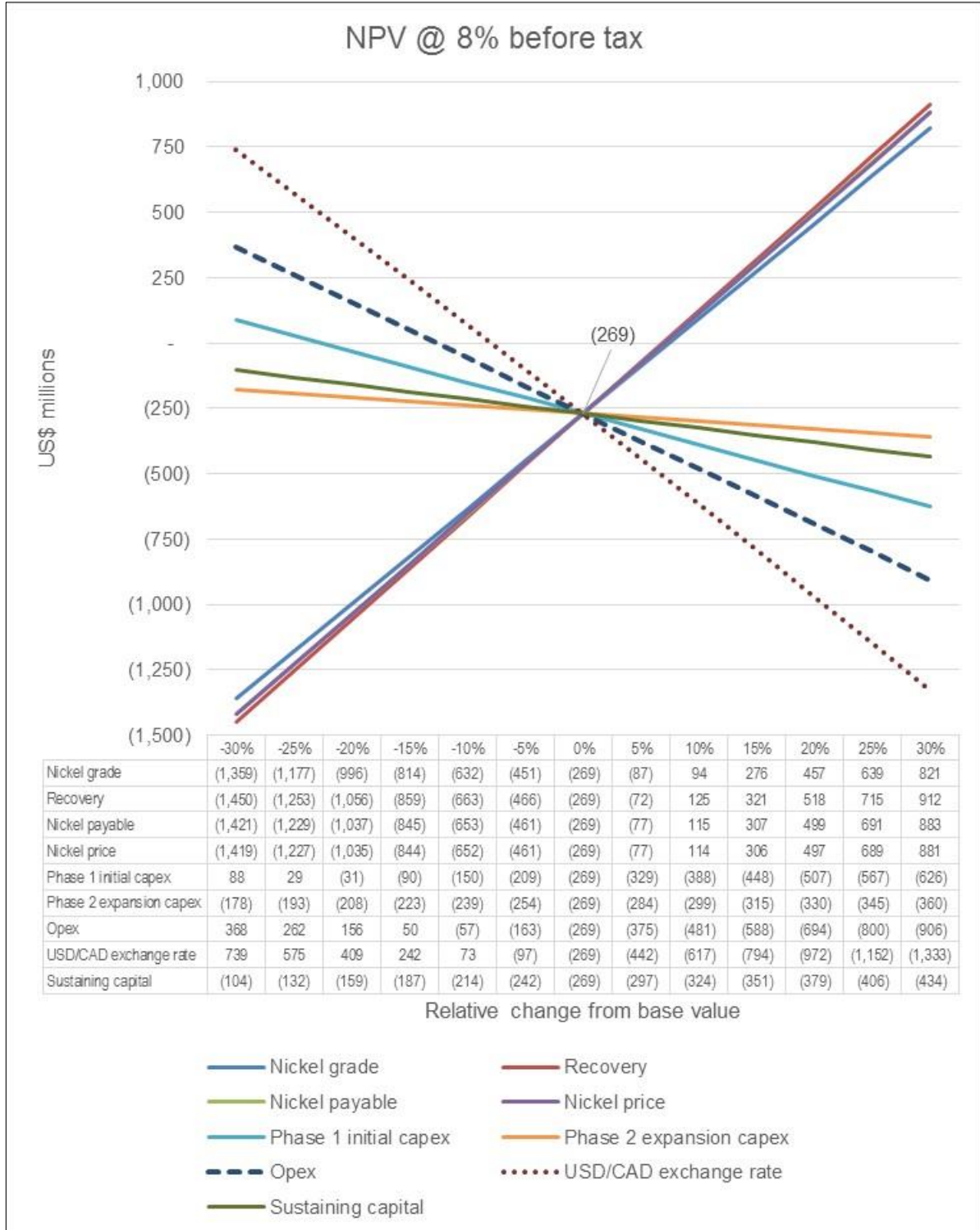
Table 22.10: Unit Cash Flow Summary

Item	US\$/t Milled	US\$/lb Ni Payable	LOM US\$M
Nickel Revenue	14.13	7.50	15,850
Cobalt Revenue	1.11	0.59	1,249
Total Revenue	15.24	8.09	17,099
Treatment & Refining	-	-	-
Concentrate Transportation	(0.75)	(0.40)	(845)
Net Smelter Return (NSR)	14.49	7.69	16,254
Conic Metals Royalty	(0.29)	(0.15)	(325)
Mining Operating Cost	(2.72)	(1.44)	(3,048)
Processing & Site Infrastructure Operating Cost	(4.42)	(2.35)	(4,962)
Site Level G&A	(0.71)	(0.38)	(797)
Electrical Supply O&M	(0.04)	(0.02)	(45)
EBITDA	6.31	3.35	7,077
Phase 1 Initial Capital	(1.23)	(0.65)	(1,381)
Phase 2 Expansion Capital	(0.47)	(0.25)	(532)
Sustaining Capital	(1.72)	(0.91)	(1,928)
Closure & Reclamation Costs	(0.06)	(0.03)	(72)
Schussler-Hatzl Royalty Buyout	(0.00)	(0.00)	(3)
Pre-Tax Cash Flow	2.82	1.50	3,161
BC Mineral Tax	(0.33)	(0.18)	(372)
Corporate Tax	(0.69)	(0.37)	(779)
After-Tax Cash Flow	1.79	0.95	2,010
<i>C1 Cost (Excluding Royalty)</i>		4.00	

22.5 Sensitivity Analysis

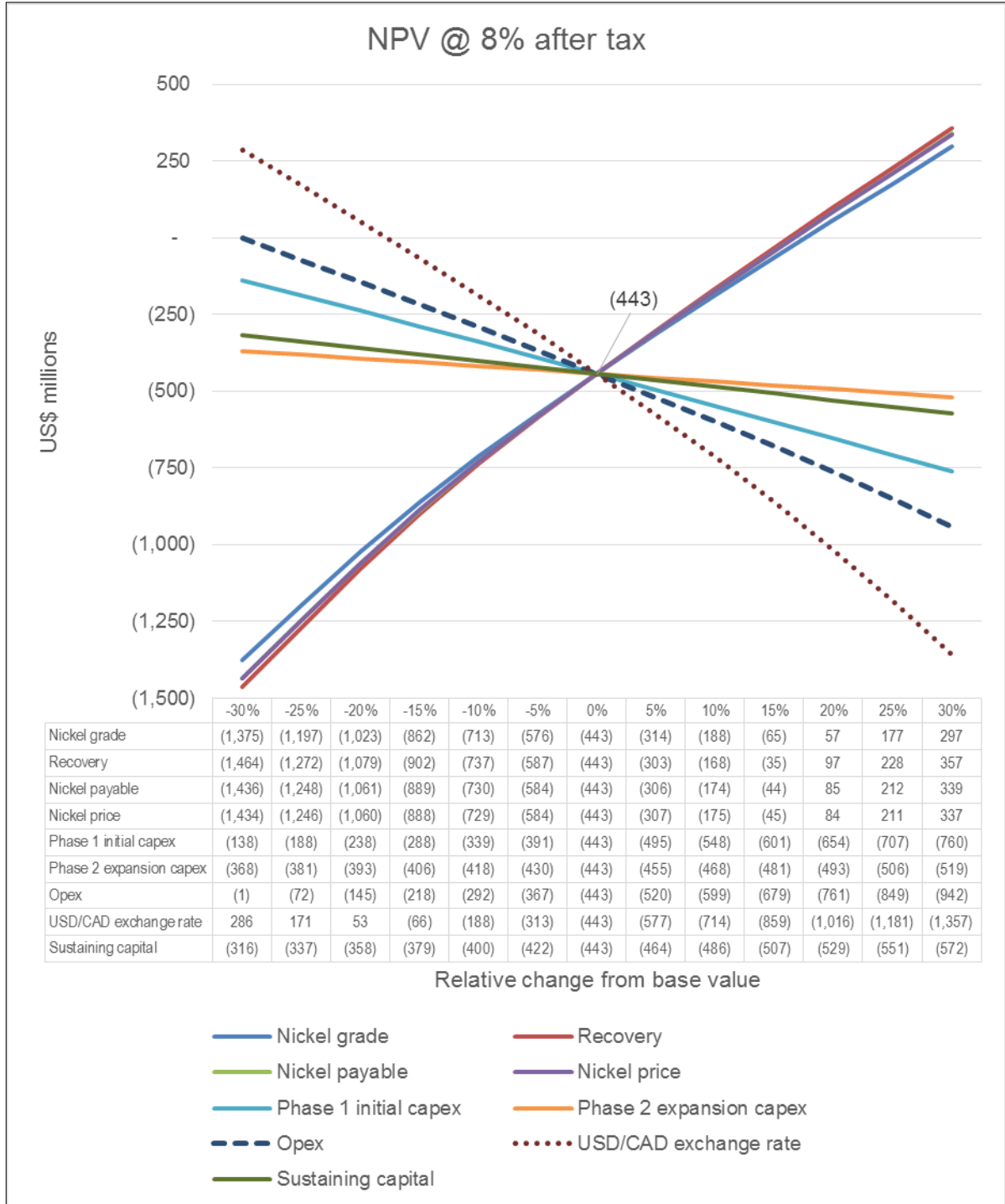
A sensitivity analysis was performed to identify key variables with significant impacts on project returns. The nickel price, exchange rate, nickel payable percent, nickel grade, recovery, capital costs, and operating costs were each varied independently on an annual basis and the resulting NPV @ 8% and IRR are shown in Figures 22-3 through 22-6 before and after taxes. The parameter ranges shown do not represent the range limits for each parameter. NPV is most sensitive to recovery, nickel payable percent, nickel price, nickel grade, and exchange rate.

Figure 22-3: NPV Pre-Tax @ 8% Sensitivity



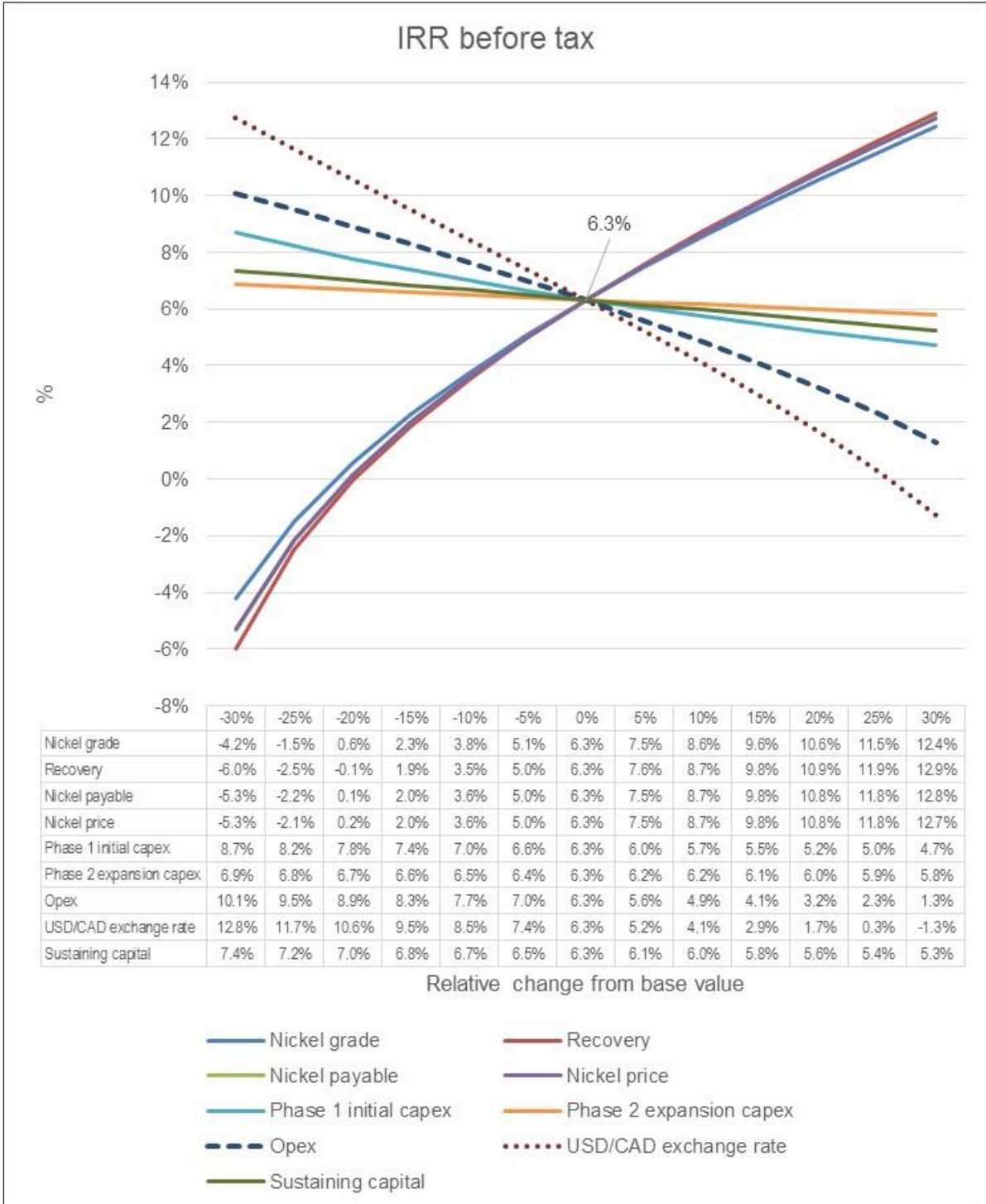
Source: Hatch, 2020.

Figure 22-4: NPV After-Tax @ 8% Sensitivity



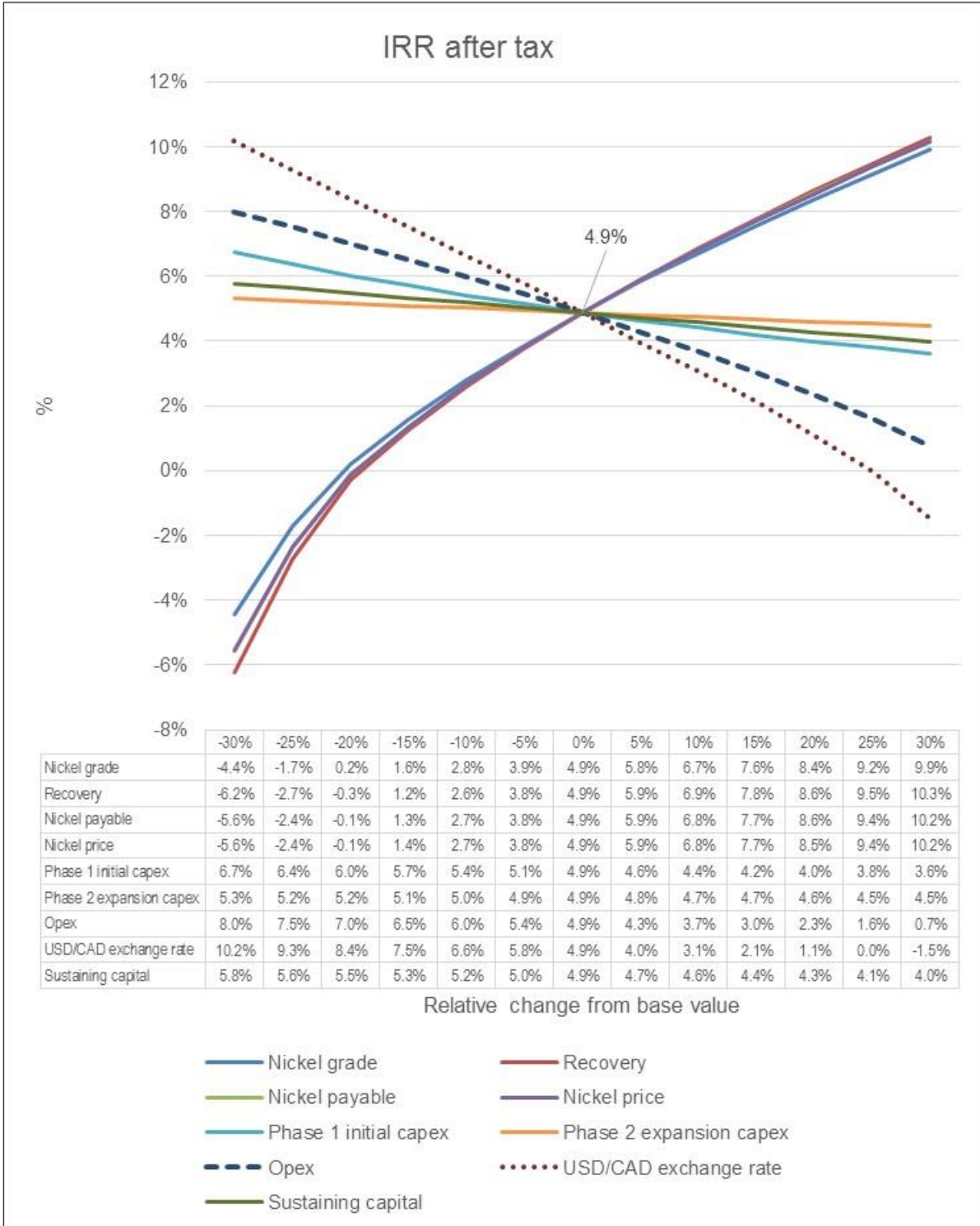
Source: Hatch, 2020.

Figure 22-5: IRR Pre-Tax Sensitivity



Source: Hatch, 2020.

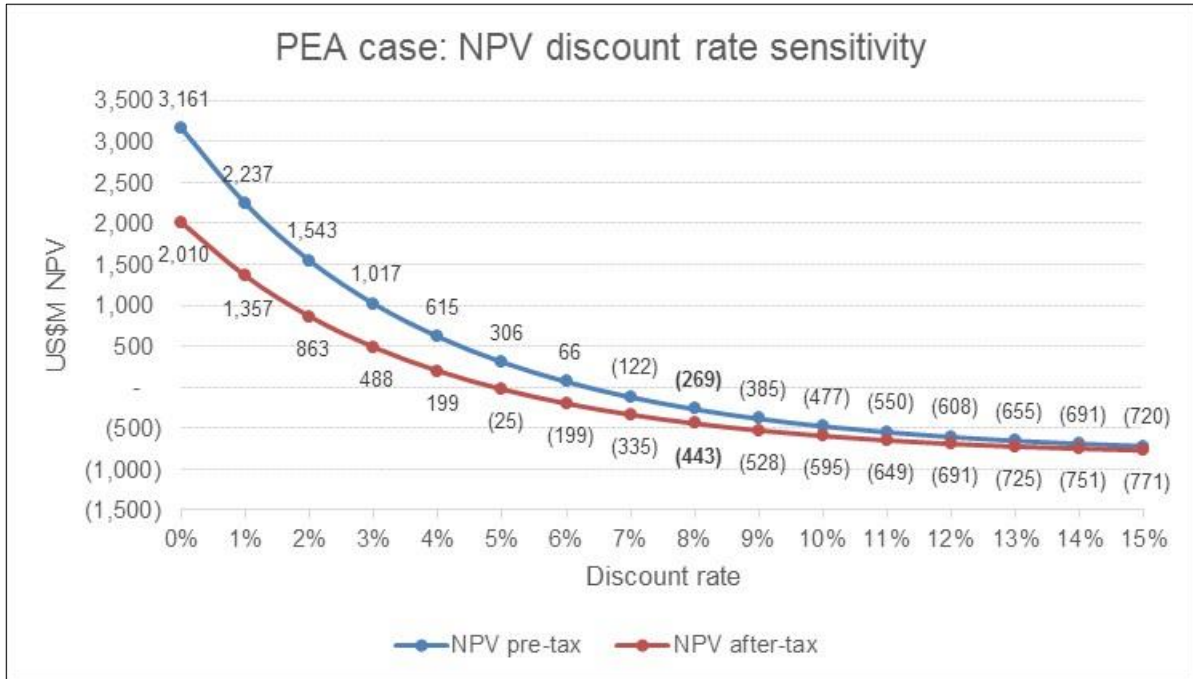
Figure 22-6: IRR After-Tax Sensitivity



Source: Hatch, 2020.

The NPV sensitivity to discount rate is shown in Figure 22-7.

Figure 22-7: NPV Discount Rate Sensitivity



Source: Hatch, 2020.

Tables 22.11 and 22.12 summarise the sensitivity of NPV @ 8% before and after taxes to changes nickel prices and USD/CAD exchange rate. The green shaded cell is at current PEA base case pricing.

Table 22.13 and Table 22.14 show the same sensitivity tables as above in terms of pre-tax and after-tax IRR.

Table 22.15 and Table 22.16 summarise the sensitivity of NPV @ 8% before and after taxes to changes in nickel price and nickel payables. The market study recommends a downside nickel payable sensitivity from 68% to 75%. The green shaded cells are current PEA base case pricing.

Table 22.17 and Table 22.18 show the same sensitivity tables as above in terms of pre-tax and after-tax IRR.

Table 22.11: NPV Pre-Tax @ 8% Sensitivity to Nickel Price & USD/CAD Exchange Rate

NPV Pre-Tax (US\$M)		Nickel Price - Flat (US\$/lb)										
USD/CAD Exchange Rate		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	0.70	(727)	(472)	(216)	39	295	550	806	1,061	1,317	1,572	1,828
	0.71	(771)	(516)	(260)	(5)	251	506	762	1,017	1,273	1,528	1,784
	0.72	(816)	(560)	(305)	(49)	206	462	717	973	1,228	1,484	1,739
	0.73	(860)	(605)	(349)	(94)	162	417	673	928	1,184	1,439	1,695
	0.74	(905)	(649)	(394)	(138)	117	373	628	884	1,139	1,395	1,650
	0.75	(949)	(694)	(438)	(183)	73	328	584	839	1,095	1,350	1,606
	0.76	(994)	(739)	(483)	(228)	28	283	539	794	1,050	1,305	1,561
	0.77*	(1,035)	(780)	(525)	(269)	(14)	242	497	753	1,008	1,264	1,519
	0.78	(1,084)	(828)	(573)	(317)	(62)	194	449	705	960	1,216	1,471
0.79	(1,129)	(873)	(618)	(362)	(107)	148	404	659	915	1,170	1,426	
0.80	(1,174)	(919)	(663)	(408)	(152)	103	359	614	870	1,125	1,381	

Notes: *Inverse of 1.30 CAD/USD applied. Colour legend: PEA base case price

Table 22.12: NPV After-Tax @ 8% Sensitivity to Nickel Price & USD/CAD Exchange Rate

NPV After-Tax (US\$M)		Nickel Price - Flat (US\$/lb)										
USD/CAD Exchange Rate		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	0.70	(780)	(580)	(392)	(213)	(39)	132	300	468	634	799	963
	0.71	(819)	(615)	(426)	(245)	(71)	100	269	437	604	769	933
	0.72	(858)	(650)	(460)	(278)	(103)	69	238	407	573	739	903
	0.73	(898)	(686)	(494)	(311)	(135)	37	207	376	542	708	873
	0.74	(939)	(722)	(529)	(344)	(167)	5	176	345	512	678	843
	0.75	(980)	(759)	(564)	(378)	(199)	(26)	145	313	481	647	812
	0.76	(1,021)	(797)	(599)	(411)	(232)	(58)	113	282	450	616	782
	0.77*	(1,060)	(833)	(631)	(443)	(262)	(88)	84	253	421	588	753
	0.78	(1,106)	(876)	(670)	(480)	(298)	(123)	49	219	388	554	720
0.79	(1,151)	(916)	(706)	(515)	(331)	(155)	17	187	356	523	689	
0.80	(1,195)	(957)	(742)	(550)	(365)	(188)	(15)	156	324	492	658	

Notes: *Inverse of 1.30 CAD/USD applied. Colour legend: PEA base case price.

Table 22.13: IRR Pre-Tax Sensitivity to Nickel Price & USD/CAD Exchange Rate

IRR Pre-Tax (%)		Nickel Price - Flat (US\$/lb)										
USD/CAD Exchange Rate		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	0.70	2.7%	4.8%	6.6%	8.2%	9.8%	11.2%	12.6%	13.9%	15.1%	16.3%	17.5%
	0.71	2.4%	4.5%	6.3%	8.0%	9.5%	10.9%	12.3%	13.6%	14.9%	16.1%	17.3%
	0.72	2.0%	4.2%	6.0%	7.7%	9.2%	10.7%	12.1%	13.4%	14.6%	15.8%	17.0%
	0.73	1.7%	3.8%	5.7%	7.4%	9.0%	10.4%	11.8%	13.1%	14.4%	15.6%	16.7%
	0.74	1.3%	3.5%	5.4%	7.1%	8.7%	10.2%	11.5%	12.8%	14.1%	15.3%	16.5%
	0.75	0.9%	3.2%	5.1%	6.9%	8.4%	9.9%	11.3%	12.6%	13.9%	15.1%	16.2%
	0.76	0.5%	2.9%	4.8%	6.6%	8.2%	9.6%	11.0%	12.3%	13.6%	14.8%	16.0%
	0.77*	0.2%	2.6%	4.6%	6.3%	7.9%	9.4%	10.8%	12.1%	13.4%	14.6%	15.7%
	0.78	-0.3%	2.2%	4.2%	6.0%	7.6%	9.1%	10.5%	11.8%	13.1%	14.3%	15.5%
0.79	-0.7%	1.9%	3.9%	5.7%	7.4%	8.9%	10.3%	11.6%	12.8%	14.1%	15.2%	
0.80	-1.2%	1.5%	3.6%	5.5%	7.1%	8.6%	10.0%	11.3%	12.6%	13.8%	15.0%	

Notes: *Inverse of 1.30 CAD/USD applied. Colour legend: **PEA base case price**

Table 22.14: IRR After-Tax Sensitivity to Nickel Price & USD/CAD Exchange Rate

IRR After-Tax (%)		Nickel Price - Flat (US\$/lb)										
USD/CAD Exchange Rate		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	0.70	1.9%	3.6%	5.1%	6.5%	7.7%	8.9%	10.0%	11.1%	12.1%	13.1%	14.0%
	0.71	1.7%	3.4%	4.9%	6.2%	7.5%	8.7%	9.8%	10.9%	11.9%	12.9%	13.8%
	0.72	1.4%	3.1%	4.6%	6.0%	7.3%	8.5%	9.6%	10.7%	11.7%	12.7%	13.6%
	0.73	1.1%	2.9%	4.4%	5.8%	7.1%	8.3%	9.4%	10.5%	11.5%	12.5%	13.4%
	0.74	0.8%	2.6%	4.1%	5.6%	6.8%	8.0%	9.2%	10.2%	11.3%	12.3%	13.2%
	0.75	0.5%	2.3%	3.9%	5.3%	6.6%	7.8%	9.0%	10.0%	11.1%	12.0%	13.0%
	0.76	0.2%	2.1%	3.7%	5.1%	6.4%	7.6%	8.7%	9.8%	10.9%	11.8%	12.8%
	0.77*	-0.1%	1.8%	3.4%	4.9%	6.2%	7.4%	8.5%	9.6%	10.7%	11.6%	12.6%
	0.78	-0.5%	1.5%	3.2%	4.6%	6.0%	7.2%	8.3%	9.4%	10.4%	11.4%	12.4%
0.79	-0.9%	1.2%	2.9%	4.4%	5.7%	7.0%	8.1%	9.2%	10.2%	11.2%	12.2%	
0.80	-1.4%	0.9%	2.7%	4.2%	5.5%	6.7%	7.9%	9.0%	10.0%	11.0%	12.0%	

Notes: *Inverse of 1.30 CAD/USD applied. Colour legend: **PEA base case price**

Table 22.15: NPV Pre-Tax @ 8% Sensitivity to Nickel Price & Nickel Payable %

NPV Pre-Tax (US\$M)		Nickel Price - Flat (US\$/lb)										
Ni Payable %		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	65%	(1,547)	(1,335)	(1,122)	(909)	(696)	(483)	(271)	(58)	155	368	581
	66%	(1,508)	(1,292)	(1,076)	(860)	(644)	(428)	(211)	5	221	437	653
	67%	(1,469)	(1,249)	(1,030)	(811)	(591)	(372)	(152)	67	286	506	725
	68%	(1,429)	(1,207)	(984)	(761)	(539)	(316)	(93)	129	352	575	797
	69%	(1,390)	(1,164)	(938)	(712)	(486)	(260)	(34)	192	418	644	870
	70%	(1,351)	(1,121)	(892)	(663)	(434)	(204)	25	254	483	713	942
	71%	(1,311)	(1,079)	(846)	(614)	(381)	(149)	84	316	549	781	1,014
	72%	(1,272)	(1,036)	(800)	(564)	(329)	(93)	143	379	615	850	1,086
	73%	(1,232)	(993)	(754)	(515)	(276)	(37)	202	441	680	919	1,158
	74%	(1,193)	(951)	(708)	(466)	(224)	19	261	504	746	988	1,231
	75%	(1,154)	(908)	(662)	(417)	(171)	75	320	566	812	1,057	1,303
	76%	(1,114)	(865)	(616)	(367)	(119)	130	379	628	877	1,126	1,375
	77%	(1,075)	(823)	(570)	(318)	(66)	186	438	691	943	1,195	1,447
	78%	(1,035)	(780)	(525)	(269)	(14)	242	497	753	1,008	1,264	1,519
79%	(996)	(737)	(479)	(220)	39	298	557	815	1,074	1,333	1,592	
80%	(957)	(695)	(433)	(171)	91	354	616	878	1,140	1,402	1,664	

Note: Colour legend: PEA base case price

Table 22.16: NPV After-Tax @ 8% Sensitivity to Nickel Price & Nickel Payable %

NPV After-Tax (US\$M)		Nickel Price - Flat (US\$/lb)										
Ni Payable %		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
	65%	(1,560)	(1,352)	(1,143)	(945)	(764)	(601)	(444)	(293)	(147)	(3)	139
	66%	(1,522)	(1,310)	(1,098)	(902)	(722)	(559)	(402)	(250)	(102)	43	187
	67%	(1,483)	(1,268)	(1,055)	(859)	(682)	(518)	(359)	(207)	(58)	89	235
	68%	(1,444)	(1,226)	(1,013)	(817)	(642)	(477)	(318)	(164)	(14)	135	282
	69%	(1,406)	(1,185)	(971)	(777)	(603)	(437)	(277)	(122)	30	181	330
	70%	(1,367)	(1,143)	(930)	(737)	(563)	(396)	(236)	(80)	74	226	377
	71%	(1,329)	(1,101)	(890)	(699)	(525)	(357)	(195)	(38)	118	272	425
	72%	(1,290)	(1,060)	(850)	(661)	(486)	(317)	(155)	4	162	317	472
	73%	(1,252)	(1,021)	(811)	(624)	(448)	(279)	(115)	46	205	363	519
	74%	(1,213)	(983)	(774)	(588)	(410)	(240)	(75)	88	248	408	566
	75%	(1,174)	(945)	(737)	(551)	(373)	(202)	(35)	129	292	453	613
	76%	(1,136)	(907)	(701)	(515)	(336)	(164)	4	171	335	498	660
	77%	(1,097)	(870)	(666)	(479)	(299)	(126)	44	212	378	543	707
	78%	(1,060)	(833)	(631)	(443)	(262)	(88)	84	253	421	588	753
79%	(1,024)	(797)	(597)	(408)	(226)	(50)	123	294	464	633	800	
80%	(988)	(763)	(563)	(372)	(190)	(13)	162	335	507	677	846	

Note: Colour legend: PEA base case price

Table 22.17: IRR Pre-Tax Sensitivity to Nickel Price & Nickel Payable %

IRR Pre-Tax (%)		Nickel Price - Flat (US\$/lb)										
		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
Ni Payable %	65%	-8.5%	-3.8%	-0.8%	1.4%	3.3%	4.9%	6.3%	7.7%	8.9%	10.1%	11.2%
	66%	-7.4%	-3.1%	-0.3%	1.9%	3.7%	5.3%	6.7%	8.0%	9.3%	10.5%	11.6%
	67%	-6.4%	-2.4%	0.2%	2.3%	4.1%	5.6%	7.1%	8.4%	9.6%	10.8%	12.0%
	68%	-5.5%	-1.9%	0.7%	2.7%	4.5%	6.0%	7.4%	8.8%	10.0%	11.2%	12.3%
	69%	-4.7%	-1.3%	1.1%	3.1%	4.8%	6.4%	7.8%	9.1%	10.4%	11.5%	12.7%
	70%	-4.0%	-0.8%	1.6%	3.5%	5.2%	6.7%	8.1%	9.5%	10.7%	11.9%	13.0%
	71%	-3.4%	-0.3%	2.0%	3.9%	5.6%	7.1%	8.5%	9.8%	11.1%	12.2%	13.4%
	72%	-2.8%	0.2%	2.4%	4.3%	5.9%	7.4%	8.8%	10.2%	11.4%	12.6%	13.7%
	73%	-2.2%	0.6%	2.8%	4.6%	6.3%	7.8%	9.2%	10.5%	11.7%	12.9%	14.1%
	74%	-1.7%	1.0%	3.2%	5.0%	6.6%	8.1%	9.5%	10.8%	12.1%	13.3%	14.4%
	75%	-1.2%	1.4%	3.5%	5.3%	7.0%	8.4%	9.8%	11.1%	12.4%	13.6%	14.8%
	76%	-0.7%	1.8%	3.9%	5.7%	7.3%	8.8%	10.2%	11.5%	12.7%	13.9%	15.1%
	77%	-0.3%	2.2%	4.2%	6.0%	7.6%	9.1%	10.5%	11.8%	13.0%	14.3%	15.4%
	78%	0.2%	2.6%	4.6%	6.3%	7.9%	9.4%	10.8%	12.1%	13.4%	14.6%	15.7%
79%	0.6%	2.9%	4.9%	6.6%	8.2%	9.7%	11.1%	12.4%	13.7%	14.9%	16.1%	
80%	1.0%	3.3%	5.2%	7.0%	8.5%	10.0%	11.4%	12.7%	14.0%	15.2%	16.4%	

Note: Colour legend: PEA base case price

Table 22.18: IRR After-Tax Sensitivity to Nickel Price & Nickel Payable %

IRR After-Tax (%)		Nickel Price - Flat (US\$/lb)										
		6.00	6.50	7.00	7.50	8.00	8.50	9.00	9.50	10.00	10.50	11.00
Ni Payable %	65%	-8.8%	-4.0%	-1.0%	0.9%	2.4%	3.7%	4.9%	6.0%	7.0%	8.0%	8.9%
	66%	-7.7%	-3.3%	-0.5%	1.2%	2.7%	4.0%	5.2%	6.3%	7.3%	8.3%	9.2%
	67%	-6.7%	-2.7%	-0.1%	1.6%	3.0%	4.3%	5.5%	6.6%	7.6%	8.6%	9.5%
	68%	-5.8%	-2.1%	0.3%	2.0%	3.4%	4.6%	5.8%	6.9%	7.9%	8.9%	9.8%
	69%	-5.0%	-1.5%	0.6%	2.3%	3.7%	4.9%	6.1%	7.2%	8.2%	9.2%	10.1%
	70%	-4.3%	-1.0%	1.0%	2.6%	4.0%	5.2%	6.4%	7.5%	8.5%	9.5%	10.4%
	71%	-3.6%	-0.5%	1.3%	2.9%	4.3%	5.5%	6.7%	7.7%	8.8%	9.7%	10.7%
	72%	-3.0%	-0.1%	1.7%	3.2%	4.6%	5.8%	6.9%	8.0%	9.1%	10.0%	11.0%
	73%	-2.4%	0.2%	2.0%	3.5%	4.8%	6.1%	7.2%	8.3%	9.3%	10.3%	11.2%
	74%	-1.9%	0.5%	2.3%	3.8%	5.1%	6.4%	7.5%	8.6%	9.6%	10.6%	11.5%
	75%	-1.4%	0.9%	2.6%	4.1%	5.4%	6.6%	7.8%	8.8%	9.9%	10.9%	11.8%
	76%	-0.9%	1.2%	2.9%	4.3%	5.7%	6.9%	8.0%	9.1%	10.1%	11.1%	12.1%
	77%	-0.5%	1.5%	3.2%	4.6%	5.9%	7.2%	8.3%	9.4%	10.4%	11.4%	12.3%
	78%	-0.1%	1.8%	3.4%	4.9%	6.2%	7.4%	8.5%	9.6%	10.7%	11.6%	12.6%
79%	0.2%	2.1%	3.7%	5.1%	6.5%	7.7%	8.8%	9.9%	10.9%	11.9%	12.9%	
80%	0.5%	2.4%	4.0%	5.4%	6.7%	7.9%	9.1%	10.1%	11.2%	12.2%	13.1%	

Note: Colour legend: PEA base case price.

23.0 ADJACENT PROPERTIES

There are no adjacent properties that meet the definition of NI 43-101.

There are two nearby properties that could be relevant to further project development. These are described briefly in the subsections below.

In addition, there are a number of jade and placer mining operations in the area. These facilities are not expected to provide any significant benefit or risk to the Turnagain project.

23.1 Kutcho Copper-Zinc-Silver-Gold Deposit

The Kutcho copper-zinc-silver-gold deposit lies approximately 40 km southeast of the Turnagain deposit. Kutcho Copper Corporation (Kutcho) owns 100% of the project as of October 2020.

A pre-feasibility study was completed in 2017, and Kutcho is currently conducting a feasibility study (source: Kutcho Copper Corporation SEDAR filing, effective date June 15, 2017).

Kutcho received a Section 11 Order from the British Columbia Environmental Assessment Office on December 12th, 2019 (source: December 13, 2019 Press Release issued by Kutcho Copper Corporation).

If both the Kutcho and Turnagain facilities are constructed, approximately 60 to 70 km of road access will be shared, depending on the final route selected for each company.

23.2 Eaglehead Copper-Molybdenum-Gold Deposit

The Eaglehead copper-molybdenum-gold deposit lies approximately 14 km west of the Turnagain deposit. District Copper Corporation owns a 100% interest in this porphyry Cu-Mo-Au project, which was the subject of a 2019 Technical Report (source: District Copper Corporation SEDAR filing, effective date October 21, 2019).

Should Eaglehead and Turnagain proceed to development, approximately 70 km of road access will be in common (depending on the final route selected for each company).

It is important to note that the author is not implying similarities in geology, commodity type or mineral resource. The author is not relying on any technical information, so verification and validation was not performed. However, these projects may benefit from shared infrastructure and community relationships that may assist in advancing to sustainable development.

24.0 OTHER RELEVANT DATA & INFORMATION

The completion of additional technical programs, engineering studies, and environmental studies is expected to take a minimum of 3.0 years. Following successful financing, project construction is expected to take an additional 2.5 to 3.0 years, depending on leading activities.

A preliminary project execution plan will be prepared in the next study phase.

25.0 INTERPRETATION & CONCLUSIONS

Based on the outcomes of this PEA, the contributors have drawn the following key conclusions.

25.1 Geology & Mineral Resources

The mineral resources were estimated in conformity with CIM's "Estimation of Mineral Resources and Mineral Reserves Best Practices Guidelines" (December, 2019) and are reported in accordance with NI 43-101 guidelines.

The 362 drill holes in the database were supplied in electronic format by Giga Metals, 307 of which had assay values. The primary economic contributor is shown to be nickel (Ni%) content, and the secondary is cobalt (Co%). Sulphur (S%) has similarly been analysed and estimated on a block-by-block basis. Assay values were composited to 4.0 m within the mineralised domains: (1) Du-Wh-Sp (dunite, wehrlite, serpentinite); (2) cPx-oPx (clinopyroxenite, olivine, magnetite and hornblende clinopyroxenite); (3) volcanics; (4) dykes; (5) overburden.

The mineralised domains were re-interpreted and refined including the current drilling data. The mineral resource estimate is based on an additional 36 infill drill holes totalling 8,940 metres drilled in 2018 in the areas of the conceptual open pit in addition to updated geological modelling.

Mineral resources are classified under the categories of *measured*, *indicated* and *inferred* according to CIM guidelines. The author evaluated the resource in order to ensure that it meets the condition of "reasonable prospects of eventual economic extraction" as suggested under NI 43-101. The criteria considered were confidence, continuity and economic cut-off in addition to considering constringed the resources within an optimised pit shell based on.

Using a cut-off grade of 0.1% Ni, the Turnagain property contains an estimated 1,073 Mt of measured and indicated resources at 0.220% Ni and 0.013% Co. An additional 1,142 Mt grading 0.217% Ni and 0.013% Co is classified as inferred. The resource estimate is presented in Table 25.1.

Table 25.1: Mineral Resource Estimate

Resource Category	Kilotonnes	% Ni (T)	% Co (T)
Measured	360,913	0.230	0.014
Indicated	712,406	0.215	0.013
Measured & Indicated	1,073,319	0.220	0.013
Inferred	1,142,101	0.217	0.013

Notes: **(1)** All mineral resources have been estimated in accordance with Canadian Institute of Mining and Metallurgy and Petroleum ("CIM") definitions, as required under National Instrument 43-101 ("NI 43-101"). **(2)** Mineral resources are reported in relation to a conceptual pit shell in order to demonstrate reasonable expectation of eventual economic extraction, as required under NI 43-101; mineralisation lying outside of these pit shells is not reported as a mineral resource. **Mineral resources are not mineral reserves & do not have demonstrated economic viability.** **(3)** Open pit mineral resources are reported at a cut-off grade of 0.1% Ni. Cut-off grades are based on a price of US \$7.50 per pound, nickel recoveries of 60%, mineralized material and

waste mining costs of \$2.80, along with milling, processing and G&A costs of \$7.20. **(4)** Inferred mineral resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorised as mineral reserves. However, it is reasonably expected that the majority of inferred mineral resources could be upgraded to indicated. **(5)** Due to rounding, numbers presented may not add up precisely to the totals provided and percentages may not precisely reflect absolute figures.

This PEA indicates the Turnagain property generates an internal rate of return below the applied discount rate on the estimated N.I. 43-101 compliant resource at base case scenario modelling parameters.

This PEA indicates the Turnagain property generates an internal rate of return below the applied discount rate on the estimated N.I. 43-101 compliant resource at base case scenario modelling parameters. The project economics could improve with the opportunities noted in Section 25.8. It is recommended that Giga Metals carry the project forward to the pre-feasibility stage in accordance with the budget in Table 1.8. Recommendations by study area for the next phase are summarized in Section 26.

25.2 Mining

The Turnagain deposit will be mined using conventional open pit mining methods employing high-volume trucks and shovels. The use of large mining equipment will achieve high mining rates and ensure the lowest possible mine operations unit costs. A mining strategy was developed that delivers higher value mineralised material to the mill in the early years of the mine life. During the later years in the 37-year life, the mill will be fed with low-grade stockpile material. This strategy involves a phased approach to the production schedule, whereby the project commences at a lower throughput level of 45,000 t/d for the first five years, and expands to a 90,000 t/d operation for the remainder of the mine life.

The mine production plan is primarily based on respective value cut-off grades. Variations in throughput, energy draw, and recovery are critical factors in actual unit costs. Variations in these factors have the potential to impact the mine development plan/design/sequence.

Further geotechnical, geomechanical (open pit), and hydrogeological studies are required to support the detailed mine design and site configurations.

25.3 Metallurgical Testing

Five different variability studies have been conducted on project samples since 2009. Each of these studies revealed a link between rougher nickel recovery and sulphur head grade, so these have been used to build a basic geometallurgical model for the project.

Further work is required to refine the flowsheet. This work includes investigating the use of regrinding in concentrate cleaning and determining how to tailor the production of concentrates for specific markets. Additional work is also needed on lower sulphur-bearing samples.

25.4 Recovery Methods

Concentrator design work completed to date confirms that the Turnagain mineralisation can be treated in a 90,000 t/d HPGR plus ball mill circuit followed by froth flotation to produce a high-grade nickel concentrate.

The two-train comminution circuit followed by four banks of rougher flotation also lends itself to a phased approach. The capital cost estimate has been developed accordingly.

25.5 Tailings & Water Management

Results of the work completed to date suggest that the current waste and water management concept is practicable and should be carried forward to the next level of design (pre-feasibility study).

The conceptual design presented in this report can likely be optimised as the design basis and operating criteria are further refined.

25.6 Power Supply

With construction of the 287 kV powerline to Tatogga Lake there is increased certainty of power supply to the Turnagain Project and increased confidence in associated capital cost estimates.

25.7 Economic Analysis

The PEA base case is based on the long-term nickel and cobalt prices of US\$7.50/lb Ni and US\$22.30/lb Co as provided by Wood Mackenzie, and returns a pre-tax IRR of 6.3% and pre-tax NPV @ 8% of US\$(269) M. The after-tax NPV @ 8% is US\$(443) M and the after-tax IRR is 4.9%. The project returns are highly sensitive to a variety of factors.

25.8 Opportunities & Risks

There are certain risks that may affect the viability of the project going forward that should be studied and addressed. Opportunities also exist that could have a positive impact on the project going forward. These risks and opportunities are outlined below.

25.8.1 Risks

Potential project risks are outlined in the subsections below.

25.8.1.1 Geology & Mineral Resources

- Further studies related to lithological and geometallurgical characteristics may require refined domain models that restrict the amount of recoverable resource and decrease the size of the mineral resources.

- COVID-19 poses a risk to timelines and availability of personnel needed for project advancement and completion.
- There is no guarantee that further drilling will result in additional resources or increased classification.
- The optimised pit that constrains the resources (which defines the 'reasonable prospects of eventual economic extraction') traverses the river. This option has not been ruled out; however, it is not the selected option in this design.
- Lower commodity prices will change size and grade of the potential targets.
- Further work may disprove previous models and therefore result in condemnation of targets and potential negative economic outcomes.

25.8.1.2 Mining

- Pit geotechnical and hydrogeological parameters are preliminary and shallower pit slopes could negatively impact resources particularly in the vicinity of the Turnagain River. However, the risk of significantly increasing strip ratios is not considered to be high.
- The mine production schedule described in this study includes inferred resources that are considered too speculative geologically to have the economic considerations applied to them that would enable them to be categorised as mineral reserves, and there is no certainty that these data will be realised.
- It is assumed that waste dumps will be constructed by low-cost, end-dumping methods. Operating costs will increase if the waste dumps have to be constructed in limited-height lifts due to foundation weakness or poor material quality issues.

25.8.1.3 Recovery Methods

- Long-term stockpiling of lower grade material may expose material to metallurgical degradation and may negatively impact mineral processing metal recoveries.
- The algorithm used to estimate overall nickel recovery in the concentrator has been validated against few samples of mineralized material containing less than 0.5% sulphur grade, implying a lower confidence level in projected recoveries for the later years in the mine life (after Year 16 of operation, some years below 0.5% S grade). This further implies that the process design requirements of the recovery circuit may require changes as further metallurgical testwork is completed.
- The HPGR comminution circuit design for the processing plant requires extensive bulk material transport infrastructure (conveyors, bins, etc.). The cold climate of the Turnagain operation may lead to issues in material handling at transfer points due to frozen material.
- The impact of the Turnagain mineralized material on HPGR equipment wear (e.g., HPGR rolls and discharge splitter) has yet to be determined through HPGR pilot testwork. There is potential that HPGR equipment wear rates may be higher than

estimated in this study, which may adversely impact project economics through increased operating expenditure.

25.8.1.4 Project Infrastructure

- Geotechnical parameters for the waste dump and low-grade stockpile designs and configurations need to be confirmed, although there is flexibility in the site layout to accommodate some adjustments.

25.8.1.5 Environmental Baseline Studies, Permitting & Social or Community Impact

- The environmental impact assessment process requires multiple consecutive years of environmental baseline studies and assessment of the results, as well as extensive public, stakeholder and Indigenous Group consultation processes. The EIA process has not yet commenced in a formal manner, and the project timeline should reflect the probable duration of this process, including the uncertainty associated with the regulatory and consultation aspects of the process.
- Environmental aspects associated with infrastructure and ancillary aspects of the project, such as the access road, transmission line, camp and airstrip facilities, may need to be included in the scope of the EIA and an assessment certificate issued prior to work commencing.

25.8.2 Opportunities

Potential project opportunities are outlined in the subsections below.

25.8.2.1 Geology & Mineral Resources

- An intelligent, systematic exploration program could provide an excellent opportunity for successfully uncovering new discoveries.
- An increased understanding and derivation of alternative theories may result in further discovery and significant expansion for the project.
- Higher commodity prices will change size and grade of the potential targets.
- Potential for expansion and classification upgrade of resources contained within the ultimate pit and in the immediate proximity.
- Additional resources in the Hatzl and Cliff areas, with the latter offering potential for additional platinum and palladium values.
- Enhanced geometallurgical knowledge of the mineralisation will aid in detailing and segregating higher grade recoverable resources.
- Further metallurgical improvements are possible, particularly in relation to geological modelling and recovery.
- The opportunity of full project optimisation, taking into account the geometallurgical characteristics of the mineralisation as noted above.
- Opportunity to employ in-country resources and personnel due to COVID-19.

25.8.2.2 Mining

- Re-routing a portion of the Turnagain River to facilitate access to mineralisation in the eastern Horsetrail Zone which is currently limited to the north by the natural river alignment.
- Use of automated mine production equipment offers potential productivity improvements and reduced operating costs.
- Use of diesel-electric, hybrid, or all-electric haul trucks may offer potential for reduced operating costs and carbon footprint.
- While light-duty vehicles, such as the support fleet, can feasibly be replaced by battery electric alternatives soon arriving on the market, heavier hauling trucks exceeding 100 tonnes of hauling capacity may require a more energy dense storage technology. Given that such vehicles have an electric drive already in place, the use of hydrogen fuel cells with batteries as a hybrid enables the electrification of these vehicles to maintain their payload capacity while not sacrificing range significantly. Currently there are initiatives to engineer and produce hydrogen fuel cell haul trucks with a greater hauling capacity than 100 tonnes. Release dates are anticipated starting from 2021.
- Electrified trolley assist could possibly be applied to some sections of the haul routes to reduce haul truck fuel consumption.
- Application of in-pit and/or semi-mobile crushing and conveying may offer potential for reduced pit haulage fuel consumption and mine operating unit costs.

25.8.2.3 Metallurgical Testing

- Enhanced geometallurgical knowledge of the mineralisation as an aid to pit optimisation and to facilitate targeting of higher value zones earlier in the mine life.
- Further metallurgical improvements, particularly related to geological modelling and recovery.

25.8.2.4 Recovery Methods

- Potential to achieve higher payment for concentrates via other process technologies (roasting, hydrometallurgical refining, etc.).
- Additional preliminary engineering studies have indicated potential opportunities to improve project economics using an alternate comminution circuit design approach that may allow up to 35% higher single-train capacity.
- Opportunities linked to recent developments in comminution technology and flowsheet design can be explored in further studies. Configurations that may become attractive in the near future, and may be an object for future trade-offs:
 - HPGR-HPGR-BM-BM circuit to increase HPGR utilisation and overall comminution energy efficiency
 - HPGR-HPGR-stirred mill allowing even greater comminution energy efficiency

- Other mineral processing options, such as gravity separation, may provide an opportunity to improve recovery or may be used as a pre-concentration stage to reduce comminution circuit energy consumption. The Pt-Pd values in the nickel concentrate are not expected to be at payable levels. A gravity circuit on nickel concentrate could create a high-grade payable platinum-palladium concentrate.
- Expediting process plant expansion phasing will increase mineral processing capacity in early years, and may improve project economics.
- Woodgrove & Eriez flotation reactors may offer an opportunity to reduce plant footprint and energy usage in the recovery circuit if future testwork demonstrates their effectiveness in processing Turnagain ore.
- Modifications to flotation chemistry may offer opportunities to improve recovery.
- Additional metallurgical testwork has indicated potential improvements to project economics with a revised flotation strategy including separate high-grade and low-grade flotation circuits (roughers in series producing high- and low-grade rougher concentrates for separate cleaning, allowing for customised reagent usage and possible low-grade rougher concentrate regrinding).

25.8.2.5 Project Infrastructure & Tailings Management Facility

- Utilise run-of-mine waste rock as TMF buttress material to reduce total site footprint and potentially reduce TMF construction costs.
- Shared access development costs with the potential development of the Kutcho Creek Project further to the west.

25.8.2.6 Power Supply

- Potential to negotiate the BC Hydro connection in the context of helping the government achieve its climate goals (avoid LNG, implement non-diesel mining fleet).
- Potential elimination of Tariff Supplement 37, which would significantly reduce projected BC Hydro interconnection fees.

25.8.2.7 Environmental Baseline Studies, Permitting & Social or Community Impact

- Potential to provide economic opportunities for First Nations with infrastructure ownership and operation as well as contracting opportunities.
- Potential to monetise the sequestration of carbon in the tailings facility.
- Based on the diesel and electricity consumption for mining activities, the carbon intensity calculated for the operations is averaged to 74,428 tCO_{2e}/year. Most of the emissions are direct emissions (scope 1) and are coming from the diesel consumption of the mining fleet. There is an opportunity to reduce the carbon intensity to 23,080 tCO_{2e}/year through electrification of the mining fleet and shift the majority of the fleet-emissions to indirect emissions (scope 2) associated with the generation of electrical power by BC Hydro.

26.0 RECOMMENDATIONS

26.1 Introduction

This PEA indicates the Turnagain property generates an internal rate of return below the applied discount rate on the estimated N.I. 43-101 compliant resource at base case scenario modelling parameters. The project economics could improve with the opportunities noted in Section 25.8. It is recommended that Giga Metals carry the project forward to the pre-feasibility stage in accordance with the budget in Table 1.8. Recommendations by study area for the next phase are summarised in the sections below.

26.2 Geology & Mineral Resources

To advance the Turnagain Project to the pre-feasibility study stage and further evaluate the potential adjacent deposits, the following work program is recommended:

- drill 25 holes for a total of 8,650 m focussed on upgrading inferred resources within the design pit to indicated resources and for geotechnical purposes
- carry out geometallurgical study and geometallurgical domain modelling to support an updated resource estimation and improved metallurgical modelling
- explore for significant Hatzl and Cliff deposits for potential to bring into resources

26.3 Mining

26.3.1 Plant Throughput & Metal Recoveries

Plant throughput and metal recoveries are applied without incorporating potential variations within or between the deposit geological domains. The geological model used in this PEA is a significant re-interpolation of data when compared to previous studies. Further geometallurgical testing, geological interpreting and geological modelling will be necessary to confirm the universal applicability of the parameters used in this report. It is recommended that future mine planning studies be performed incorporating updated geological, geometallurgical and domain data.

26.3.2 Increased Production Rate with Mine Resource Expansion

The Hatzl Zone has been excluded from the mining plan in this PEA study. The geological model outcrops in the zone, indicating there is potential for increasing the near-surface mineable resource. The inclusion of the Hatzl deposit would increase the size of the mine.

Attractive mineralisation appears to extend below the Turnagain River from the Horsetrail zone and the current pit shell configurations are limited by the river boundary. It is recommended that trade-off studies be performed to determine the viability of re-routing the river to the east to facilitate recovery of mineralisation both deeper in the Horsetrail pit and to the east of the current planned shell crest.

Fleet selections should be further refined to assess the potential application of automation, trolley assist, and pit crusher conveyor systems.

The proposed life of mine is 37 years. It is a low strip ratio operation, indicating there is an opportunity to increase the production capacity and throughput rate to better take advantage of economies of scale and lower unit costs. Lower operating costs could generate higher revenues and potentially increase the mineable resource. It is therefore recommended that production rate scenario trade-off studies be performed for further optimization. These scenario runs are to incorporate updated geological modelling, updated metallurgical testing, geometallurgical domain assessment, and updated scenario costing.

26.3.3 Geotechnical & Hydrogeological Risks

A limited number of geotechnical and hydrogeological studies have been conducted on pit wall stability and waste disposal locations. Pit slopes may have to be decreased, thereby reducing the total accessible resource and to some degree increasing the strip ratio. Conversely, any increase to wall slope angles would increase the volume of accessible resource.

Groundwater sources must be studied in order to implement a dewatering plan and determine a safe slope angle for the south pit wall, particularly with regard to the proximity of Turnagain River. Even relatively minor pit slope issues on the south wall could have potentially significant consequences. The low-lying areas within the potential pit limits are receptors for water draining off the slopes, and are deemed to be saturated. Hydrogeological studies are recommended to determine the degree of dewatering necessary to keep the pit dry under operating conditions.

Hydrogeological and geotechnical studies are recommended to determine the degree of dewatering necessary to keep the pit dry under operating conditions, and assess pit slope and waste dump design parameters.

26.4 Metallurgical Testing

To further advance the project the following work is recommended:

- Carry out testwork on low sulphur feed material. The majority of the samples tested to date have contained sulphur that is much higher than now planned.
- Enhance the current understanding of geometallurgical drivers and improve the geometallurgical link to the resource model. For example, potentially correlate lithotypes, alterations, etc. with throughput, grind energy and recovery.
- Test gravity separation on nickel concentrate samples to determine if a payable PGE concentrate can be produced.

26.5 Recovery Methods

The following aspects of mineral processing design will need to be explored in subsequent phases of this project:

- Explore the potential for regrinding part of the rougher concentrate to achieve higher recovery, potentially up to 4%.
- Explore the potential to produce two concentrates targeting two different markets.
- Conduct a grade versus recovery test work program (there might be opportunities to use a different reagent scheme if the focus is recovery and not grade, such as in this case (18% Ni grade).
- Conduct further comminution and HPGR pilot testwork to validate and refine the design of the comminution flowsheet. Comminution testwork recommendations for future phases of study are as follows:
 - single-stage open-circuit HPGR tests at different specific pressing force settings (~800 kg): ~\$13,000 preliminary estimate cost for the testwork program
 - second-stage open-circuit HPGR tests at different specific pressing force settings (use first-stage HPGR product): ~\$6,000 preliminary estimate cost for the testwork program
 - locked cycle HPGR tests with edge recycle at one recommended specific pressing force setting (700 kg): ~\$13,000 preliminary estimate cost for the testwork program
 - stirred mill testing for second-stage fine grinding (optional) (~20 kg composite from subsample of HPGR testwork product): ~\$5,000 preliminary estimate cost for the testwork program
 - due to the lack of certainty in power cost, stirred mill testwork can be explored to further provide comminution alternatives
- Conduct further flotation testwork using products of HPGR and comminution testwork.
- Conduct thickening and filtration testwork for concentrate. Tailings settling tests should be carried out to investigate tailings thickener as a means of reducing pumping costs associated with tailings reclaim.
- Optimise flotation equipment selection and sizing:
 - investigate recent flotation equipment developed (more modern) as opposed to tank cells (e.g., Eriez stack cells, Woodgrove SFRs)
 - investigate coarser flotation testing Eriez hydrofloat options

26.6 Project Infrastructure & Tailings Management Facility

Further optimisation required in the next phase of study includes the following:

- tailings thickener to save power pumping reclaim water back from TMF and have smaller tailings lines
- Evaluate the potential use of mine waste rock for TMF construction
- PFS design for earthworks and roads to improve the capital cost estimate accuracy

26.7 Power Line

In order to address risks associated with the transmission line and to avoid unnecessary delays in approval processes, key recommendations/next steps include the following:

- request BC Hydro conduct a System Impact Study to confirm available transmission capacity and connection methods
- review transmission line cost estimating assumptions and updating transmission line cost estimates, as necessary (estimates were based on actual construction information on the cost of the NTL from Terrace to Bob Quinn, and the transmission line extension to Tatogga Lake)
- assess potential transmission line routes for cases with connection to BC Hydro's grid; particularly, the section along Highway 37 beside Stikine Provincial Park
- engage with First Nations
- consult with stakeholders and engage with the public
- keep a watching brief on:
 - the progress of BC Hydro's Site C project, and public statements regarding the project's anticipated effect on electricity rate schedules
 - progress of other projects proposing to connect to the NTL, as this may impact the cost of interconnection for the proposed Turnagain mine
 - discussions regarding Tariff Supplement 37, and provide input to BC Hydro/Province of BC through channels such as the Mining Association of BC
 - the economics of large-scale batteries for industrial load shaping
 - the status of alternative LNG terminal projects and the commodity cost of LNG
- Optimisation in the next phase of study:
 - confirm the most economic configuration for the site power grid (i.e., main substation at the concentrator plant and 25 kV overhead line distribution to the other areas)
 - investigate how to improve the power factor, especially by reviewing options for large drives such as for the ball mills
 - consider diesel (rather than electric) mining equipment (shovels and drills) to reduce load swings on the site power grid

26.8 Environmental Baseline Studies, Permitting & Social or Community Impact

With initiation of the EIA process, the scope of environmental baseline studies will be defined, and the consultation and engagement process requirements will be established. Based on these inputs and realistic timelines for the EIA processes considering recent experience for mines in BC, a permitting strategy, timeline and work plan must be developed. This strategy must integrate with the planned progress of the design, and include an allowance for an assessment of alternatives and reviews by interested parties and stakeholders.

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ATTACHMENT 1: QUALIFIED PERSON CERTIFICATES

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Ian Thompson, do hereby certify that:

1. I am Senior Mining Engineer with the firm of Hatch Ltd. with an office located at 1066 West Hastings Street, Suite 400, Vancouver, BC, Canada.
2. I am a graduate of UBC, where in 1989 I obtained a Bachelor of Applied Science degree in Mining and Mineral Process Engineering.
3. I have practiced my current profession continuously since 1989. My principal experience is in the area of open pit mining, mine design, mine planning and development, and reserve evaluations.
4. I am a Professional Engineer registered with the Engineers and Geoscientists British Columbia (Registration #27598).
5. I have personally inspected the subject property on October 9 to 10, 2018.
6. I have read the definition of a qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
7. I, as a qualified person, am independent of the issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Sections 1.1, 1.2, 1.3, 1.8, 1.9, 1.11, 1.12, 1.13, 2, 3, 4.4, 5.1, 5.4, 15, 16, 18.3, 21 (except for 21.1.2, 21.1.3.1, 21.1.4, 21.2.3, 21.2.6), 22, 24, 25.2, 25.7, 25.8.1.2, 25.8.2.2, 26.1, 26.3 and 27, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
9. I have had no prior involvement with the subject property.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Ian S. Thompson, P.Eng.
Senior Mining Engineer

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Persio Pellegrini Rosario, do hereby certify that:

1. I am the Director of Comminution with the firm of Hatch Ltd. with an office located at 1066 West Hastings Street, Suite 400, Vancouver, BC, Canada.
2. I am a graduate of the University of British Columbia, where, in 2003 and 2010, respectively, I obtained the Master in Applied Sciences (MAsc) and the Doctor in Philosophy (PhD) degrees in Mineral Processing through the Mining and Mineral Processing Department.
3. I have practiced my current profession continuously since 2003. My principal experience is in the areas of base and precious metals mineral processing.
4. I am a Professional Engineer registered with the registered with the Engineers and Geoscientists of British Columbia.
5. I have not personally inspected the subject property.
6. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
7. I, as a qualified person, am independent of the issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Sections 1.7, 17, 21.1.2, 21.2.3, 25.4, 25.8.1.3, 25.8.2.4, 26.5, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
9. I have had no prior involvement with the subject property.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Persio Pellegrini Rosario, MAsc, PhD, P.Eng
Director, Comminution – Mining & Mineral Processing

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Evan Lewis Jones, do hereby certify that:

1. I am Regional Director, Environmental Services Group, with the firm of Hatch Ltd. with an office located at 1066 West Hastings Street, Suite 400, Vancouver, BC, Canada.
2. I am a graduate of the University of British Columbia, where, in 1985, I obtained a Bachelors of Applied Science through the Bio-Resource Engineering Department.
3. I am a graduate of the University of British Columbia, where, in 1990, I obtained a Masters of Applied Science through the Civil Engineering Department.
4. I have practiced my current profession continuously since 1985. My principal experience is in the areas of Environmental Engineering.
5. I am a Professional Engineer registered with the Engineers and Geoscientists of British Columbia;
6. I have not personally inspected the subject property.
7. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
8. I, as a qualified person, am independent of the issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
9. I am a contributing author of the Technical Report and am responsible for Sections 1.10, 4.3, 5.2, 5.3, 5.6, 20, 25.8.1.5, 25.8.2.7, 26.8, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
10. I have had no prior involvement with the subject property.
11. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 9 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
12. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Evan Jones, P.Eng., EP(CEA)
Regional Director, Environmental Services Group

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Gerald (Gerry) Schwab, do hereby certify that:

1. I am a Project Manager with the firm of Hatch Ltd. with an office located at 1066 West Hastings Street, Suite 400, Vancouver, BC, Canada.
2. I am a graduate of the University of British Columbia, where, in 1984 I obtained a BSc in Mechanical Engineering through the Engineering Department.
3. I have practiced my current profession continuously since 1984. My principal experience is in the areas of process plant design, and project management.
4. I am a Professional Engineer registered with the Engineers and Geoscientists of British Columbia;
5. I have not personally inspected the subject property.
6. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
7. I, as a qualified person, am independent of the issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Sections 5.5, 18.1, 18.5.5, 18.5.6, 18.5.7, 18.6, 18.7, 18.9, 18.10, 25.8.1.4, 25.8.2.5, 26.6, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
9. I have had no prior involvement with the subject property.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Gerry Schwab, P.Eng.

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Garth David Kirkham, do hereby certify that:

1. I am a consulting geoscientist with an office at 6331 Palace Place, Burnaby, British Columbia.
2. I am a graduate of the University of Alberta in 1983 with a B. Sc.
3. I have continuously practiced my profession since 1988. My principal experience is in the areas of geology and resource estimation having authored many NI43-101 technical reports including Bralorne, Table Mountain, Monument Bay, Minto, Kutcho Creek, Cerro Las Minitas and Cerro Blanco. I am currently the Geological and Resource Technical Expert for Group Ten Metals and Valore Metals developing the Stillwater West PGE-Ni and Kluane PGE-Ni-Cu, and the Pedra Branca PGE-Cr meta-volcanic, ultramafic deposits, respectively.
4. I am a Professional Geoscientist and a member in good standing of the Engineers and Geoscientists British Columbia.
5. I have visited the property on October 9 to 10, 2018.
6. I have read the definition of "qualified person" set out in National Instrument 43-101 and certify that by reason of education, experience, independence and affiliation with a professional association, I fulfil the requirements of a Qualified Person as defined in National Instrument 43-101.
7. I am independent of Giga Metals Corporation as defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Sections 1.4, 1.5, 4.1, 4.2, 6, 7, 8, 9, 10, 11, 12, 14, 23, 25.1, 25.8.1.1, 25.8.2.1, 26.2, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
9. I have not had prior involvement in the Turnagain project.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Garth Kirkham, P.Geol.
President, Kirkham Geosystems Ltd.

CERTIFICATE OF QUALIFIED PERSON

I, Daniel Friedman, P.Eng., do hereby certify that:

1. This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").
2. I am employed as a Specialist Civil Engineer of Knight Piésold Ltd. with an office at Suite 1400 - 750 West Pender Street, Vancouver, British Columbia, V6C 2T8, Canada.
3. I am a graduate of McGill University, Montreal, Canada, B.Eng. (Civil), 2003. I have practiced my profession continuously since 2004. My principal experience is in the areas of water and waste management for mining projects and hydrotechnical engineering.
4. I am a Professional Engineer (No. 32571) in good standing with Engineers and Geoscientists of British Columbia in the area of Civil Engineering.
5. I have read the definition of "qualified person" set out in National Instrument 43-101 (NI 43-101) and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfill the requirements to be a "qualified person" for the purposes of NI 43-101.
6. I visited the Turnagain property on September 7, 2005, and June 16, 2009.
7. I am a contributing author of the Technical Report and am responsible for Sections 1.9.2, 18.2, 18.4, 18.5.1, 18.5.2, 18.5.3, 18.5.4, 21.1.4, 21.2.6, 25.5, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
8. I am independent of the Issuer and related companies applying all of the tests in Section 1.5 of the NI 43-101.
9. I have had no involvement with the property that is the subject of this Technical Report.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Effective Date: October 28, 2020

Signing Date: February 3, 2021

– *Original signed and sealed* –

Daniel Friedman, P.Eng.

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Ronald J. Monk, do hereby certify that:

1. I am a Principal and Energy Sector Leader with the firm of Kerr Wood Leidal Associates Ltd. with an office located at 200 – 4185A Still Creek Drive Burnaby, BC, Canada V5C 6G9.
2. I am a graduate of the University of British Columbia, where, in 1987 I obtained Bachelor of Applied Science (with Honours), in Civil Engineering through the Civil Engineering Department.
3. I am a graduate of the University of British Columbia, where, in 1992 I obtained a Master of Engineering, in Civil Engineering (Hydraulics and Construction Management) through the Civil Engineering Department.
4. I have practiced my current profession continuously since 1987. My principal experience relevant to this Technical Report is in the areas of power supply analysis, connection to power utilities, power utility rates and tariffs and the planning of power lines for mines.
5. I am a Professional Engineer registered with Engineers and Geoscientists BC.
6. I have not personally inspected the subject property.
7. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
8. I am independent of the Issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
9. I am a contributing author of the Technical Report and am responsible for Sections 1.9.1, 18.8, 21.1.3.1, 25.6, 25.8.2.6 and 26.7 and accept professional responsibility for these sections of the Technical Report.
10. I have prior involvement with the subject property regarding power supply alternatives and carbon reduction strategies since August 2011.
11. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 9 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
12. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– *Original signed and sealed* –

Ronald J. Monk, M.Eng., P.Eng.
Principal & Energy Sector Leader

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Christopher John Martin, do hereby certify that:

1. I am President with the firm of Blue Coast Metallurgy Ltd with an office located at 1020 Herring Gull Way, Parksville, BC V9P 1R2.
2. I am a graduate of Camborne School of Mines, where, in 1984 I obtained a Bachelor of Science Degree in Mineral Processing Technology, and McGill University, where, in 1987 I obtained a Master of Engineering Degree in Metallurgical Engineering through the Department of Mining and Metallurgy.
3. I have practiced my current profession continuously since 1987. My principal experience is in the areas of comminution, and beneficiation of base and precious metal minerals, both in operations and project development.
4. I am a Chartered Engineer registered with the Engineering Council of the United Kingdom, and a Member of the Institution of Materials, Minerals and Mining.
5. I personally inspected the subject property on October 19, 2010.
6. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
7. I, as a qualified person, am independent of the Issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Sections 1.6, 13, 25.3, 25.8.2.3, 26.4, and edits thereto as set out in the updated Technical Report dated February 3, 2021, and accept professional responsibility for these sections of the Technical Report.
9. I have had no prior involvement with the subject property.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the sections of the Technical Report for which I have accepted responsibility contain all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Christopher John Martin
President

CERTIFICATE OF QUALIFIED PERSON

This certificate applies to the technical report entitled, "N.I. 43-101 Technical Report & Preliminary Economic Assessment for the Turnagain Project – Amended" prepared for Giga Metals Corporation (the "Issuer") dated February 3, 2021, with an effective date of October 28, 2020 (the "Technical Report").

I, Andrew Robert Mitchell, do hereby certify that:

1. I am Head of Nickel Research with the firm of Wood Mackenzie Ltd with an office located at Exchange Place 5 Sempole Street, Edinburgh, EH3 8BL, United Kingdom.
2. I am a graduate of Camborne School of Mines, where, in 1988 I obtained Ph. D in pyrometallurgy through the same institution.
3. I have practiced my current profession continuously since 1995. My principal experience is in the areas of nickel market analysis.
4. I am a professional engineer registered with the Institute of Materials, Minerals and Mining.
5. I have personally not inspected the subject property.
6. I have read the definition of qualified person set out in National Instrument 43-101 and certify that by virtue of my education, affiliation to a professional association, and past relevant work experience, I fulfill the requirements to be a qualified person for the purposes of National Instrument 43-101.
7. I, as a qualified person, am independent of the issuer, as that term is defined in Section 1.5 of National Instrument 43-101.
8. I am a contributing author of the Technical Report and am responsible for Section 19 and accept professional responsibility for this section of the Technical Report.
9. I have had no prior involvement with the subject property.
10. I have read National Instrument 43-101 and the sections of the Technical Report referenced in paragraph 8 of this Certificate and confirm that these sections have been prepared in accordance with National Instrument 43-101.
11. As of the effective date of this Technical Report, to the best of my knowledge, information and belief, the section of the Technical Report for which I have accepted responsibility contains all scientific and technical information required to be disclosed to make the Technical Report not misleading.

Signed and sealed this 3rd day of February 2021

– Original signed and sealed –

Andrew Robert Mitchell, PhD.
Research Director, Head of Nickel Research

ATTACHMENT 2: UNITS OF MEASURE, ACRONYMS & ABBREVIATIONS

Units of Measure

Above mean sea level	amsl
Ampere	A
Annum (year).....	a
Billion years ago	Ga
Carbon dioxide equivalent.....	CO ₂ e
Carbon dioxide equivalent (total)	tCO ₂ e
Centimetre	cm
Cubic centimetre	cm ³
Cubic feet per second	ft ³ /s or cfs
Cubic foot	ft ³
Cubic inch.....	in ³
Cubic metre	m ³
Cubic yard	yd ³
Day	d
Days per week.....	d/wk
Days per year (annum).....	d/a
Dead weight tonnes.....	dwt
Degree	°
Degrees Celsius	°C
Degrees Fahrenheit.....	°F
Diameter	∅
Dry metric ton	dmt
Foot	ft
Gallon	gal
Gallons per minute (US).....	gpm
Gigawatt-hours	GWh
Gram.....	g
Grams per litre.....	g/L
Grams per tonne	g/t
Greater than	>
Hectare (10,000 m ²)	ha
Hertz.....	Hz
Horsepower	hp
Hour.....	h
Hours per day.....	h/d
Hours per week	h/wk
Hours per year.....	h/a
Inch.....	"
Kilo (thousand)	k
Kilogram	kg
Kilograms per cubic metre.....	kg/m ³
Kilograms per hour	kg/h
Kilograms per square metre	kg/m ²
Kilojoule.....	kJ
Kilometre	km

Kilometres per hour	km/h
Kilonewton	kN
Kilopascal	kPa
Kilovolt	kV
Kilovolt-ampere	kVA
Kilovolts	kV
Kilowatt	kW
Kilowatt hour	kWh
Kilowatt hours per tonne.....	kWh/t
Kilowatt hours per year.....	kWh/a
Less than	<
Litre	L
Litres per minute.....	L/m
Megabytes per second	Mb/s
Megapascal	MPa
Megavolt-ampere	MVA
Megawatt	MW
Megawatt-hours.....	MWh
Metre	m
Metres above sea level	masl
Metres per minute	m/min
Metres per second.....	m/s
Metric ton (tonne)	t
Micrometre (micron)	µm
Miles per hour.....	mph
Milliamperes	mA
Milligram	mg
Milligrams per litre	mg/L
Millilitre.....	mL
Millimetre	mm
Million	M
Million tonnes	Mt
Minute (plane angle).....	'
Minute (time)	min
Month.....	mo
Nanoteslas	nT
Newton	N
Newtons per metre	N/m
Ounce	oz
Parts per billion.....	ppb
Parts per million.....	ppm
Pascal (newtons per square metre)	Pa
Pascals per second	Pa/s
Percent	%
Phase (electrical).....	Ph
Pound(s)	lb
Pounds per square inch	psi
Power factor	pF
Revolutions per minute.....	rpm
Second (plane angle)	"
Second (time)	s
Specific gravity	SG

Square centimetre	cm ²
Square foot	ft ²
Square inch	in ²
Square kilometre	km ²
Square metre	m ²
Thousand tonnes	kt
Tonne (1,000 kg)	t
Tonnes per day	t/d
Tonnes per hour	t/h
Tonnes per year	t/a
Total dissolved solids	TDS
Total suspended solids	TSS
Volt	V
Week	wk
Weight/weight	w/w
Wet metric ton	wmt
Yard	yd
Year (annum)	a
Year (US)	y

Abbreviations/Acronyms

Acid base accounting	ABA
Acid rock drainage	ARD
Alternating current	AC
Ammonium nitrate	AN
Ammonium nitrate and fuel oil	ANFO
Association for the Advancement of Cost Engineering	AACE
Autogenous grinding	AG
Average emission factor	AEF
Bed volume	BV
Blue Coast Metallurgy Ltd.	Blue Coast
British Columbia	BC
Canadian	CDN
Canadian dollars	CAD or C\$
Canadian Electrical Manufacturers Association	CEMA
Canadian Gas Association	CGA
Canadian Institute of Mining and Metallurgy	CIM
Canadian Metals Exploration Ltd	CME
Canadian Standards Association	CSA
Capital cost allowance	CCA
Closed-circuit television	CCTV
Coarse ore storage	COS
Cominco Engineering Services Ltd.	CESL
Commissioned land surveyor	CLS
Compound annual growth rate	CAGR
Degree of alteration	DOA
Democratic Republic of Congo	DRC
Differential global positioning system	DGPS
Differential pressure	DP
Direct current	DC
Distributed control system	DCS

Effective grinding length	EGL
Electric vehicle	EV
Electrical resistance	Ohm
Energy storage system.....	ESS
Engineering, procurement, and construction management	EPCM
Environmental impact assessment	EIA
Environmental impact statement.....	EIS
Environmental, social & governance	ESG
Fisheries and Oceans Canada.....	DFO
Flow coefficient.....	CV
Free on board.....	FOB
Front-end loader.....	FEL
Global positioning survey	GPS
Global positioning system	GPS
Goods and Sales Tax (Canada).....	GST
Greenhouse gas.....	GHG
Hard Creek Nickel Corporation	HNC
Helicopter-borne electromagnetic	HBE
High density polyethylene	HDPE
High pressure	HP
High voltage	HV
High-pressure acid-leaching.....	HPAL
High-pressure grinding rolls	HPGRs
Horizontal-to-vertical ratio	H:V
Induced polarisation	IP
Input/output	I/O
Institute of Electrical and Electronics Engineers	IEEE
Instrumentation and control.....	I&C
Internal rate of return	IRR
International Standards Organization.....	ISO
Isopropyl xanthate collector	SIPX
Kerr Wood Leidal Ltd.....	KWL
Kirkham Geosystems Ltd.	Kirkham
Knight Piesold Ltd.	KP
Kutcho Copper Corporation	Kutcho
Land and Resource Management Plan.....	LRMP
Light emitting diode	LED
Liquified natural gas	LNG
Load-haul-dump unit (scooptram)	LHD
Local area network	LAN
London Metal Exchange.....	LME
Low grade.....	LG
Low pressure	LP
Methyl isobutyl carbinol	MIBC
Mill head value	MHV
Motor control centre	MCC
National Building Code of Canada	NBC
National Electrical Manufacturers Association	NEMA
National Electrical Safety Code.....	NESC
National Inventory Report (Canada)	NIR
Net present value	NPV
Net smelter royalty	NSR

Nickel pig iron	NPI
Nickel-cobalt-aluminum	NCA
Nickel-manganese-cobalt	NMC
Northwest Transmission Line	NTL
Not potentially acid-generating	NPAG
Occupational Safety and Health Administration	OSHA
Original equipment manufacturer	OEM
Overburden	OB
Overflow	O/F
Oversize	O/S
Papua New Guinea	PNG
Personal computer	PC
Phase (electrical)	Ph
Plant control system	PCS
Platinum Group Elements	PGEs
Polyvinyl chloride	PVC
Potentially acid generating	PAG
Power factor	pF
Preliminary economic assessment	PEA
Process flow diagram	PFD
Provincial Sales Tax	PST
Qualified person	QP
Relative humidity	RH
Rock mass rating	RMR
Rock quality designation	RQD
Run-of-mine	ROM
Semi-autogenous grinding	SAG
Supervisory control and data acquisition	SCADA
Tahltan Central Government	TCG
Tailings management facility	TMF
Traditional Land Use	TLU
Treatment and refining charges	TC/RC
Unconfined compressive strength	UCS
Underflow	U/F
Undersize	U/S
Uninterruptible power supply	UPS
Union Miniere Exploration and Mining Corporation Ltd.	UMEX
Valued ecosystem component	VEC
Variable frequency drive	VFD
Very high frequency	VHF
Very low frequency	VLf
Virtual private network	VPN
Volatile compound	VOC
Volt direct current	VDC
Water treatment plant	WTP
Wood Mackenzie	WM
Workplace Hazardous Material Information System	WHMIS